

Planning Proposal

Amendment to the Zoning and Height of Building Map for Lake Macquarie Private Hospital - Gateshead

Draft Amendment to *Lake Macquarie Local Environmental Plan 2014*

Post-Gateway version

| | |
|---|---|
| Local Government Area: | Lake Macquarie City Council (Council) |
| Name of Draft LEP: | Draft Amendment to <i>Lake Macquarie Local Environment Plan 2014</i> – Lake Macquarie Private Hospital |
| Subject Land: | Lake Macquarie Private Hospital 3 Sydney Street, 2 & 4 Casey Street, 36 & 38 Pacific Highway, Gateshead |
| Land Owners: | Ramsay Health Care Australia Pty Ltd |
| Applicant: | Akalan Projects on behalf of Ramsay Health Care Australia Pty Ltd |
| Department of Planning, Industry and Environment Reference Number: | PP-2021-6648 |
| Gateway Determination Date: | 27/09/2022 |
| Council Reference Number | RZ/13/2021 |
| Document Date: | October 2022 |
| Document Author: | Amber Stewart – Strategic Planner |
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| Version | Date | Details |
|---------|--------------|---|
| 1 | June 2022 | Council endorsement for Gateway Determination |
| 2 | October 2022 | Post-Gateway Public Exhibition |

INTRODUCTION

This planning proposal relates to Lake Macquarie Private Hospital (LMPH), 3 Sydney Street, 2 & 4 Casey Street, 36 & 38 Pacific Highway, Gateshead.

The hospital opened in 1973 with initially 36 beds, offering general surgery, orthopaedic, gynaecology and elective cosmetic surgery. The hospital has grown to 187 beds, expanded its services to include cardio-vascular, intensive care ward, emergency department, and a specialist radiology and pathology suite.

The hospital is now operating at or near capacity and requires additional space to provide services that meet the needs of the growing Lake Macquarie population and wider Hunter region. The proponent is undertaking a State Significant Development Application (SSD-38025700) with the NSW Department of Planning and Environment (The Department) to enable the development of a hospital expansion.

The proponents are seeking an amendment to the height of building map for the northern part of the site, from 10m to 37m to facilitate the expansion of the hospital. A building height limit of 37m (which equates to 10 storeys) was identified as the height required to contain the new theatres, beds, car parking and consulting suites needed to meet the projected demands.

Following Gateway Determination, The Department have proposed also applying an SP2 Infrastructure (Health Services Facilities) zoning to the site.

PART 1 – OBJECTIVES OR INTENDED OUTCOMES

The intended outcome of this planning proposal is to facilitate a State Significant Development (SSD) proposal for the expansion of LMPH, which will:

- deliver on identified strategic goals for Gateshead as a regionally significant health precinct;
- enable a hospital expansion that supports future healthcare needs of our community;
- encourage a cluster of medical facilities and services at Gateshead, including LMPH, which opens possibilities for an expanded, regionally significant health precinct. This precinct would complement the increased density and diversity of housing in surrounding areas such as Windale, Whitebridge and Kahibah;
- capture significant local, regional and state, social and economic benefits including substantial private financial investment, construction and operational employment and multiplier effects, improved healthcare product and other public benefits;
- facilitate delivery of public domain improvements, improved connectivity and activation;
provide infrastructure and related uses, and prevent development that is not compatible with or that may detract from the provision of infrastructure, also provide land required for the development or expansion of major health, education and community facilities.

While this planning proposal seeks to enable an SSD through local provisions, the physical development is being considered separately through the SSD assessment process. It should be noted other applications could be made under the proposed planning controls should this specific development not proceed.

PART 2 – EXPLANATION OF PROVISIONS

The proposed objectives will be achieved by amending the LMLEP 2014 with the following changes:

| Table 1: Proposed Changes to LMLEP 2014 Maps and Instrument | | |
|---|---|--|
| Item No. | Address | Explanation of provisions |
| 1 | Part Lot 90 DP 1233497, Lot 6,7 and 8 DP 24268 | Height increase from 10m to 37m Amend Height of Buildings Map from 10m to 37m (See sites identified on the Height of Buildings Maps as shown in PART 6). |
| 2 | Lot 90 DP 1233497, Lot 2 DP 1223084, Lot 4,6,7 and 8 DP 24268 | Rezone from R3 Medium Density Residential to SP2 Infrastructure (Health Services Facilities). |

PART 3 – JUSTIFICATION

A. NEED FOR THE PLANNING PROPOSAL

1. *Is the planning proposal a result of any strategic study or report?*

No. The proposal was put forward by the applicant to facilitate the expansion of the existing hospital as it is operating at near capacity.

2. *Is the planning proposal the best means of achieving the objectives or intended outcomes, or is there a better way?*

Yes, a planning proposal to amend the LMLEP 2014 is considered the most appropriate means of achieving the identified objectives and intended outcomes.

A building height limit of 37m (which equates to 10 storeys) was identified as the height required to contain the new theatres, beds, car parking and consulting suites needed to meet the projected demands.

B. RELATIONSHIP TO STRATEGIC PLANNING FRAMEWORK

3. *Is the planning proposal consistent with the objectives and actions contained within the applicable regional or sub-regional strategy (including the Sydney Metropolitan Strategy and exhibited draft strategies)?*

Hunter Regional Plan 2036 (HRP)

The planning proposal supports the Hunter Regional Plan's (HRP) aim of growing the region's economy and supporting the growth of local communities. The expansion of the hospital supports increased demands as the Lake Macquarie and Hunter populations grow. It also provides a number of new jobs through both the initial construction and ongoing operation of the hospital.

The site is located within the Greater Newcastle area. The HRP 2036 recognises that this area is a growing area for health services with an aim to develop a national Centre of Excellence for Health and Education.

Direction 8: Promote innovative small business and growth in the service sectors

The planning proposal seeks to support the expansion of the existing hospital. As the hospital is located adjacent to the Pacific Highway the expansion of the hospital meets the goals of this direction as it will expand opportunities for health services to use the hospital.

Direction 26: Deliver infrastructure to support growth and communities

This direction speaks to supporting growing communities through the expansion of infrastructure, including health services. This proposal is consistent with this direction as it will support the expansion of the hospital and its services, supporting expected demand from the growing and aging population that is forecast for Lake Macquarie and the Greater Hunter region.

Draft Hunter Regional Plan 2041 (DHRP 2041)

The existing Hunter Regional Plan includes a commitment for its regular review. The review provides an opportunity to consider the changes in the last 5 years that affect the region, the challenges and opportunities ahead, and update the plan to respond.

The draft Hunter Regional Plan 2041 (the draft Plan) builds on the previous plan which was finalised in October 2016 and resets the regional plan priorities to ensure it continues to respond to the region's needs for the next 20 years.

Objective 7: Plan for businesses and services at the heart of healthy, prosperous and innovative communities

Objective 7 speaks to the need to have services, including health care readily accessible to the growing population. This proposal is consistent with this direction as it will facilitate the expansion of the hospital. Expanding the hospital will provide new services to support the current and future population of the region.

In summary, the planning proposal is considered to be consistent with the draft Hunter Regional Plan 2041, as it will contribute to supporting the growing and aging population that the region will experience. It is also located in a geographically advantageous position that is not at risk to flooding or bushfire with easy access to the Pacific Highway. This is important for ensuring the ongoing resilience for the region.

Greater Newcastle Metropolitan Plan 2036 (GNMP)

The planning proposal is consistent with and supports the objectives of Greater Newcastle Metropolitan Plan 2036 (GNMP) specifically Strategy 4: Grow health precincts and connect the health network. The GNMP identifies the site as being part of a major health precinct (Figure 17 from the GNMP), which has the ability to provide additional job opportunities and support an aging population.

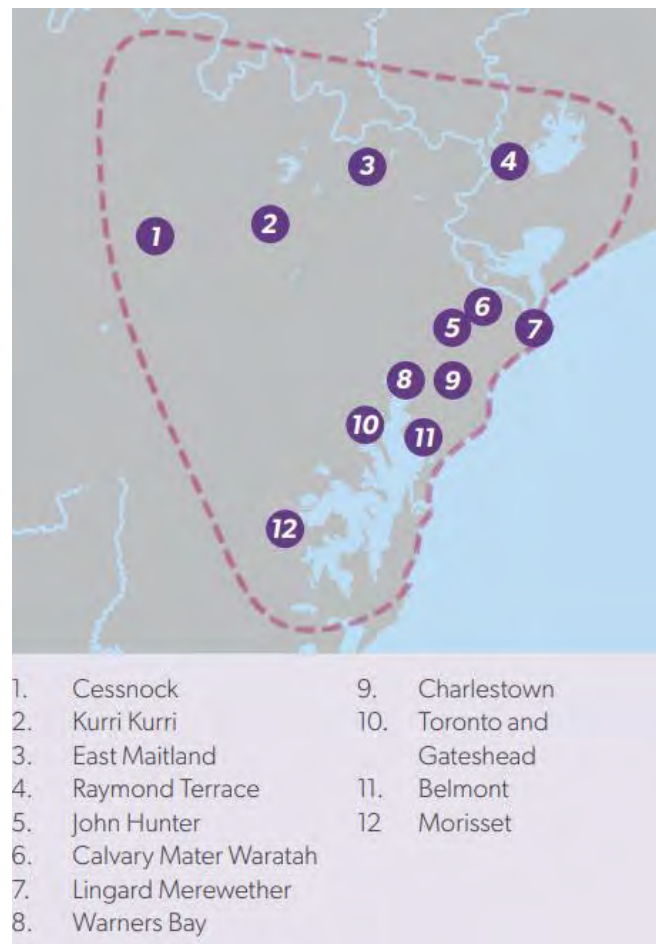


Figure 1 – Major Health Precincts in Greater Newcastle – Figure 17 from GNMP

4. *Is the planning proposal consistent with the local council's Community Strategic plan or other local strategic plan?*

Community Strategic Plan 2017-2027 (CSP)

The Lake Macquarie City Community Strategic Plan 2017-2027 has been developed with the people of Lake Macquarie outlining the vision and values of the community and providing clear strategies to achieve this. The Proposal is consistent with the vision for a diverse economy as well as lifestyle and wellbeing. The planning proposal will support a sustainable and diverse economy whilst providing the community with access to adaptable and inclusive community and health services.

Local Strategic Planning Statement (LSPS)

The planning proposal is consistent with and supports the Lake Macquarie City LSPS, its planning priorities and actions for the City. The LSPS identifies that the hospital is part of the North East Growth Area and envisages the Gateshead health precinct to grow and expand (page 42). Specifically, the Proposal supports the principles of the LSPS that aim to respond to and encourage development of new education, health and innovation clusters especially Action 3.10 Prepare a Gateshead Medical Precinct concept plan to facilitate the orderly development of this medical precinct including allied health and other supporting businesses. This Proposal intends to support the expansion of the LMPH encouraging more employment opportunities and densities in the Gateshead Health Precinct. Therefore, it is

considered that this Planning Proposal aligns with the broad directions of the Lake Macquarie City LSPS.

C. Is the planning proposal consistent with State Environmental Planning Policies? (SEPPs)

An assessment of the planning proposal and its consistency with the applicable State Environmental Planning Policies is provided in Table 2 below.

Table 2: Planning proposal consistency with relevant SEPPs

| SEPP and Relevance | Implications |
|--|--|
| State Environmental Planning Policy (Planning Systems) 2021 | |
| <i>Chapter 2 – State and regional development</i> | The proposal is to facilitate the expansion of the hospital. This development will be facilitated through an SSD application. The proposal is consistent with this policy and will assist the assessment of the SSD for the expansion of the hospital. |
| State Environmental Planning Policy (Industry and Employment) 2021 | |
| <i>Chapter 3 – Advertising and signage</i> | Any signage associated with future commercial premises on the Site would be assessed and approved in accordance with this SEPP. |
| State Environmental Planning Policy (Transport and Infrastructure) 2021 | |
| <i>Chapter 2 – Infrastructure</i> The aim of the policy is to facilitate the expansion of the hospital. | This SEPP provides for certain proposals, known as Traffic Generating Development, to be referred to Transport for NSW for concurrence. Referral may be required for the expansion of the existing LMPH where the size or capacity satisfies certain thresholds. Schedule 3 lists the types of development that are defined as Traffic Generating Development. Details of the development would be confirmed at the development application stage following the planning proposal. The SEPP enables development for the purposes of Health Services Facilities within the SP2 zone and the proposed expansion of LMPH is permitted with consent on the site. |

D. Is the proposal consistent with Ministerial Directions made under S 9.1?

An assessment of the planning proposal and its consistency with the applicable Ministerial Directions is provided in Table 3 below.

Table 3: Planning Proposal consistency with relevant Ministerial S 9.1 Directions

| Relevant s9.1 Directions and Objectives | Consistency/Comment |
|--|--|
| Focus Area 1: Planning Systems | |
| 1.1 Implementation of Regional Plans Give legal affect to the vision, land use strategy, goals, directions and actions contained in Regional Plans | Consistent. The proposal is consistent with the Greater Newcastle Metropolitan Plan 2036 and the overarching Hunter Regional Plan 2036 and draft Hunter Regional Plan 2041. The proposed zone will facilitate the expansion of the hospital and the availability of local jobs and health services. |
| 1.3 Approval and Referral Requirements Ensure that LEP provisions encourage the efficient and appropriate assessment of development. | Consistent. The proposal is consistent with this direction as it does not seek to include provisions which require concurrence, consultation or referral of development applications to a Minister or public authority and will not identify development as designated development. |
| 1.4 Site Specific Provisions Discourage unnecessarily restrictive site-specific planning controls. | Consistent. The proposed change to the height of building map and zone will allow the future expansion of the hospital. It is considered not restrictive. The detail of this development is subject to a separate SSD application. |
| Focus area 3: Biodiversity and Conservation | |
| 3.1 Conservation Zones To protect and conserve environmentally sensitive areas. | Consistent. The proposed amendment does not impact any Conservation zoned land. |
| 3.2 Heritage Conservation To conserve items, areas, objects and places of environmental heritage significance and indigenous heritage significance. | Consistent: There are no known, listed or identified items of indigenous heritage significance; or other areas, objects and environmental places of significance applicable to the site. |
| Focus area 4: Resilience and Hazards | |
| 4.1 Flooding (a) Ensure that development of flood prone land is consistent with the NSW Government's Flood Prone Land Policy and the principles of the Floodplain Development Manual 2005, and | Consistent. The site is not identified as flood prone land. |

| Relevant s9.1 Directions and Objectives | Consistency/Comment |
|---|--|
| (b) Ensure that the provisions of a LEP on flood prone land are commensurate with flood behavior and include consideration of the potential flood impacts on and off the subject land. | |
| 4.2 Coastal Management To protect and manage coastal areas of NSW. | Consistent. The Land is not mapped within the Coastal Management SEPP 2018 as a Coastal area or Coastal Environmental Area. |
| 4.3 Planning for Bushfire Protection (a) Protect life, property and the environment from bush fire hazards, by discouraging the establishment of incompatible land uses in bush fire prone areas, and (b) Encourage sound management of bush fire prone areas. | This site is not identified as bushfire prone land. |
| 4.4 Remediation of Contaminated Land The objective of this direction is to reduce the risk of harm to human health and the environment by ensuring that contamination and remediation are considered by planning proposal authorities. | Consistent. The site is not identified as contaminated land. The existing uses of the site are for car parking and residential accommodation and the subject sites have not been used for any activity listed as potentially contaminating land use or activity. The proposal will facilitate the expansion of the existing hospital located to the south of the subject sites. |
| 4.5 Acid Sulfate Soils The objective of this direction is to avoid significant adverse environmental impacts from the use of land that has a probability of containing acid sulfate soils. | This site is not identified as containing acid sulfate soils. |
| 4.6 Mine Subsidence and Unstable Land The objective of this direction is to prevent damage to life, property and the environment on land identified as unstable or potentially subject to mine subsidence. | The subject site is located within a mine subsidence district. Preliminary studies have been undertaken which did not identify any known concerns which would prohibit development. Subsidence Advisory NSW will be included in the agency consultation of this proposal prior to undertaking community consultation. Further detailed studies will also be undertaken as part of the State Significant Development Application. |

| Relevant s9.1 Directions and Objectives | Consistency/Comment |
|--|--|
| Focus area 5: Transport and Infrastructure | |
| <p>5.1 Integrating Land Use and Transport Ensure that urban structures, building forms, land use locations, development designs, subdivision and street layouts achieve the following planning objectives:</p> <ul style="list-style-type: none"> (a) improving access to housing, jobs and services by walking, cycling and public transport, and (b) increasing the choice of available transport and reducing dependence on cars, and (c) reducing travel demand including the number of trips generated by development and the distances travelled, especially by car, and (d) supporting the efficient and viable operation of public transport services, and (e) providing for the efficient movement of freight. | <p>Consistent. The proposal seeks to increase the maximum permitted building height, to facilitate the expansion of the existing hospital. The site is highly accessible by an extensive local and regional road network including Pacific Highway. Bus stops along Pacific Highway provide services between Newcastle and Belmont. The provision of additional health services on the site will make use of established road infrastructure and public transport bus routes and improve viability of the public transport system through increased demand.</p> |
| Focus area 6: Housing | |
| <p>6.1 Residential Zones</p> <ul style="list-style-type: none"> (a) Encourage a variety and choice of housing types to provide for existing and future housing needs, (b) Make efficient use of existing infrastructure and services and ensure that new housing has appropriate access to infrastructure and services, and (c) Minimise the impact of residential development on the environment and resource lands. | <p>Inconsistent. The site is currently zoned R3 Medium Density Residential, however, is used for the purposes of an approved health services facility. The conditions of the Gateway Determination require the zone to be changed to SP2 Infrastructure consistent with the existing and ongoing use of the site. The proposal is consistent with the Hunter Regional Plan 2036, the Greater Newcastle Metro Plan 2036 and the Lake Macquarie Local Strategic Planning Statement and is consistent with this Direction.</p> <p>Even though this proposal is inconsistent, it is justified due to the existing use, intended strategic direction and public benefit provided by the hospital</p> |

E. Environmental, Social and Economic Impact

1. Is there any likelihood that critical habitat or threatened species, populations or ecological communities or their habitats, will be adversely affected as a result of the proposal?

The site is extensively developed with a mix of hospital uses, and residential and car parking associated with the adjoining hospital. There are no known critical habitat or threatened species, populations, ecological communities or their habitats that will be adversely affected due to the proposal.

2. Are there any other likely environmental effects as a result of the Planning Proposal and how are they proposed to be managed?

The potential environmental impacts relate to:

- The visual impact to the surrounding area and overshadowing.
- Traffic and parking
- Mine subsidence

Visual Impact

A Visual Impact Assessment (Attachment 1) and shadow analysis (Attachment 2) has been undertaken by the proponent to investigate the potential visual and solar impacts to neighbouring sites and the surrounding area.

Given the location of the proposed additional building height, overshadowing will mostly impact the existing hospital site.

While there will be some visual and overshadowing impact from the future development, these impacts are typical of an area undergoing transition and are considered acceptable when balanced against the strategic direction for the precinct and the social and economic benefits.

Traffic

A traffic and parking assessment (Attachment 3) has been undertaken by the proponent to support the SSD proposal. The report concludes that the existing road network and intersections are adequate to cope with the proposed hospital expansion. While the planning proposal seeks to amend planning controls, rather than proposing a specific development outcome, the report demonstrates that existing infrastructure can support development under the proposed changes. As such, the proposed change to the maximum Height of Building (HOB) will not result in demand for additional road infrastructure upgrades.

Mine Subsidence

A desktop Mine Subsidence Risk study (Attachment 4) has been undertaken which did not identify any known concerns which would affect the proposed changes to the maximum permitted height of buildings.

3. Has the Planning Proposal adequately addressed any social and economic effects?

Yes. A high-level assessment of the social and economic benefits has been undertaken to support the SSD proposal (Attachment 5). The proposal to increase the maximum permitted building height will facilitate expansion of the hospital providing additional health services for the community in an easily accessible location. The planning proposal will enable an expansion of the hospital which has economic benefits to the local community with potential growth on approximately 189 new ongoing jobs (e.g. nurses, administration staff, cleaners, food preparation) and staff medical specialist roles (e.g. surgeons, anaesthetist and other specialists).

Expansion of the hospital facilitated by this planning proposal is also likely to create an additional 800 - 1,000 direct and in-direct jobs during the construction period.

Overall, the proposal will facilitate the expansion of the hospital which will result in positive economic and social outcomes for Lake Macquarie and the region.

F. State and Commonwealth Interests

4. Is there adequate public infrastructure for the Planning Proposal?

The Site is serviced by existing infrastructure that is capable of servicing expansion of LMPH under the proposed changes to the LEP. In particular the Site is accessible by the established local and regional road network, including Pacific Highway which is also a key public transport bus route.

5. What are the views of State and Commonwealth public authorities consulted in accordance with the gateway determination?

Consultation with State and Commonwealth public authorities will occur in accordance with the Gateway determination. Consultation will occur with the following authorities:

- Health NSW
- Subsidence Advisory NSW, and
- Transport for NSW

PART 4 – COMMUNITY CONSULTATION

The planning proposal will be formally exhibited in accordance with the Lake Macquarie Community Participation Plan and the Gateway determination. It is recommended that the planning proposal be exhibited for at least 28 days.

PART 5 – CONCLUSION

This planning proposal seeks to rezone the site to SP2 Infrastructure (Health Services Facilities) and also seeks to increase heights across Part Lot 90 DP 1233497, Lot 6,7 and 8 DP 24268 from 10m to 37m to facilitate an SSD proposal for the expansion of the LMPH.

This proposal is acceptable based on the strategic direction for the precinct and the social and economic benefits it provides.

PART 6 – MAPPING

1. Locality Map



2. Subject Land Map



- Subject Land
- Land Parcel

Air Photo

2022 Aerial Photography

Nearmap Imagery 2022

0 50
Metres

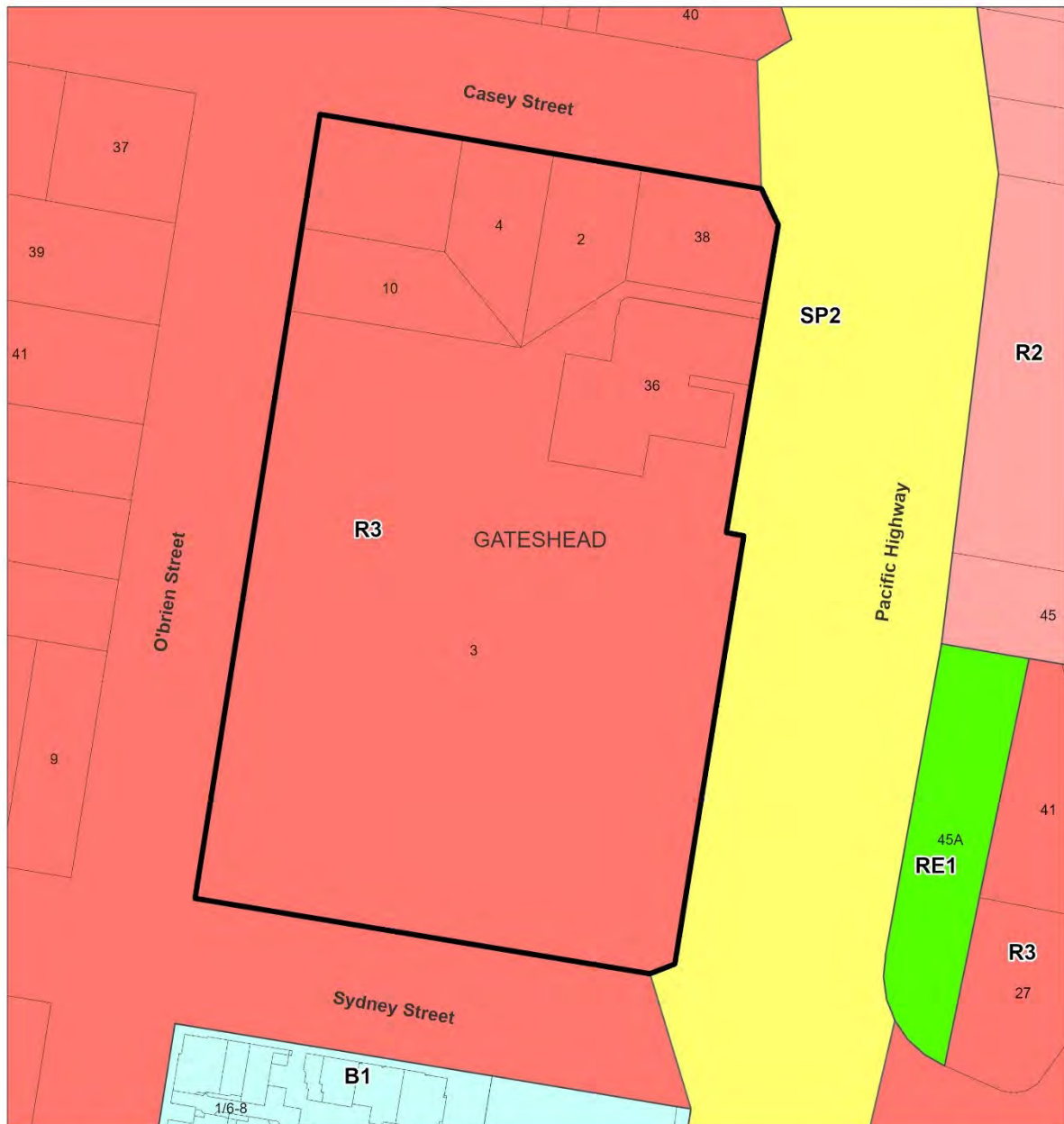
N
Projection GDA 1994
Zone 56



Date: 19/10/2022

Planning Proposal: RZ/13/2021

3. Current Land Zoning



- Legend**
- Subject Land
 - Land Parcel
 - Land Zoning**
 - B1 Neighbourhood Centre
 - R2 Low Density Residential
 - R3 Medium Density Residential
 - RE1 Public Recreation
 - SP2 Infrastructure

Existing
Land Zoning Map
 Lake Macquarie Local Environmental Plan 2014

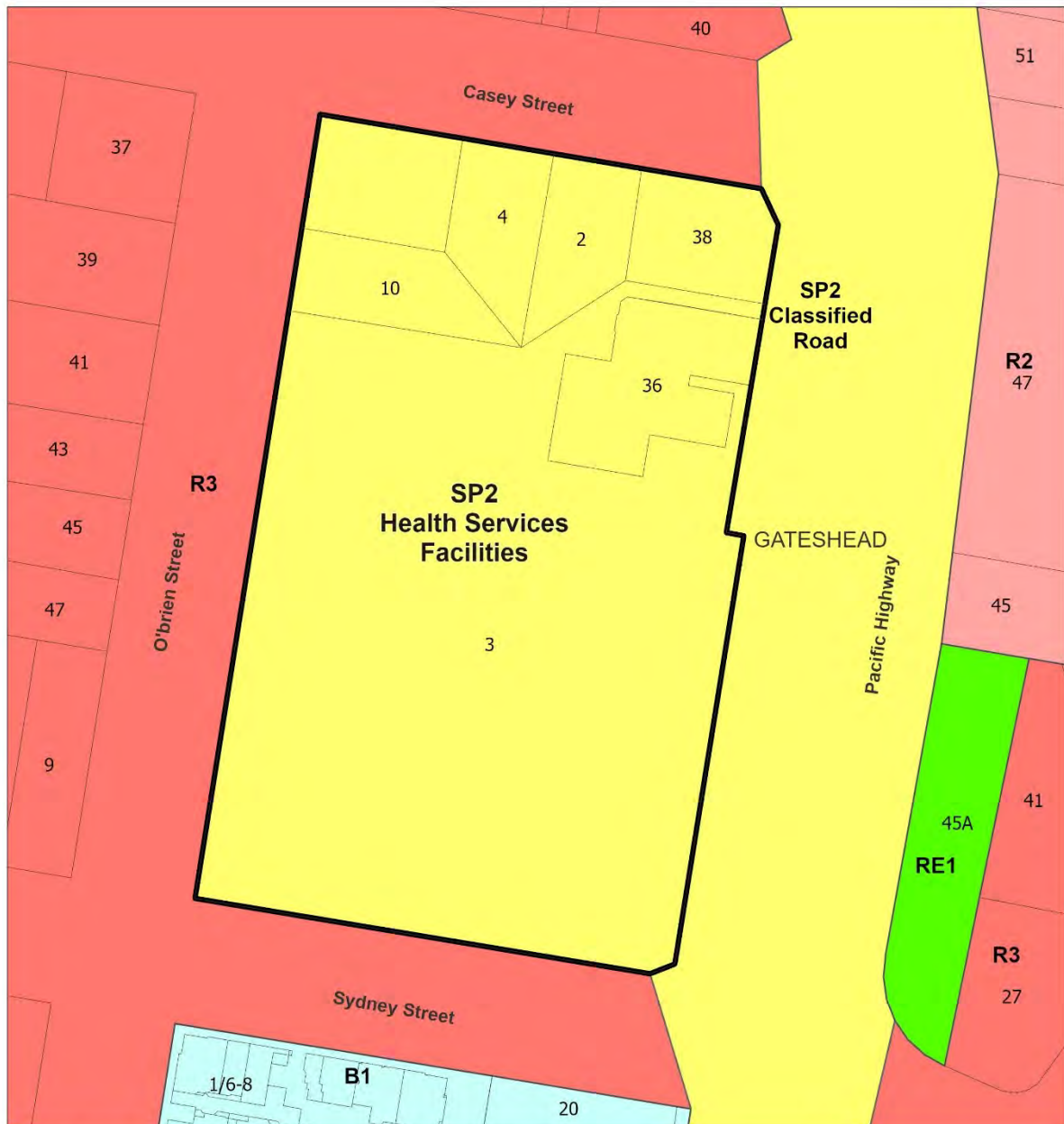
0 50
 Metres

N
 Projection GDA 1994
 Zone 56



Date: 19/10/2022 Planning Proposal: RZ/13/2021

4. Proposed Land Zoning



- Legend**
- Subject Land
 - Land Parcel
 - Land Zoning**
 - B1 Neighbourhood Centre
 - R2 Low Density Residential
 - R3 Medium Density Residential
 - RE1 Public Recreation
 - SP2 Infrastructure

Proposed

Land Zoning Map

Lake Macquarie Local Environmental Plan 2014



N
Projection GDA 1994
Zone 56



Date: 19/10/2022 Planning Proposal: F2014_01383

5. Existing Height of Building Map



6. Proposed Height of Building Map



PART 7 – PROJECT TIMELINE

| Stage | Timeframe (working days) and/or date |
|---|--------------------------------------|
| Gateway determination | 25 days Received 27/09/22 |
| Pre-exhibition (including agency consultation) | 50 days |
| Public exhibition (commencement and completion dates) | 28 days |
| Consideration of submissions | 20 days |
| Post exhibition review and additional studies (if required) | 55 days |
| Submission to Department to finalise LEP | 10 days |
| Gazettal of LEP Amendment | 45 days |

ATTACHMENTS

Attachment 1: Visual Impact Assessment

Attachment 2: Shadow analysis

Attachment 3: Traffic and parking assessment

Attachment 4: Mine Subsidence Risk study

Attachment 5: High-level social and economic benefits assessment

Attachment 1: Visual Impact Assessment

LAKE MACQUARIE PRIVATE HOSPITAL

Visual Impact Assessment Report

November 2021

Title: Lake Macquarie Private Hospital Visual Impact Assessment Report
Prepared for: Ramsay Health Care
Date: 29.11.2021
Status: Final
Prepared by: Hatch RobertsDay
Approved by: Hatch RobertsDay

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01

INTRODUCTION & METHODOLOGY

INTRODUCTION

PURPOSE OF THIS REPORT

Hatch RobertsDay has been commissioned by Ramsay Health Care to prepare this visual impact assessment (VIA) report in support of the planning proposal to amend Lake Macquarie Local Environmental Plan 2014 to include additional building height on the proposed site described as 3 Sydney Street, 2 & 4 Casey Street, 36 & 38 Pacific Highway, Gateshead.

The VIA investigates on the possible visual impacts that proposed building may have on the surrounding and adjacent publicly accessible areas, and provides detailed assessment of the sensitivity and magnitude of the changes from different vantage points in comparison to the existing.

PROPOSAL OVERVIEW

The proposed site is regular in shape and has a total area of approximately 14,041m². The Site presently contains the existing LMPH which is operated by Ramsay Health Care. LMPH adjoins low density residential development to the north, east and west of the Site as well as shop top housing and specialised medical consulting suites to the south.

The proposed amendment to LMLEP intends to facilitate the future redevelopment of the Site for an expansion to the existing Lake Macquarie Private Hospital (LMPH) comprising additional inpatient beds, inpatient theatres, day surgery theatres, consulting suites, oncology chairs and a pharmacy.

The concept design has been informed by detailed site analysis and consideration of the surrounding context in order to provide an optimal development outcome that capitalises on the strategic potential of the land, uplifts the surrounding public domain and provides a high level of amenity.



PROPOSED OFFICE BUILDING AND PARKING LOT

Proposal (Source: HPI Architects)

ASSESSMENT METHODOLOGY

CONTEXTUAL ANALYSIS

A number of locations were inspected to evaluate the scenic qualities and visual prominence of Lake Macquarie Private Hospital site to identify potential vantage viewpoints.

The key vantage points for the purpose of view analysis have been determined through identification of physical absorption capacity and visibility of the site as well as focus on the areas that are more likely to be affected by the proposal.

DETAILED ASSESSMENT METHODOLOGY

A qualitative assessment of the visual impacts and changes to landscape has been undertaken based on the following guidelines:

- RMS Environmental Impact Assessment Guidance Note: Guidelines for landscape character and visual impact assessment (2013)
- The Guidance for Landscape and Visual Impact Assessment (GLVIA), Third Edition (2013) prepared by the Landscape Institute and Institute of Environmental Management and Assessment; and Visual Representation of Development Proposals, Technical Guidance Note 02 (2017)
- The guidelines describe the assessment as a way to define the changes to the physical landscape and day to day visual effects of a project on people's views. The determination of the impacts is based on the following criteria:

Sensitivity is defined as "The sensitivity of a landscape character zone or view and its capacity to absorb change" (EIA No4 Guidelines, 2013, RMS).

The visual sensitivity of a view is defined by the nature of the view and its duration. A higher visual sensitivity is given to views which would be seen for longer, by a higher numbers of potential viewers and where visual amenity is important to viewers (value of the view). The context of the view and the distance from the views are also used to determine the visual sensitivity level of the landscape.

Magnitude is defined as "The measurement of the scale, form and character of a development proposal when compared to the existing condition" (EIA No4 Guidelines, 2013, RMS).

It reflects the degree of visual contrast between the proposal and the existing landscape setting. In the case of visual assessment this also relates to how far the proposal is from the viewer.

For the purposes of this assessment the criteria listed in the following tables have been specifically defined for sensitivity and magnitude of change for both the assessment of landscape character and the visual impact to viewpoints. The combined assessment of sensitivity and magnitude provides an overall rating of the visual impact, as shown in the Impact Level table.

VISUALISATION OF THE DEVELOPMENT AND PROPOSED SCENARIOS

Finalisation of the design and supporting technical

documentation enabled the selected vantage points to be realistically documented.

The accuracy of the existing and proposed images is based on the following process and information:

- Creating a 3D model of the terrain/ surrounding context based on the site survey information as well as the contour and cadastre information downloaded from SixMaps and Nearmap aerial image (georeferenced to GDA94/MGA56 geographical)
- Digitally linking the 3D massing model of the proposed built form provided by the project architect in the context 3D model
- Positioning camera in 3D software based on the viewpoints coordinate data recorded during site visit
- Importing actual photographs in 3D software to prepare proposed scenarios from vantage points based on existing coordination and identified reference points
- Photo matching and rendering to reflect landscaping, intended materials and lighting

Photomontages are intended to be printed at A3 and to be viewed at a distance of 300mm. That is the distance between the eye and the image and will enable the viewer to experience an approximation of what the proposed view would look like in the real world.

| | | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|------------|
| | | Very High | High | Moderate | Low | Very Low | Negligible |
| SENSITIVITY | Very High | Substantial | Very High | High | High/Moderate | Moderate | None |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low | None |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low | None |
| | Low | High / Moderate | Moderate | Moderate/ Low | Low | Low/ Negligible | None |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible | None |

Table 1. Impact Level (Matrix of Sensitivity & Magnitude)

| Sensitivity | Criteria |
|------------------|--|
| Very High | Nationally designated landscape with high conservation or heritage value and absence of landscape detractors. Protected views identified in planning policy designation, State designated publicly accessible landscape or heritage assets. |
| High | Locally designated valued landscape with many distinctive characteristics and very few landscape detractors. Public views with a high visual prominence and a high number of users in close proximity, private views in close proximity, passive recreational receptors where the landscape has a high visual value. Travellers on road, rail or other transport routes where travel involves recognised scenic routes. |
| Moderate | Landscape with some distinctive characteristics and few landscape detractors. Public views with a moderate visual value and a moderate number of users in close proximity, active recreational receptors where the landscape has little visual value. |
| Low | Landscape with few distinctive characteristics and presence of landscape detractors. Public views with a little visual value and a low number of users, where receptors are mostly road users in motor vehicles or passers-by, people at their work place or views from commercial buildings where the landscape has some visual value. |
| Very Low | Landscape with no distinctive characteristics and presence of many landscape detractors. Public views with none visual value and a limited number of users not in close proximity, people at their work place or views from commercial buildings where the landscape has little or no visual value. |

Table 2.Sensitivity Ranking Criteria

| Magnitude | Criteria |
|-------------------|---|
| Very High | Total loss or major change to key characteristics of the existing landscape. The proposal forms a significant and immediately apparent part of the scene. It significantly contrasts in scale and character (either existing or planned). It is severely detrimental to the quality of the scene. |
| High | Notable loss or change to key characteristics of the existing landscape. The proposal forms a dominant feature of the scene to which other elements become subordinate. It contrasts in scale and character (either existing or planned). It is reducing the quality of the scene. |
| Moderate | Partial loss or change to key characteristics of the existing landscape. The proposal forms a visible new element within the overall scene, yet one that is relatively compatible with the surrounding character (either existing or planned) and view's composition. It is possibly reducing the quality of the scene. |
| Low | Minor loss or change to key characteristics of the existing landscape. The proposal constitutes only a minor component of the wider view, that is compatible with the surrounding character (either existing or planned) and view's composition. |
| Very Low | Limited or no loss or change to key characteristics of the existing landscape. The proposal constitutes only a minor component of the wider view, which might be missed by the casual observer or receptor. Awareness of the proposal would not have an effect on the overall quality of the scene. |
| Negligible | No change in the landscape or view. |

Table 3. Magnitude Ranking Criteria

02

SITE ANALYSIS

LOCAL CONTEXT

LOCAL CONTEXT

The proposed site is located within the suburb of Gateshead which forms part of the Lake Macquarie local government area (LGA). It is situated approximately 15km south west of Newcastle Central Business District (CBD). The Site affords road linkages to Pacific Highway and Newcastle Inner City Bypass. The Site is also highly accessible via public transport including bus services on Pacific Highway and Oxford Street.

The surrounding context exhibits a number of residential and recreation uses, mainly characterised by low density residential housing shop top housing and specialised medical consulting suites known as Lake Macquarie Specialist Centre. It is noted that the Site comprises an existing health services facility known as the LMPH and has been integrated harmoniously within its context.



Sportfields



Low Density Residential



Existing Lake Macquarie Private Hospital



Commercial/ Retail



St Mary's Catholic College



Local School



PHOENIX CHARLESTOWN
BASEBALL CLUB



LOW DENSITY
HEALTHY RESIDENTIAL



LOW DENSITY
HEALTHY RESIDENTIAL



ST MARY'S
CATHOLIC SCHOOL



WIRIPAANG
PUBLIC SCHOOL



HUNTER SPORTS
PUBLIC SCHOOL



ALLEN DAVIS FIELD



INDUSTRIAL AREAS



SITE

LAKE MACQUARIE SCENIC MANAGEMENT GUIDELINES 2013

Lake Macquarie Scenic Management Guidelines document guides decisions regarding scenic and landscape values at the planning proposal stage. The visual impact analysis considers the following guidelines to ensure the scenic and landscape values are protected surrounding the site and provide responses to the relevant guidelines.

LANDSCAPE TYPE

The Scenic Management Guidelines introduces four landscape types for Lake Macquarie LGA. The proposed site is located in the **Hinterland** landscape type of Lake Macquarie LGA where views of the lake or coast are generally not available.

LOCATIONS SENSITIVE TO VISUAL CHANGE

Significant natural landscape features, natural landscape types with inherent natural values and landscapes with heritage or cultural values are identified as visually sensitive landscapes in the Lake Macquarie Scenic Management Guidelines. The proposed site is within an area which is not identified as part of lake or coastal landscape and does not have any conservation values, indigenous landscapes and other heritage significance. Therefore, the proposed site is not considered to be a visually sensitive landscape. However, the site is located along Pacific Highway with potentially a high visibility from the main road and a high visual sensitivity to change from this location.

SCENIC MANAGEMENT ZONES

The proposed site is within **Gateshead** landscape setting and **12 (hinterland, moderate settlement)** Scenic Management Zone.

GATESHEAD

A moderate level of development exists around the proposal, with residential areas consisting of mostly detached housing. Mix of uses present, including a dominance of health facilities, commercial and industrial.

The Lake Macquarie Scenic Management Guidelines requires future developments to have regards to protecting native vegetation and vegetation in and around residential areas and commercial centres. Any views of development from main roads should be softened by screening vegetation and appropriate design measures such as set-backs.

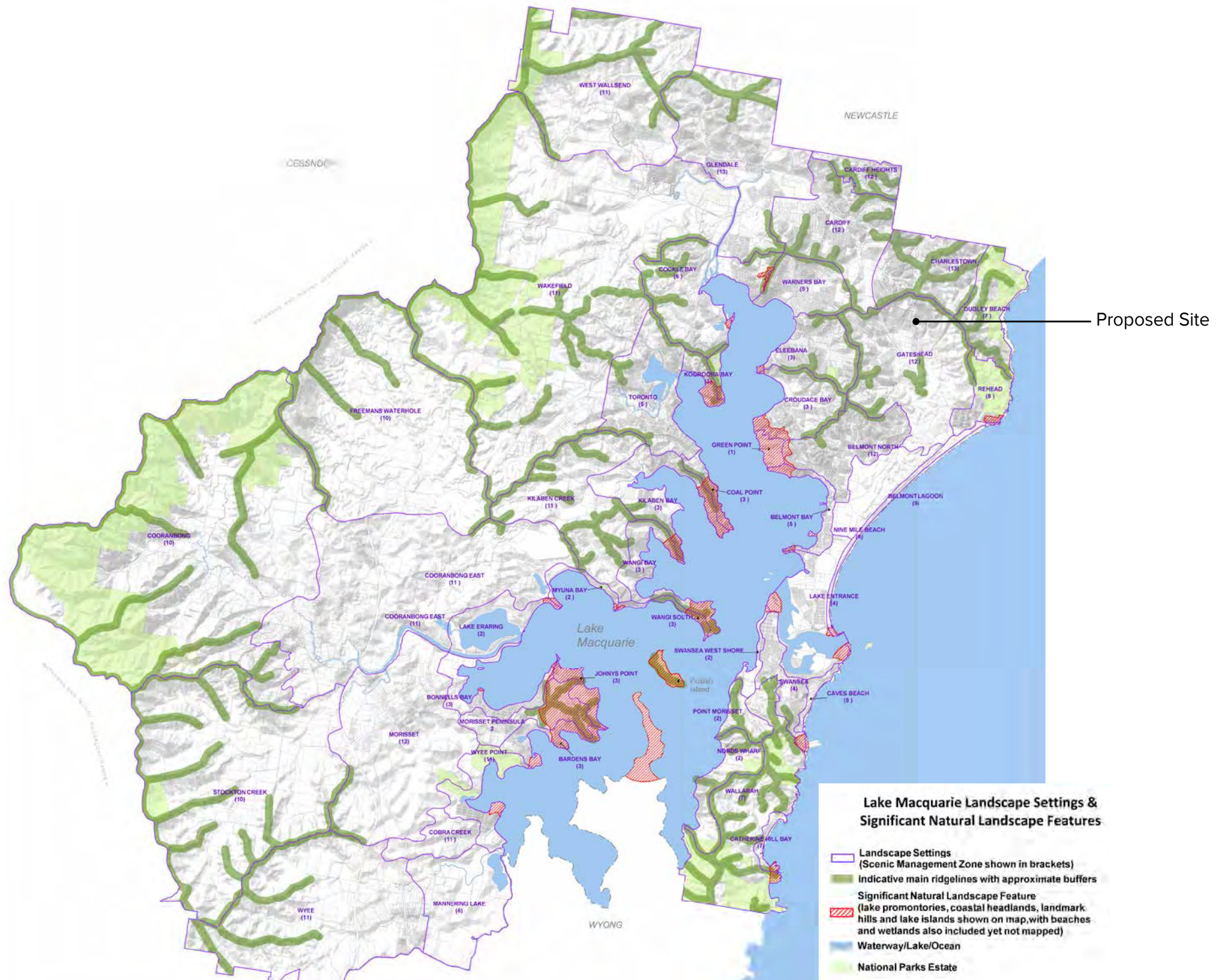
Any development within these areas is to satisfy a number of guidelines which are covered on page 32 of this report.

COMMERCIAL DEVELOPMENT AND TOWN CENTRES

The Guidelines recommends following design measures to improve visual outcomes in the category of Commercial Development and Town Centres:

- Ensure all opportunities taken to increase street trees and other streetscape improvements;
- Where suitable reduce the width of street pavements through measures such as widening footpaths and breaking-up car parking lanes with landscaping, this can encourage outdoor café dining which will activate the street;
- Identify existing view corridors to surrounding natural features such as the lake, coastline or western ranges and ensure these are preserved and enhanced where possible;
- Any proposed commercial/industrial development, particularly along main roads and town centres, should be treated with non-garish (i.e. overly bright) colours, limit overwhelming signage and increase amenity through appropriate landscaping;
- Identify opportunities to introducing view corridors when new developments are proposed; and
- Maintain a human-like scale to provide suitable amenity to centres through the use of continuous low awnings.

Refer to page 32 for our response to the guidelines where applicable.



03

VISUAL ANALYSIS

VANTAGE POINTS

THE VISUAL CATCHMENT

Visibility

The visibility of a site is influenced by a number of factors. These include physical factors such as topography, the pattern and alignment of streets, character of open space, type of vegetation, and the ability of the existing and future elements of the landscape setting to physically hide, screen or disguise the proposed development. It also includes other factors such as distance, direction and angle of view as well as the siting and scale of the proposal.

Due to the existing highway and location of the site as a corner lot, land to the immediate east and north is considered to have the greatest potential for visual exposure of the proposal. In addition, due to the low density character of the precinct and relatively larger number of local residents which may be exposed to the proposal, Casey Street was considered to also be of particular interest as part of the VIA.

Visual Receptors

People within the visual catchment who will be affected by the changes in views and visual amenity are referred to as visual receptors. There are a number of different types of visual receptor for the proposal:

- Travellers on Pacific Highway from north and south- high number of receptors
- Member and visitors of the educational facilities from east- medium number of receptors
- Residents at home and visitors from north and west- low number of receptors
- People engaged in outdoor recreation from south west- medium number of receptors

SELECTION OF VANTAGE POINTS

The key vantage points for the purpose of visual impact assessment have been determined through identification of visual catchment and visibility of the site as well as focus on the areas that are more likely to be affected by the proposal. This includes nearby public receivers and significant vantage points in the broader public domain.

The key vantage points analysed include:

- Public open space along Johnsons Creek
- Pacific Highway
- Surrounding streets including Casey Street, O'Brien Street and Oxford Street
- St Paul's Primary School

“*Landscape and Visual Assessment (LVA) is an essential tool of reconciling development with landscape and scenic values and promoting better outcomes for our communities.*”

Guidance Note for Landscape and Visual Assessment, 2018



View 1

View 3

View 4

View 2

View 5

View 6



VISUAL IMPACT ASSESSMENT

Viewpoint 1- from public open space along Johnsons Creek



Google Earth Coordinate: 32°58'55.4"S 151°41'15.7"E

Viewpoint 1

The aim of assessing the view is:

- To understand the visual impact of the proposal viewed from the public open space where people are engaged in outdoor recreation
- To assess to what degree the existing vegetation and structures screen or disguise the future development
- To test the extent to which the change of built elements may alter the existing character of the view

| SENSITIVITY | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|
| | Very High | High | Moderate | Low | Very Low | Negligible |
| | Very High | Substantial | Very High | High | High/Moderate | Moderate |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low |
| | Low | High / Moderate | Moderate | Moderate/ Low | Low | Low/ Negligible |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible |

Impact Level - Existing context (Matrix of Sensitivity & Magnitude)

| SENSITIVITY | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|
| | Very High | High | Moderate | Low | Very Low | Negligible |
| | Very High | Substantial | Very High | High | High/Moderate | Moderate |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low |
| | Low | High / Moderate | Moderate | Moderate/ Low | Low | Low/ Negligible |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible |

Impact Level - Potential Future context (Matrix of Sensitivity & Magnitude)

Sensitivity

The sensitivity of view from the public open space along Johnsons Creek factors the following:

- The public open space is used for passive and active recreation including walking, exercising and relaxing. Users engaged in passive recreation are more sensitive to visual change of their surroundings
- High numbers of receptors

However, the visual value is considered to be low due to the existing urban character and landscape detractors. As a result, the sensitivity of the view is considered MODERATE.

Magnitude

The magnitude of the proposal in this view is considered MODERATE in existing context and NEGLIGIBLE in potential future context, due to:

- Proposal forms a relatively dominant feature of the scene and contrasts in scale and massing with the existing low density character. However, the extent of the area over which the changes are visible is low. In other words, the change to the view's composition is relatively low
- Proposal is in the distance
- Proposal will not be visible from this location in the potential future context

The visual impact for this view is assessed as MODERATE in existing context and NONE in potential future context.



Existing



Proposed



Potential Future

Viewpoint 2- from Pacific Highway



Google Earth Coordinate: 32°59'02.2"S 151°41'30.5"E

| | | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|------------|
| | | Very High | High | Moderate | Low | Very Low | Negligible |
| SENSITIVITY | Very High | Substantial | Very High | High | High/Moderate | Moderate | None |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low | None |
| | Moderate | High | High/Moderate | Moderate | Moderate/ Low | Low | None |
| | Low | High / Moderate | Moderate | Moderate/ Low | Low | Low/ Negligible | None |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible | None |

Impact Level (Matrix of Sensitivity & Magnitude)

Viewpoint 2

The aim of assessing the view is:

- To understand the visual impact of proposed built forms viewed from the main highway
- To assess to what degree the existing structures and buildings screen or disguise the future development
- To test the extent to which the change of built elements may alter the existing character of the view

Sensitivity

The view from Pacific Highway considered to have MODERATE sensitivity due to:

- Although the number of receptors is considered to be high, they have short term views to the proposal
- Receptors are mostly travellers on road that are less likely to notice, appreciate or be concentrating on views
- Public view has limited visual value due to the existing urban character with limited natural elements

Magnitude

The magnitude of the proposal in this view is considered LOW, due to:

- Proposal is in the distance
- Proposal is partly screened by the existing structures and vegetation
- The proportion of the view occupied by the proposed development is low

The visual impact for this view is assessed as MODERATE/ LOW, which is the combination of the sensitivity and magnitude of impact.



Existing

Proposed Building



Proposed

Viewpoint 3- from Casey Street



Google Earth Coordinate: 32°58'47.9"S 151°41'24.6"E

Viewpoint 3

The aim of assessing the view is:

- To understand the visual impact of proposed built forms viewed from the surrounding residential street
- To assess to what degree the existing vegetation screen or disguise the future development
- To test the extent to which the change of built elements may alter the existing character of the view

| | | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|------------|
| SENSITIVITY | | Very High | High | Moderate | Low | Very Low | Negligible |
| | Very High | Substantial | Very High | High | High/Moderate | Moderate | None |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low | None |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low | None |
| | Low | High / Moderate | Moderate | Moderate/ Low | Low | Low/ Negligible | None |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible | None |

Impact Level - Existing context (Matrix of Sensitivity & Magnitude)

| | | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|------------|
| SENSITIVITY | | Very High | High | Moderate | Low | Very Low | Negligible |
| | Very High | Substantial | Very High | High | High/Moderate | Moderate | None |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low | None |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low | None |
| | Low | High / Moderate | Moderate | Moderate/ Low | Low | Low/ Negligible | None |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible | None |

Impact Level - Potential Future context (Matrix of Sensitivity & Magnitude)

Sensitivity

The view from Casey Street is considered to have MODERATE sensitivity due to:

- Public view is from a low density residential street
- Although public view has limited visual value, visual amenity is important to receptors which are mainly the local residents
- Moderate numbers of receptors in close proximity

Magnitude

The magnitude of the proposal in this view is considered HIGH in existing context and

MODERATE in potential future context, due to:

- Proposal forms a relatively dominant feature of the scene and contrasts in scale and massing with the existing low density character. However, the extent of the area over which the changes are visible is low
- Proposal is partly screened by existing vegetation, including large trees
- There will be less visual contrast between the proposal and the surrounding setting in the potential future context which reduces the magnitude

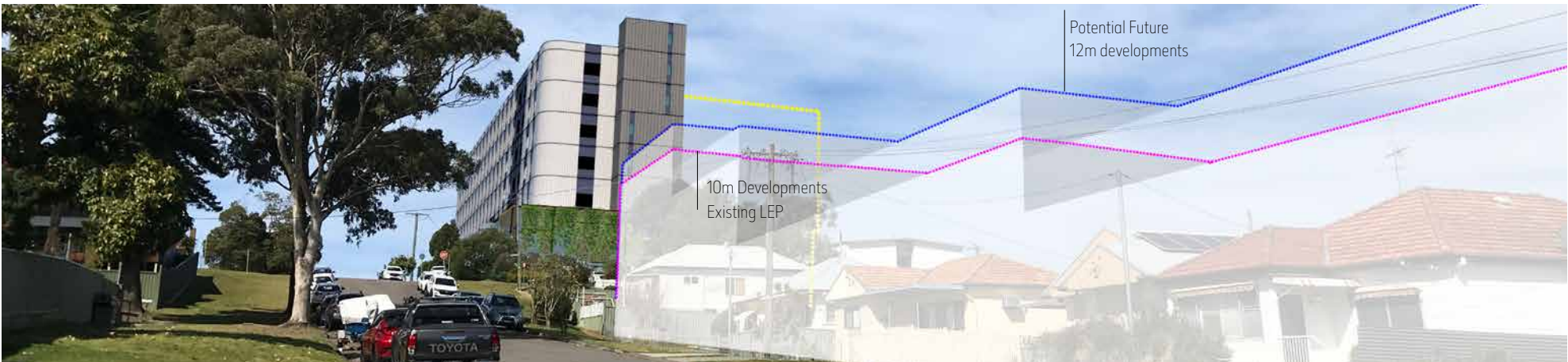
The visual impact for this view is assessed as HIGH/ MODERATE in existing context and MODERATE in potential future context.



Existing



Proposed



Potential Future

Viewpoint 4- from O'Brien Street



Google Earth Coordinate: 32°58'45.9"S 151°41'29.3"E

Viewpoint 4

The aim of assessing the view is:

- To understand the visual impact of proposed built forms viewed from the surrounding residential street
- To assess to what degree the existing vegetation screen or disguise the future development
- To test the extent to which the change of built elements may alter the existing character of the view

| | | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|------------|
| | | Very High | High | Moderate | Low | Very Low | Negligible |
| SENSITIVITY | Very High | Substantial | Very High | High | High/Moderate | Moderate | None |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low | None |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low | None |
| | Low | High / Moderate | Moderate | Moderate/ Low | Low | Low/ Negligible | None |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible | None |

Impact Level - Existing context (Matrix of Sensitivity & Magnitude)

| | | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|------------|
| | | Very High | High | Moderate | Low | Very Low | Negligible |
| SENSITIVITY | Very High | Substantial | Very High | High | High/Moderate | Moderate | None |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low | None |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low | None |
| | Low | High / Moderate | Moderate | Moderate/ Low | Low | Low/ Negligible | None |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible | None |

Impact Level - Potential Future context (Matrix of Sensitivity & Magnitude)

Sensitivity

The view from O'Brien Street is considered to have MODERATE sensitivity due to:

- Public view is from a low density residential street
- Although public view has limited visual value, visual amenity is important to receptors which are mainly the local residents
- Moderate numbers of receptors in close proximity

Magnitude

The magnitude of the proposal in this view is considered VERY HIGH in existing context and

MODERATE in potential future context,due to:

- The proposal forms a dominant feature of the scene and contrasts in scale and massing with the existing low density character
- The proportion of the view occupied by the proposal is high. As a result, the change to the view's composition is relatively high
- There will be less visual contrast between the proposal and the surrounding setting in the potential future context- The proposal will be largely screened

The visual impact for this view is assessed as HIGH in existing context and MODERATE in potential future context.



Existing

Proposed Building



Proposed



Potential Future

Viewpoint 5- from Oxford Street



Google Earth Coordinate: 32°58'43.2"S 151°41'32.3"E

Viewpoint 5

The aim of assessing the view is:

- To understand the visual impact of proposed built forms viewed from the main highway and adjacent residential street
- To assess to what degree the existing structures and buildings screen or disguise the future development
- To test the extent to which the change of built elements may alter the existing character of the view

| | | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|------------|
| SENSITIVITY | | Very High | High | Moderate | Low | Very Low | Negligible |
| | Very High | Substantial | Very High | High | High/Moderate | Moderate | None |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low | None |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low | None |
| | Low | High / Moderate | Moderate | Moderate/ Low | Low | Low/ Negligible | None |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible | None |

Impact Level - Existing context (Matrix of Sensitivity & Magnitude)

| | | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|------------|
| SENSITIVITY | | Very High | High | Moderate | Low | Very Low | Negligible |
| | Very High | Substantial | Very High | High | High/Moderate | Moderate | None |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low | None |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low | None |
| | Low | High / Moderate | Moderate | Moderate/Low | Low | Low/ Negligible | None |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible | None |

Impact Level - Potential Future context (Matrix of Sensitivity & Magnitude)

Sensitivity

The view from Oxford Street is considered to have **LOW** sensitivity due to:

- Receptors are mostly travellers on road that are less likely to notice, appreciate or be concentrating on views
- Public view has limited visual value due to the existing urban character with limited natural elements
- Low number of receptors from Oxford Street. The viewpoint is also representative of the view from Pacific Highway. In this case, number of receptors is considered to be high however, they have short term views to the proposal.

Magnitude

The magnitude of the proposal in this view is considered **HIGH** in existing context and **MODERATE** in potential future context, due to:

- The proposal forms a relatively dominant feature of the scene and contrasts in scale and massing with the existing low density character. However, it is partly screened by the existing landscape detractors including housing, structures and utility poles
- There will be less visual contrast between the proposal and the surrounding setting in the potential future context which reduces the magnitude

The visual impact for this view is assessed as **MODERATE** in existing context and **MODERATE/ LOW** in potential future context.

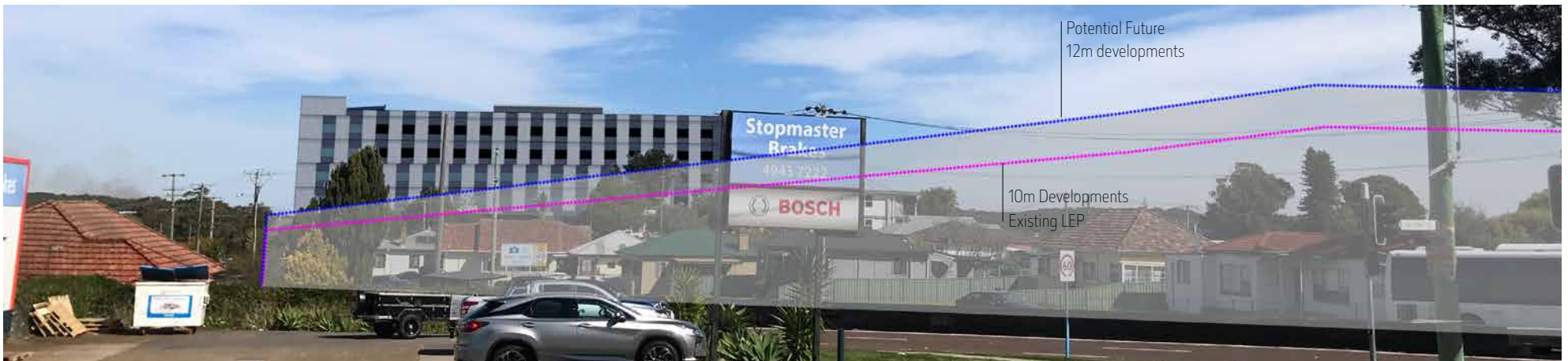


Existing

Proposed Building



Proposed



Potential Future

Viewpoint 6- from St Paul's Primary School



Google Earth Coordinate: 33°48'43.1"S 150°58'29.6"E

| | | MAGNITUDE | | | | | |
|-------------|-----------|-----------------|---------------|----------------|-----------------|-----------------|------------|
| | | Very High | High | Moderate | Low | Very Low | Negligible |
| SENSITIVITY | Very High | Substantial | Very High | High | High/Moderate | Moderate | None |
| | High | Very High | High | High/ Moderate | Moderate | Moderate/Low | None |
| | Moderate | High | High/Moderate | Moderate | Moderate/Low | Low | None |
| | Low | High / Moderate | Moderate | Moderate/Low | Low | Low/ Negligible | None |
| | Very Low | Moderate | Moderate/ Low | Low | Low/ Negligible | Negligible | None |

Impact Level (Matrix of Sensitivity & Magnitude)

Viewpoint 6

The aim of assessing the view is:

- To understand the visual impact of proposed built forms viewed from the surrounding educational facilities
- To assess to what degree the existing structures and buildings screen or disguise the future development
- To test the extent to which the change of built elements may alter the existing character of the view

Sensitivity

The sensitivity of view from St Paul's Primary School has LOW sensitivity due to:

- The attention of people will be focused on their work and activities, not on their surrounding
- Students engaged in active recreation are less sensitive to visual change of their surroundings

Magnitude

The magnitude of the proposal in this view is considered MODERATE due to:

- The proposal forms a relatively dominant feature of the scene and contrasts in scale and massing with the existing low density character. However, the extent of the area over which the changes are visible is low.
- Proposal is not in close proximity and is partly screened by existing school's buildings and facilities

The visual impact for this view is assessed as MODERATE/ LOW, which is the combination of the sensitivity and magnitude of impact.



Existing

Proposed Building



Proposed

RESPONSE TO SCENIC MANAGEMENT GUIDELINES

Guidelines

| |
|---|
| View corridors to the lake, coast and western ranges along streets, within public reserves and from town centres are retained and enhanced where possible |
| Car parks should be sited and designed to not dominate views from public areas or main roads |
| New and increased recreational activities within public reserves may be suitable, yet should aim to preserve and improve important natural features and public access |
| Existing ridgeline vegetation which provides a dominant backdrop to views from main roads, the lake and coast is retained |
| opportunities to rehabilitate any degraded areas are identified |
| Any proposed commercial/industrial development along main roads, in particular, should be treated with non-garish (i.e. overly bright) colours, limit overwhelming signage and increase amenity through appropriate landscaping |
| Neighbourhood centres should be enhanced with landscape improvements and street tree planting |
| Any views of development from the coast or lake should be softened by screening vegetation and appropriate design measures such as set-backs |
| Green breaks that provide visual relief to the urban area should be preserved, and enhanced, where possible |

Our Response

| |
|--|
| There is no view corridor to the lake, coast or any significant ranges around the proposal. |
| The proposal accommodates ground floor active uses along Pacific Highway to create visual interest and activation. The car park facade is integrated into design and screened by greenery. Therefore, it is not considered to be a dominant feature when viewed from surrounding vantage points. |
| There is no recreational activities as a result of the proposal. No natural features or public spaces will be affected. |
| Pacific Highway is providing views to the northern and southern ridgelines (refer to page 15). These views are not affected by the proposed development. |
| Not applicable. |
| The proposed modular facade is treated with non-garish colours and some neutral tones which blend in with the natural surroundings. The facade incorporates greenery with climbing plants to increase the visual amenity and soften the views. |
| Street trees are retained which reduce the visual impact perceived from the surrounding main roads. |
| Not applicable. |
| The area surrounding the site is not highly developed (mainly low density detached housing) which requires less visual relief. However, the proposal incorporates green facade, facade articulation and adequate setbacks to reduce the bulk and provide some visual relief in the built form. |

CONCLUSION

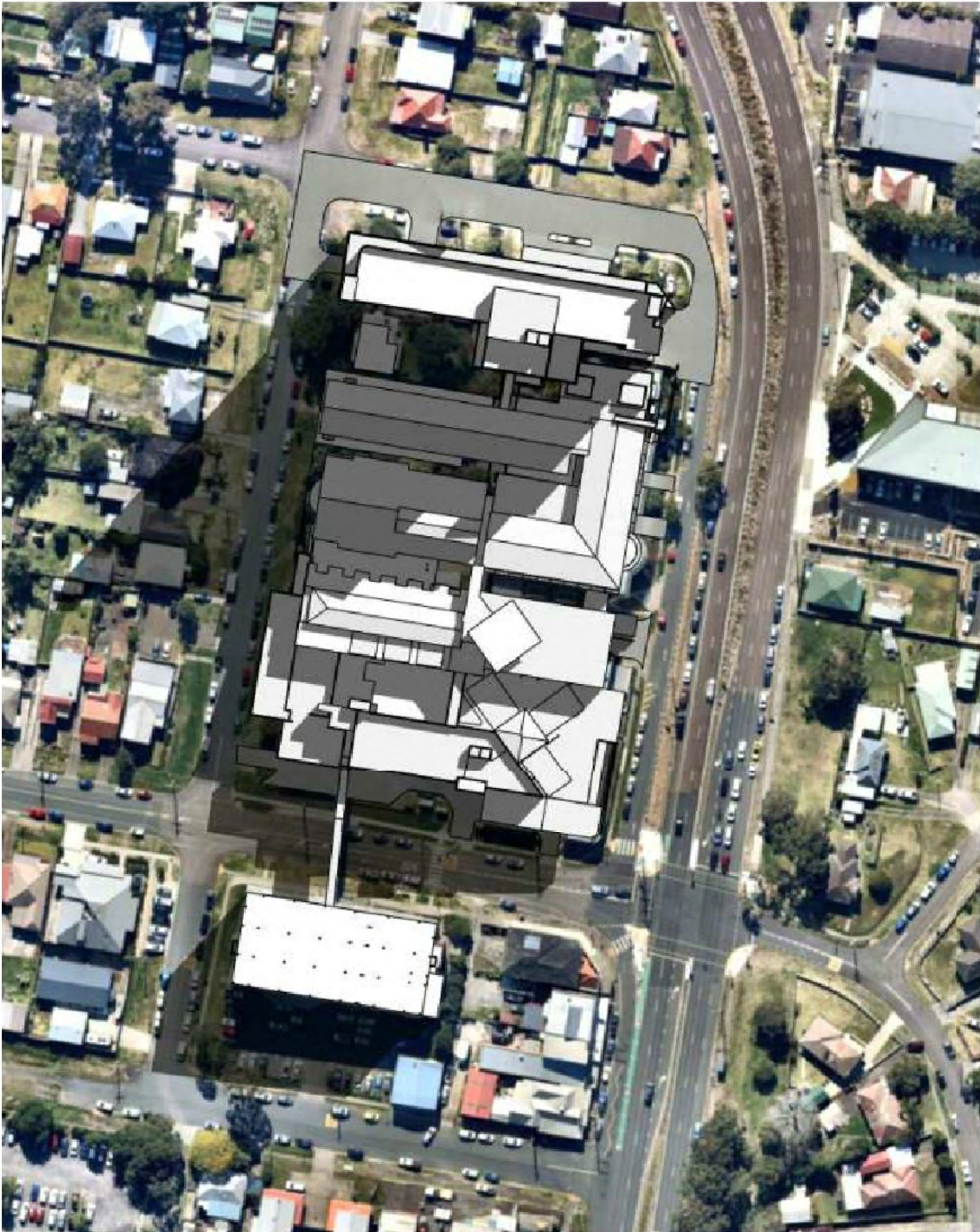
In general, the visual sensitivity of the views are considered Moderate to Low. The proposal is located in the Hinterland landscape type of Lake Macquarie LGA where views of the lake or coast are not available. The area surrounding the proposal does not have any scenic or conservation values and is not considered to be a visually sensitive landscape. However, the proposed site is fronting Pacific Highway with a high visibility which increases the visual sensitivity to change. It is argued that receptors in Pacific Highway are mostly travellers on road that are passing through therefore have short term views and are less likely to notice, appreciate or be concentrating on views. In addition, surrounding local streets are low traffic volume roads with a low number of potential viewers.

The proposal forms a visible new element and a relatively dominant feature of the overall scene in some of the vantage points. As a result, the magnitude of proposal is considered High to Moderate in the current context. However, it is anticipated that the Gateshead Precinct go through some future transformations to become one of the major health destinations in the area. As a result, the magnitude of proposal is considered Moderate in the potential future context.

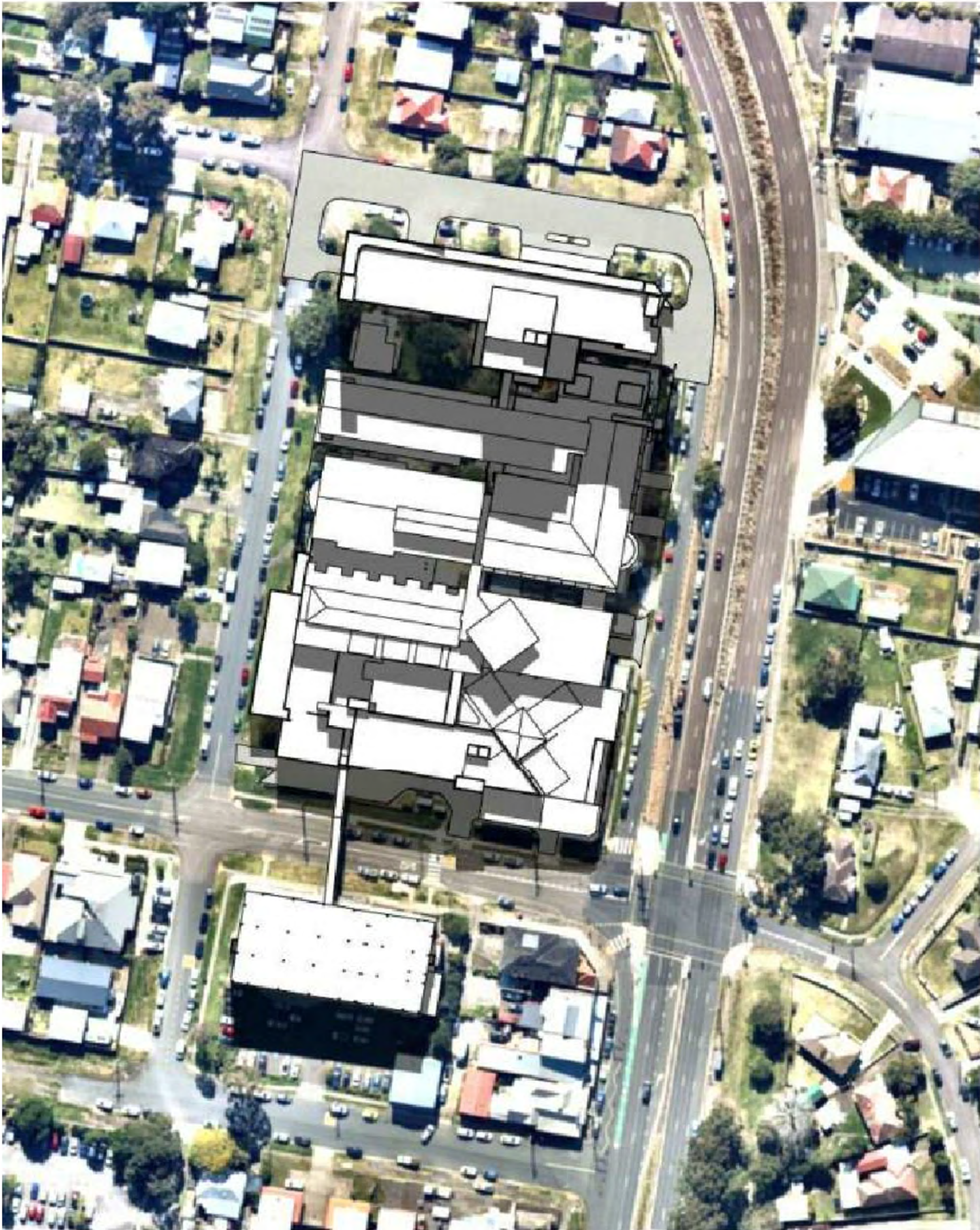
In summary:

- The proposal is consistent and compatible with the future planned character of the Gateshead as a regionally significant health precinct and contributes to the evolving character of the area from a residential neighbourhood to a health hub;
- The proposal is consistent with the requirements in the Lake Macquarie Scenic Management Guidelines;
- The strategic location of the site along Pacific Highway is ideal to create a gateway tower as an iconic entry to Gateshead Health Precinct;
- It is anticipated that the surrounding lands around the Private Hospital will accommodate health allied services and medium density housing to support the Precinct. Therefore, there will be less visual contrast between the proposal and the surrounding setting compared to the existing low density scenario;
- There already exists a presence of landscape detractors in all vantage points including existing structures, housing, utility poles, billboards and etc. which reduce the dominance of the proposal;
- Existing vegetation and mature trees along main streets partly screen the proposal and reduce the visual impact; and
- The proposal does not reduce the quality of the scenes by delivering design excellence.
- Use of facade treatment, articulation and colour selection reduce the bulk impact and increase the visual amenity.

Attachment 2: Shadow analysis



1. WINTER SOLSTICE 9AM



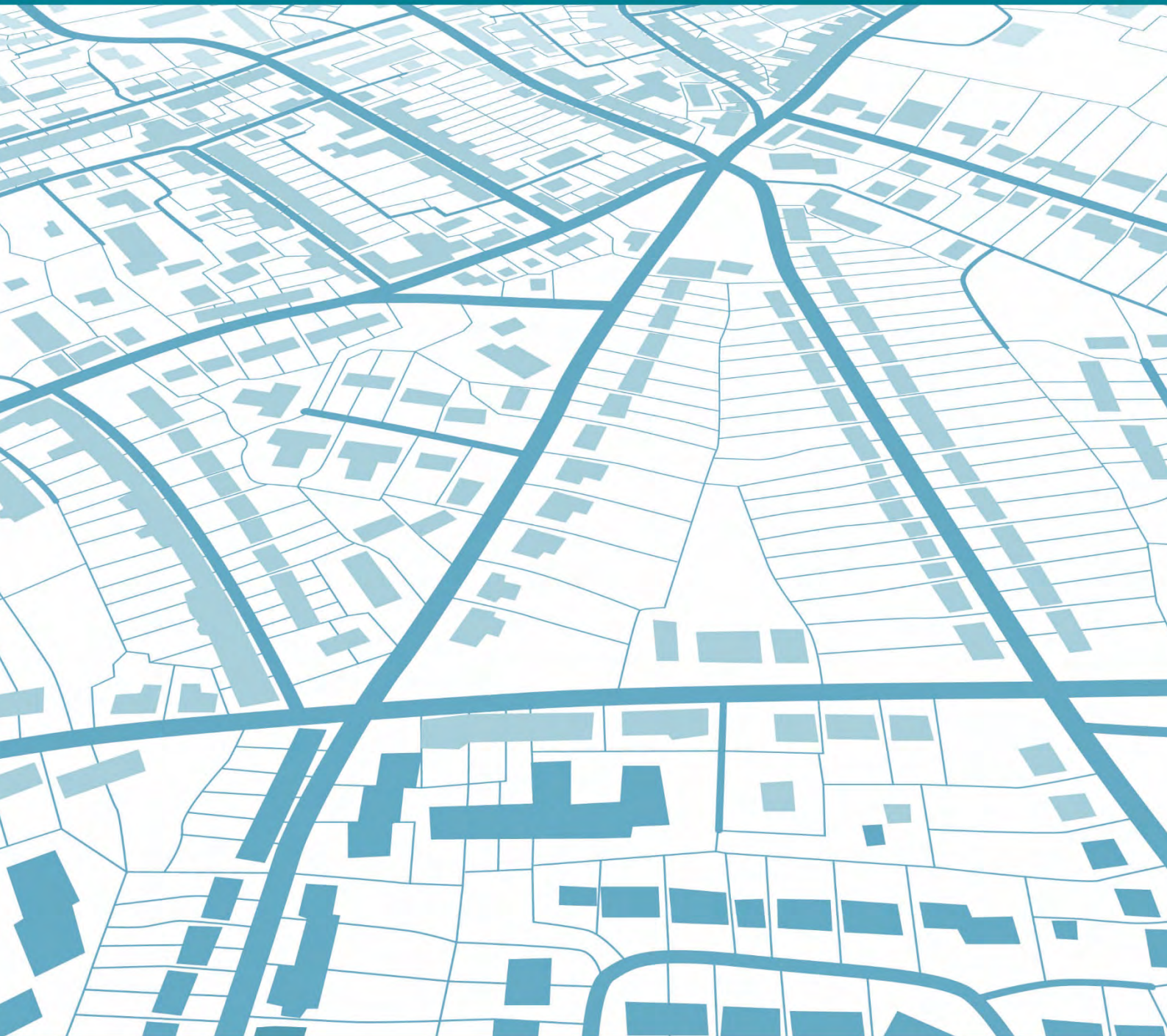
2 WINTER SOLSTICE 12NOON



3 WINTER SOLSTICE 3PM

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|--|----------------------|---------------|------------------|
| 1 | FIRST ISSUE | 25.10.21 | HS |
| REV | REVISION DESCRIPTION | DATE | BY |
| Project LAKE MACQUARIE PRIVATE HOSPITAL MASTERPLAN | | | |
| Principal RAMSAY HEALTHCARE PTY LTD | | | |
| <div><div></div><div></div></div> | | | |
| <div><div></div><div></div><div>HEALTH PROJECTS INTERNATIONAL Architects and Health Facility Planners 401-403 15th-17th Ground Floor, Suite 1, 68 Alfred Street, Missions Point, NSW 2061 Ph: (02) 9460 4199 Fax: (02) 9460 4299</div></div> | | | |
| Block/ Zone | Drawn HC | Checked HS | Date 25.10.21 |
| Drawing Title SHADOW DIAGRAMS | | | Scale/s NTS |
| Days No. LMPH17-DA-SH | | | Issue 1 |
| CAD File LMPH17-DA-SH | | | |

Attachment 3: Traffic and parking assessment



Lake Macquarie Private Hospital Planning Proposal

Traffic and Parking Assessment

Ref: 21297
Date: OCT 2021
Rev: C

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1.0 Introduction

This report has been prepared for Ramsay to provide a Traffic, Transport and Parking Assessment to accompany a Planning Proposal which forms part of a Development Masterplan for a significant upgrade of the Lake Macquarie Private Hospital that includes:

- Planning Proposal to permit the height of the proposed Ward Tower building
- staged development
- expansion of the Hughes Street car park
- alterations and additions which are subject to existing consents

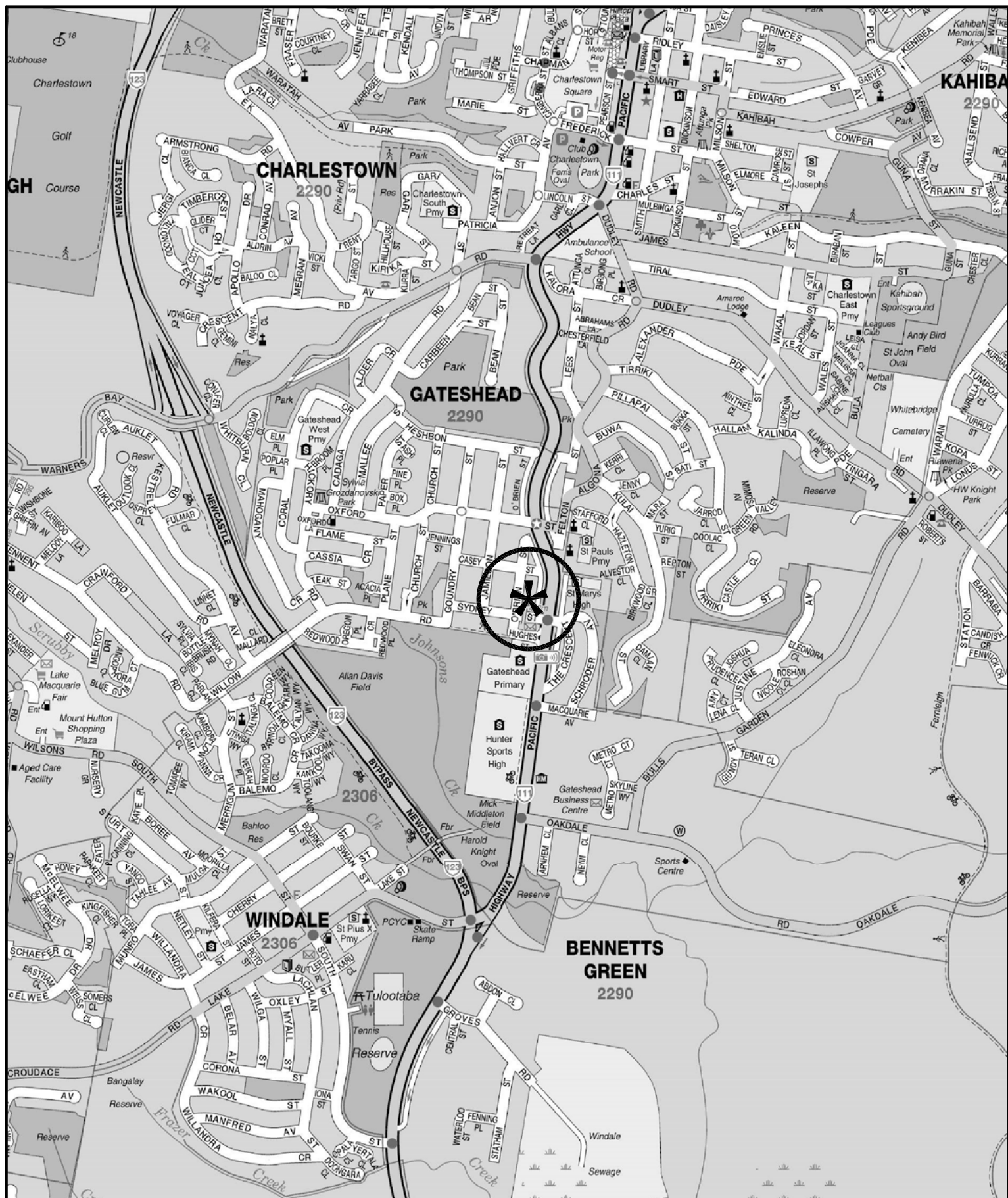
Lake Macquarie Private Hospital (Figure 1) provides healthcare services for the Newcastle and Lake Macquarie areas as well as the Hunter and New England areas. The hospital is a 187 bed “Acute Medical and Surgical Facility”, with Emergency Department and Cancer Centre, linked by overhead walkway to the Lake Macquarie Specialist Centre which provides radiology and pathology services and contains medical consulting suites.

The Hospital has been subject to increasing demands for its services due to the increasing number and aging of the population in the Central Coast area and there have been a number of alterations and additions undertaken over the years while there are 2 outstanding development consents which have not been implemented as yet.

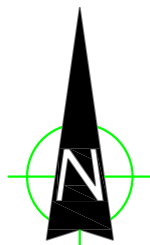
The Development Masterplan involves 5 stages and the proposed Ward Tower represents Stage 3 of that process and the Planning Proposal is submitted in the context of the Masterplan.

The purpose of this report is to:

- ❖ describe the existing hospital, the outstanding Consents, the Development and the Planning Proposal Masterplan
- ❖ describe the road network serving the site and the prevailing traffic conditions on that network
- ❖ assess the adequacy and appropriateness of the proposed parking provision
- ❖ assess the potential traffic implications of the proposed development
- ❖ assess the proposed vehicle access, internal circulation and servicing arrangements



LEGEND



LOCATION

FIG 1

2.0 Proposed Development

2.1 Site, Context and Existing Circumstances

The Lake Macquarie Private Hospital site (Figure 2) comprises a consolidation of lots which is located to the south of the Gateshead Centre with frontages to the Pacific Highway service road, Sydney Street, O'Brien Street and Casey Street. The elements comprise:

- ❖ the hospital complex is located on the northern side of Sydney Street
- ❖ the associated medical centre located on the southern side of Sydney Street (with an overhead pedestrian bridge link)
- ❖ the leased area for carparking on part of the school site with frontage to Hughes Street

The surrounding area comprises residential dwellings to the west of the Highway while the primary and high schools are located just to the south and there is a mixture of uses on the western side of the highway.

The existing Hospital comprises:

- ❖ Emergency Department, Theatres, Oncology Unit, ICU, Cath and Vascular labs
- ❖ 187 inpatient beds
- ❖ 239 staff (maximum daytime)
- ❖ 9 Doctors
- ❖ 33 VMO's

Staff and Doctors at the Hospital have a wide range of working hours as follows:

- Doctors (shifts) 8:00am – 4:30pm, 9:30am – 6:00pm and 5:00pm – 11:00pm
- Ward nurses 7:00am – 4:30pm, 1:30pm - 10:00pm and 9:30am – 7:30am
- Theatre staff 7:00am – 7:30pm
- Allied Health 8:00am – 5:00pm
- Ward clerks 7:00am – 3:30 pm and 4:00pm – Midnight.



LEGEND



SITE

FIG 2

The Emergency Department is open 24/7 while CSSD is generally open 4:00am to 2:00am.

The existing total carparking provision of 210 spaces comprises:

- ❖ 24 spaces in an open area on the north-eastern corner of the main hospital site
- ❖ 12 spaces along the southern side of the hospital
- ❖ 148 spaces on a leased area of the school to the south
- ❖ 18 spaces accessed on O'Brien Street
- ❖ 8 spaces accessed on Casey Street

There are a number of vehicle accesses provided including a porte cochere for setdown/pickup on Sydney Street.

2.2 Approved Development

Consent (DA2320/2017) has been granted for a new 18 bed ward, 16 space car park.

Consent (DA443/2018) has been granted for additional operating theatre and CSSD facilities which comprise:

- 2 new operating theatres with reception
- Patient recovery bays (9)
- Day surgery
- Ancillary facilities including:
 - X ray room
 - Offices and lifts
 - Staff amenities
 - Waiting areas
 - Coffee cart area
 - Corridors

2.3 Development Masterplan

The Development Masterplan involves 5 stages as follows:

Stage 1 and 2

These involve the works contained in the 2 existing consents being the new 18 bed ward (DA2320/2017) and the alteration/addition for the new operating theatres, patient recovery, day surgery and ancillary facilities (DA443/2018). The additional workers will comprise:

| Stage 1 | Stage 2 |
|--------------------|----------------------|
| 4 additional staff | 6 additional staff |
| | 6 additional doctors |

The provision of a 16-space car park was included in the Stage 1 approval however, these spaces will now be incorporated into the proposed expansion of the Hughes Street car park where there will be 44 additional spaces provided on the new Level 1.

Stage 3 (Ward Tower)

The new 9 level tower building will be provided on the northern part of the site with a porte cochere on the Casey Street frontage. There will be 3 levels of car parking and 2 “cold shell” levels with a back of house lower level containing loading docks. There will be 65 new ward beds (32 existing beds deleted) with 102 staff and 20 VMO’s with 120 new parking spaces will be provided in the Tower Building while 26 existing spaces will be deleted and the NE parking will be reduced from 24 spaces to 5 spaces.

Stage 4

This involves:

- Modification to the existing main entry
- New recovery lounge
- Hybrid OT Suite
- Emergency Department expansion
- Ambulance bays
- No increase to staff or doctors

Stage 5

This stage involves 3 new theatres, 49 ward beds, 665m² medical imaging and 10 consulting suites with 25 staff and 9 VMO's. The 2nd stage of the Hughes Street carpark expansion will add 103 spaces.

Details of the Masterplan scheme are provided on the plans prepared by Health Projects International which are reproduced in part in Appendix A.

2.4 Planning Proposal

The purpose of the Planning Proposal is to amend the building height restrictions to enable construction of the proposed 9 level Ward Tower.

3.0 Road Network and Traffic Conditions

3.1 Road Network

The existing road network serving the site (Figure 3) comprises:

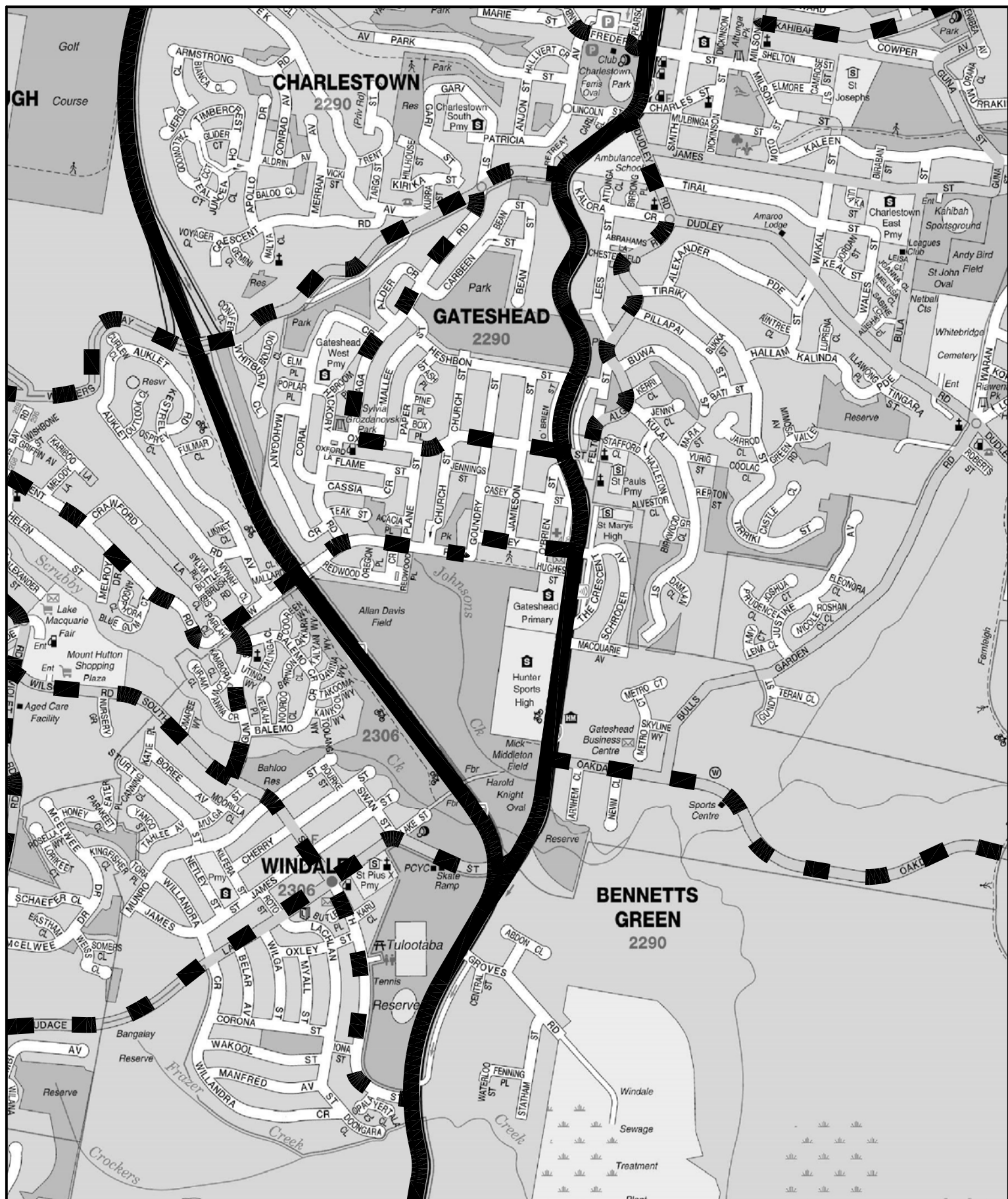
- ❖ *Pacific Highway* – a State Road and arterial route which connects between Sydney and Newcastle
- ❖ *Newcastle Inner City Bypass* – a State Road and arterial route which links between Windale and Kotara
- ❖ *Sydney Street, Willow Road and Tennent Road* – a collector route connecting between the Pacific Highway and Warners Bay Road.

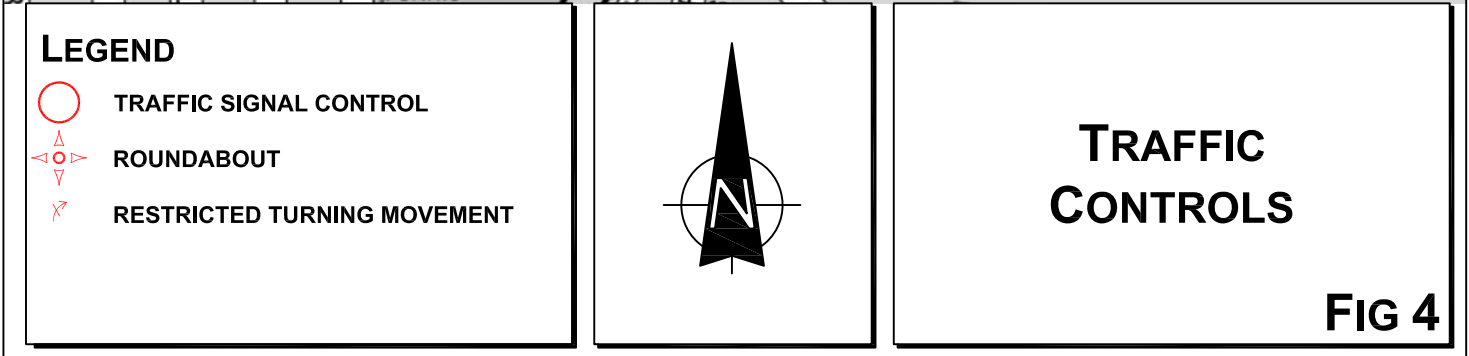
O'Brien Street, Hughes Street and Casey Street are local access roads which are relatively straight and level while there is a “service road” extending along the western side of the highway northwards from Sydney Road.

3.2 Traffic Controls

The traffic controls which have been applied to the road system in the vicinity of the site (Figure 4) include:

- ❖ the central median island along the highway which extends across the site frontage as well as the Hughes Street intersection
- ❖ the traffic control signals at the Pacific Highway and Sydney Street intersection
- ❖ the traffic signals at Pacific Highway and Oxford Street intersection
- ❖ the marked footcrossing on Sydney Street mid-way between the highway and O'Brien Street
- ❖ the 50 kmph speed limit on the local road system with section of 40 kmph in Sydney Street, O'Brien Street and Hughes Street and adjacent to schools





TRAFFIC CONTROLS

- ❖ the various GIVEWAY and STOP sign controls at intersections in the area
- ❖ the pedestrian refuge island in Sydney Street on the eastern side of O'Brien Street.

3.3 Traffic Conditions

An indication of the existing traffic conditions in the vicinity of the site is provided by data published¹ by TfNSW which is expressed in terms of Annual Average Daily Traffic (AADT). The latest recorded data indicates the following:

| | AADT |
|---------------------------------------|-------------|
| Pacific Highway south of Smart Street | 28,940 |

Collated traffic data includes SCATS data provided by TfNSW for the Pacific Highway and Sydney Street intersection (during the COVID pause in Feb 2020) traffic surveys undertaken in late October 2021 and earlier survey data for the morning and afternoon peak periods. This data has been combined with the highest movement recordings rounded off and is summarised in the following:

| | | AM | PM |
|-----------------|------------|-----------|-----------|
| Pacific Highway | Northbound | 1,320 | 880 |
| | Right-turn | 50 | 50 |
| | Left-turn | 80 | 120 |
| | Southbound | 610 | 1,410 |
| | Right-turn | 90 | 60 |
| | Left-turn | 28 | 30 |
| Sydney Street | Eastbound | 10 | 20 |
| | Right-turn | 120 | 130 |
| | Left-turn | 54 | 61 |
| The Crescent | Westbound | 10 | 10 |
| | Right-turn | 20 | 10 |
| | Left-turn | 15 | 15 |

¹ *Traffic Volume Data for Northern Region
Roads and Maritime Services*

A SIDRA analysis of the existing operational performance of the intersection has been undertaken and the results indicating a satisfactory performance are provided in Appendix D and summarised in the following:

| | AM | PM |
|------------|-----------|-----------|
| LOS | C | 39.3 |
| AVD | D | 43.0 |

Observations also confirm that the operation of this intersection is quite satisfactory even in the peak periods with no extensive or residual queuing apparent. Traffic conditions in the area are generally quite satisfactory with the traffic signal controlled intersections and central median island along the highway route.

3.4 Transport Services

Public transport services for the Hospital are provided by the Bus Route 14 which provides frequent 7 days per week services along the Highway between Newcastle and Belmont and Route 41 which operates as a regular service along Oxford Street (and the Highway). There is also an “on-demand” 7 days per week service provided for the Lake Macquarie area.

Details of these services are provided in Appendix E, indicating the location of the Route 14 bus stops adjacent to the Hospital and the times tables.

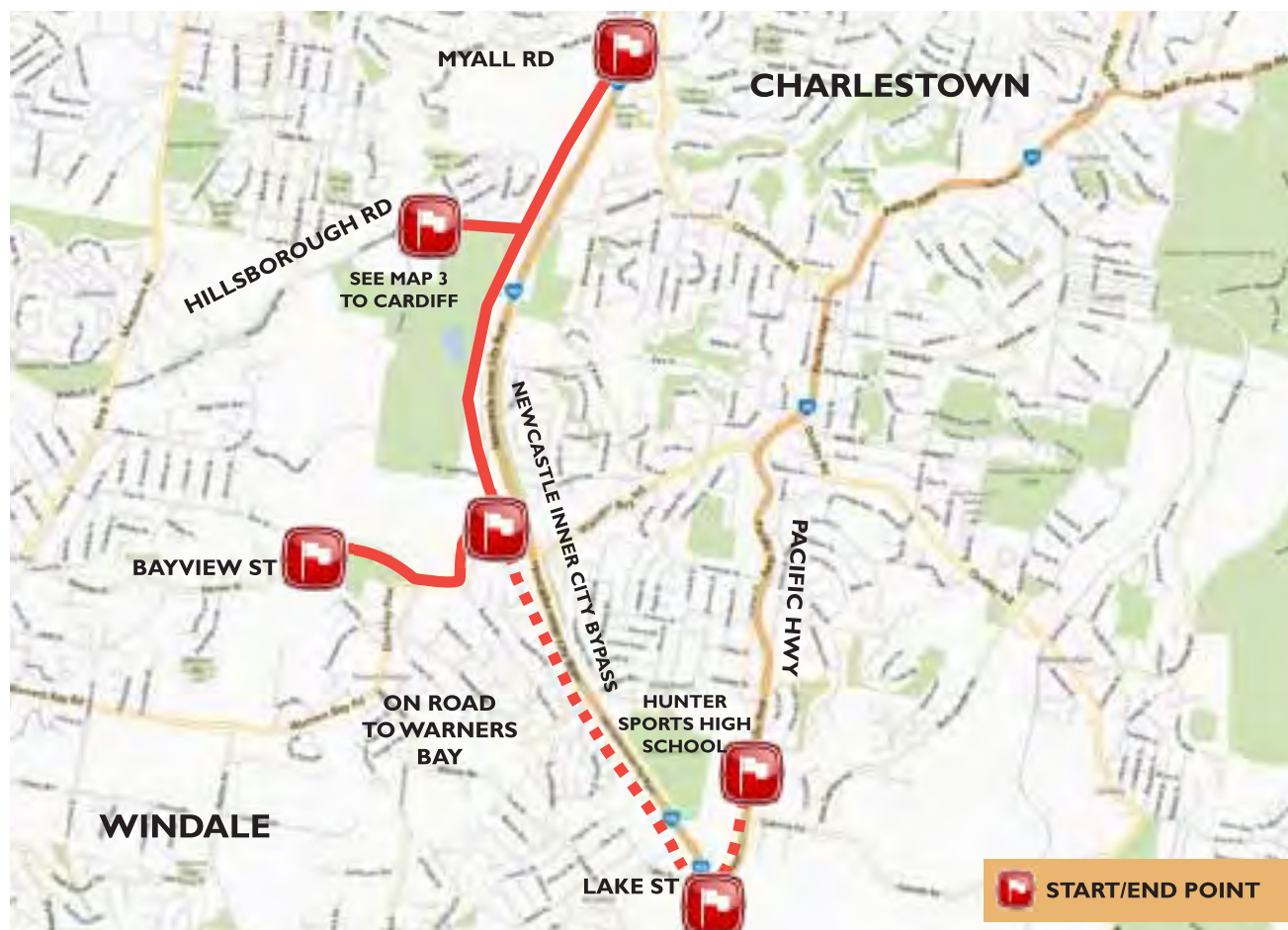
3.5 Bicycles and Pedestrians

Pedestrian facilities at the site include:

- over bridge connection to the Medical Centre
- marked footcrossing across Sydney Street
- foot paths along the highway, Sydney Street and Casey Street
- traffic signal controlled crossings at the Pacific Highway/Sydney Street intersection

Provision for cyclists is made by the shared path along the highway providing connection to the Newcastle Cycle Network (see details overleaf).

Map 5. Charlestown to Windale



This shared pathway is an ideal link between schools and the residential community, with a safe bridge crossing over the busy Newcastle Inner City Bypass. It is also a handy access way towards Warners Bay.

Location: Warners bay Road to Hunter Sports High,
Pacific Highway, Gateshead (or reverse)

Type: Linear

Distance: 2.5km

Grade: Easy to moderate

Facilities: Sportsground, club, shops

Access: Park Avenue near the Nereida
Close intersection

Information: Extensions of this track will access
Mount Hutton and Warners Bay
shopping areas



Windale overpass

MAP 2: PRINCIPAL BICYCLE NETWORK



*Refer to City of Newcastle's Cycling Strategy

Appendix 1 provides more detail on Principal Bicycle Network routes.



4.0 Parking

Lake Macquarie City Council's DCP specifies the following parking requirements in relation to the elements of the Masterplan development:

| Hospital | Day Surgery | Health Consulting Rooms |
|--------------------------|----------------------------------|----------------------------------|
| 1 space per 2 beds | 1 space per practitioner | 1 space per on-duty practitioner |
| plus 1 space per 2 staff | 1 space per 2 staff | 1 space per 2 full-time staff |
| plus Ambulance space | 1 space per 2 operating theatres | 2 spaces per consulting room |

The existing hospital therefore has a parking requirement as follows:

| | |
|---------------|---------------------------|
| 187 beds | 93.5 spaces |
| 251 staff | 125.5 spaces |
| 9 doctors | 9 spaces |
| 33 VMO's * | 16.5 spaces |
| TOTAL: | 244.5 spaces (246) |

** VMO's (Visiting Medical Officers) are only on-site part time and generally about 50% at one time.*

The existing parking provision comprises:

- 24 spaces in NE carpark
- 12 spaces along south side
- 148 spaces in the Hughes Street carpark
- 8 spaces accessed on Casey Street
- 18 spaces accessed on O'Brien Street

Total 210 spaces (36 space shortfall)

The proposed progressive provision of parking relative to the development stages is as follows:

| | |
|-------------------------|---|
| Stages 1 & 2 | Required |
| 18 beds | - 9 spaces |
| 4 staff | - 2 spaces |
| 6 Staff | - 3 spaces |
| 6 Doctors | - 6 spaces |
| Total | 20 spaces |
| Total Required | 266 spaces (246 + 20) |
| Existing | 210 spaces |
| Added | 44 spaces (Hughes Street) |
| Total | 254 spaces (Shortfall 12 spaces) |
| Stages 3 & 4 | |
| 102 Staff | 51 spaces |
| 20 VMO's | 10 spaces |
| 33 Beds | 16.5 spaces |
| Total | 76.5 spaces (77) |
| Total Required: | 343 spaces |
| Lose | 19 spaces (NE) |
| Lose | 26 spaces (Casey Street/O'Brien Street) |
| Added | 120 Spaces (Casey Street) |
| Total | 329 spaces (Shortfall 14 spaces) |
| Stage 5 | |
| 49 Beds | 24.5 spaces |
| 25 Staff | 12.5 spaces |
| 9 VMO's | 4.5 spaces |
| 3 Theatres | 1.5 spaces |
| Total | 43 spaces |
| Total Required: | 386 spaces |
| Added | 103 spaces (Hughes Street) |
| Total | 432 spaces (Excess 46 spaces) |

Consulting Suites

The proposed Medical Suites will not generally be occupied on a full-time basis as many of the practitioners will have rooms at one or more other locations. Say the concurrent occupancy is 70%, with 1 practitioner in each and 1 staff:

10 Practitioners - 10 spaces

10 staff - 5 spaces

Patients - 20 spaces

Sub-Total: 35 spaces x 70%

Total: 25 spaces

Total Required: 411 spaces (excess 21 spaces)

It is apparent that the proposed total parking provision will be quite adequate for the proposed development under the Masterplan and that the existing shortfall will be eliminated with the Stage 2 works.

5.0 Traffic

The RTA Guide to Traffic Generating Development provides traffic generation criteria in relation to Private Hospitals however, a review of the sites surveyed for that 1994 study revealed that they had very little in common with LMPH.

In 2013, RMS commissioned a consultant study² to update the Guidelines in relation to the parking and traffic generation characteristics of Major Hospitals. This study involved the surveys of sites which were split into 2 categories “Metropolitan Area Hospitals” with a high level of public transport accessibility and “Metropolitan and Regional Hospitals” with low public transport accessibility (e.g. including Sydney Adventist, John Hunter, Lismore and Blacktown hospitals).

For the latter, the traffic generation in the AM and PM peak periods:

- vtpm per staff
- vtpm per bed

The following peak traffic generation models were recommended for the hospitals which reflect the LMPH characteristics:

$$\text{AM} - 0.41 \times \text{Staff} + 0.62 \text{ Beds}$$

$$\text{PM} - 0.59 \times \text{Staff} + 0.05 \text{ Beds}$$

Accordingly, the assessed peak traffic generation of the existing LMPH is as follows:

$$\text{AM} - 0.41 \times 239 + 0.62 \times 187 = 236 \text{ vtpm}$$

$$\text{PM} - 0.59 \times 239 + 0.05 \times 187 = 182 \text{ vtpm}$$

² *Traffic Generation & Parking Analysis
For Major Hospitals
URAP for RMS, Sept 2013*

On this same basis, the assessed peak traffic generation for the Stage 3 and Stage 5 completed Masterplan development circumstances are as follows:

Stage 3

$$\text{AM} - 0.41 \times 415 + 0.62 \times 238 = 318 \text{ vtpH}$$

$$\text{PM} - 0.59 \times 415 + 0.05 \times 238 = 257 \text{ vtpH}$$

Stage 5

$$\text{AM} - 0.41 \times 449 + 0.62 \times 287 = 362 \text{ vtpH (+126)}$$

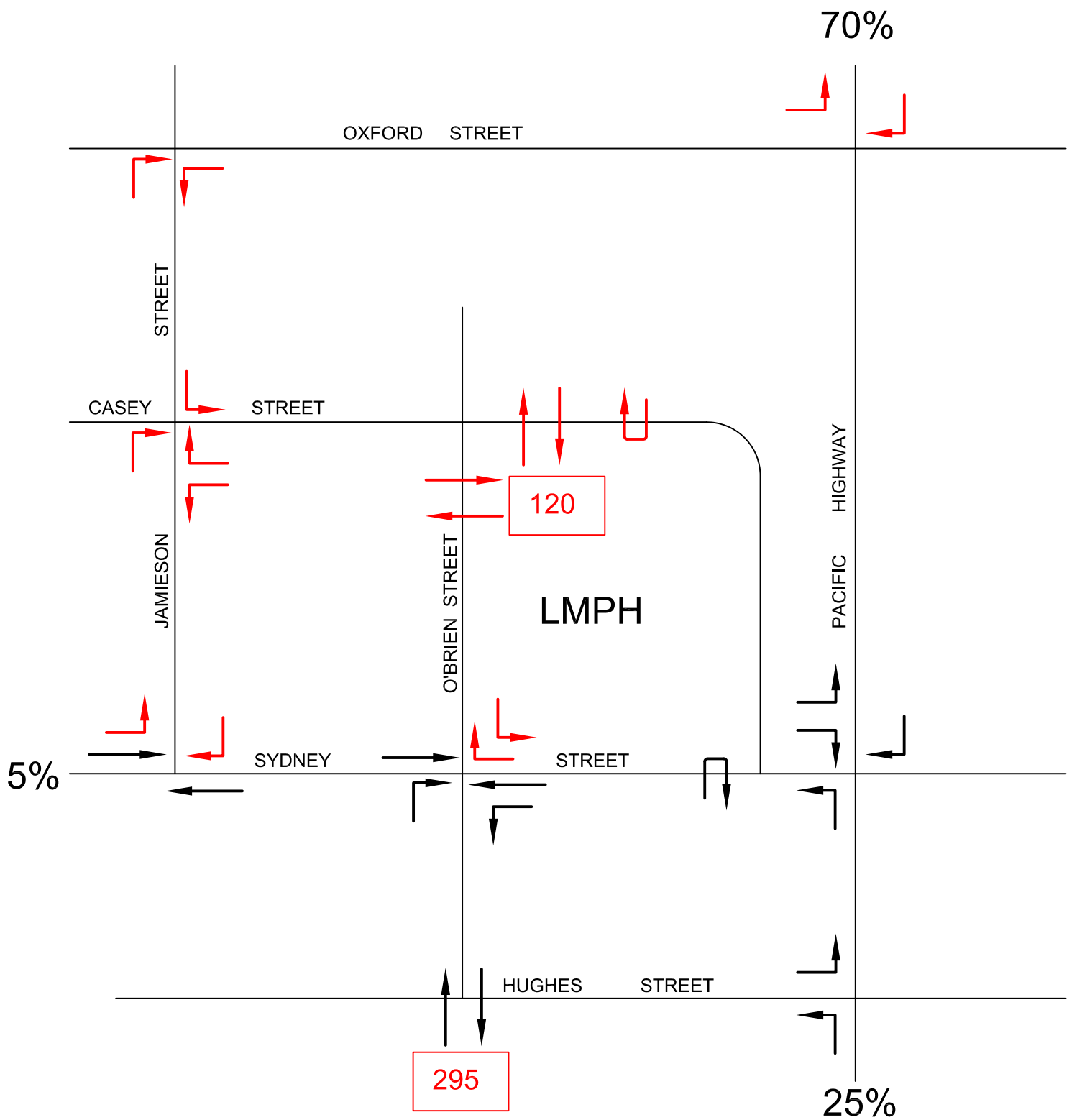
$$\text{PM} - 0.59 \times 449 + 0.05 \times 287 = 280 \text{ vtpH (+98)}$$

The approach and departure vehicle movements for the hospital will become more diverse as the development stages progress principally as a result of the advent of the Casey Street car park and porte cochere. This will result in vehicles approaching and departing the Highway via Oxford Street as indicated on Figure 5.

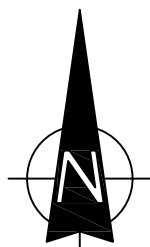
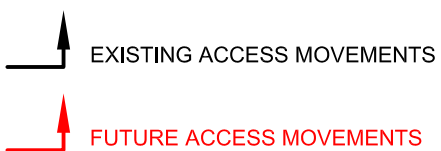
The additional movements via Oxford Street will however be relatively minor being largely comprised of vehicle movements to/from the north related to the new Casey Street car park (120 cars) and the adjacent porte cochere which will be secondary to the main Sydney Street porte cochere (and the generated movements will be no more than that of the existing porte cochere).

Surveys of the existing Hughes Street car park and Sydney Street porte cochere (see Appendix C) reveal the following peak traffic movements (vtpH):

| | AM | | PM | |
|-----------------------|----|-----|----|-----|
| | IN | OUT | IN | OUT |
| Car park (148 spaces) | 56 | 1 | 1 | 52 |
| Porte Cochere | 11 | 11 | 8 | 7 |



LEGEND



HOSPITAL ACCESS MOVEMENTS

FIG 5

This indicates that some 36% of parking spaces result in vt's during the 1 hour AM and PM peak periods. The enlarged carpark will have 295 spaces and the following traffic generation is indicated:

| | AM | | PM | |
|--------------------------|-----|-----|----|-----|
| | IN | OUT | IN | OUT |
| Hughes Street 295 spaces | 112 | 6 | 6 | 104 |
| Casey Street 120 spaces | 40 | 3 | 3 | 40 |

Some 70% of generated vehicle movements will be to/from the north along the Highway with some 25% to/from the south and 5% to/from the west. Cars from the north will approach the Hughes Street car park by turning right from the highway into Sydney Street and depart by turning left from Hughes Street to the highway.

Cars from the south will approach the Hughes Street car park by turning left from the highway into Hughes Street and depart by turning right from Sydney Street to the Highway.

Cars from the north approaching the Casey Street car park will turn right from the highway into Oxford Street and depart by turning left from Oxford Street to the highway. Cars from the south approaching the Casey Street car park will turn left from the highway into Sydney Street (or Hughes Street) and depart by right turn from Sydney Street to the highway.

Movements associated with the 2 porte cocheres will be quite minor at some 20 to 30 vtph in the AM and PM peak periods. Thus, the principal additional peak traffic movements resultant to the proposed expansion of LMPH will be at the Pacific Highway and Sydney Street intersection while the highest movement increase at the Pacific Highway and Oxford Street intersection will only be some 30 vtph (i.e. right turn into Oxford Street in the AM peak and left turn to the highway in the PM peak).

The projected future peak traffic movements at the Pacific Highway and Sydney Street intersection are as follows:

| | | AM | PM |
|-----------------|------------|-----------|-----------|
| Pacific Highway | Northbound | 1,320 | 880 |
| | Right-turn | 50 | 50 |
| | Left-turn | 120 | 130 |
| | Southbound | 610 | 1,410 |
| | Right-turn | 130 | 80 |
| | Left-turn | 28 | 30 |
| Sydney Street | Eastbound | 10 | 20 |
| | Right-turn | 130 | 154 |
| | Left-turn | 65 | 80 |
| The Crescent | Westbound | 10 | 10 |
| | Right-turn | 20 | 10 |
| | Left-turn | 15 | 15 |

The operational performance of this intersection with the projected additional traffic volumes has been modelled with SIDRA and the results are provided in Appendix D and summarised in the following:

| AM | | PM | |
|------------|------------|------------|------------|
| LOS | AVD | LOS | AVD |
| C | 41.8 | D | 44.5 |

These results indicate that this intersection will continue to operate satisfactorily during the peak traffic periods.

6.0 Access, Internal Circulation and Servicing

6.1 Access

The proposed new and changed vehicle access arrangements are as follows:

- **Sydney Street Porte Cochere**

The existing egress to Sydney Street is deleted and egress is to the highway service road.

- **Casey Street Porte Cochere**

Sperate ingress and egress driveways are provided just to the west of the highway service road where good sight distances are available.

- **Casey Street Car Park**

Combined ingress/egress driveways are provided on Casey Street and O'Brien Street where good sight distances are available.

- **Ambulance Facility**

A wide driveway is provided on the highway service road to enable 3 ambulances to access independently. Good sight distances are available at this location.

- **Loading dock**

A wide access driveway is provided on the highway service road just to the south of Casey Street to enable 2 trucks to independently access the loading dock.

Good sight distances are available at this location.

- **Hughes Street Car Park**

A new combined ingress/egress driveway will be provided on the School access roadway just to the north of the existing access driveway where good sight distances are available.

6.2 Internal Circulation

The design of the internal circulation arrangements for the various car park areas complies with the requirements of AS 2890.1 & 6 including ramps, grades, bays, aisles, turning/manoeuvring and head room etc.

6.3 Servicing

Apart from the ambulance facility, delivery and service vehicles will utilise the 2 bay loading dock on the highway service road frontage although small vehicles (e.g. pathology pick up and urgent blood delivery) will be able to use the available short term parking spaces.

The loading dock will accommodate trucks up to 14.5m semi-trailer and details of the turning path assessment for these trucks are provided in Appendix F.

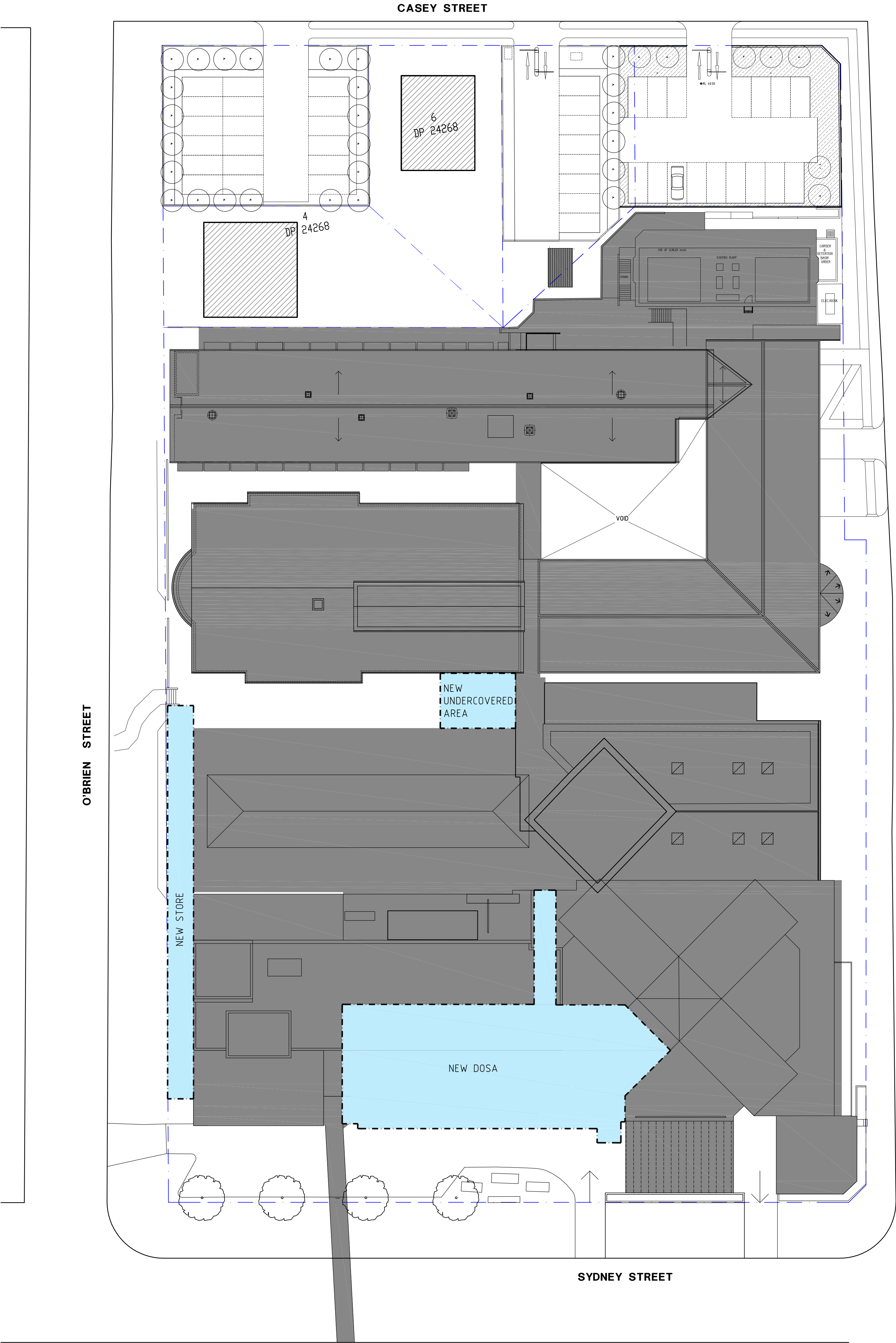
7.0 Conclusion

The proposed Development Masterplan for Lake Macquarie Private Hospital includes a Planning Proposal to permit the height of the proposed Ward Tower. This assessment has concluded that the proposed development:

- ❖ will not result in any adverse traffic implications
- ❖ will provide adequate and appropriate car parking
- ❖ will make suitable provision for vehicle access, internal circulation and servicing.

Appendix A

Approved Plans



LEGEND:

WORK IN ADDITION TO EXISTING FOOTPRINT

EXISTING BUILDING

SITE BOUNDARY

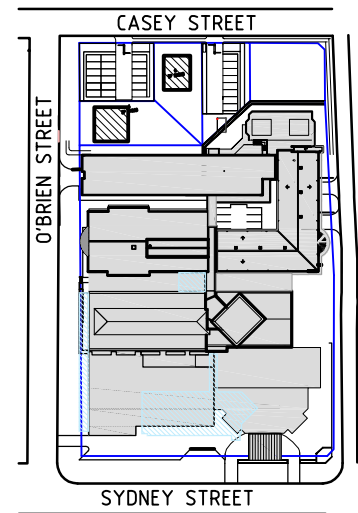
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Project
**PRIVATE HOSPITAL
LAKE MACQUARIE**

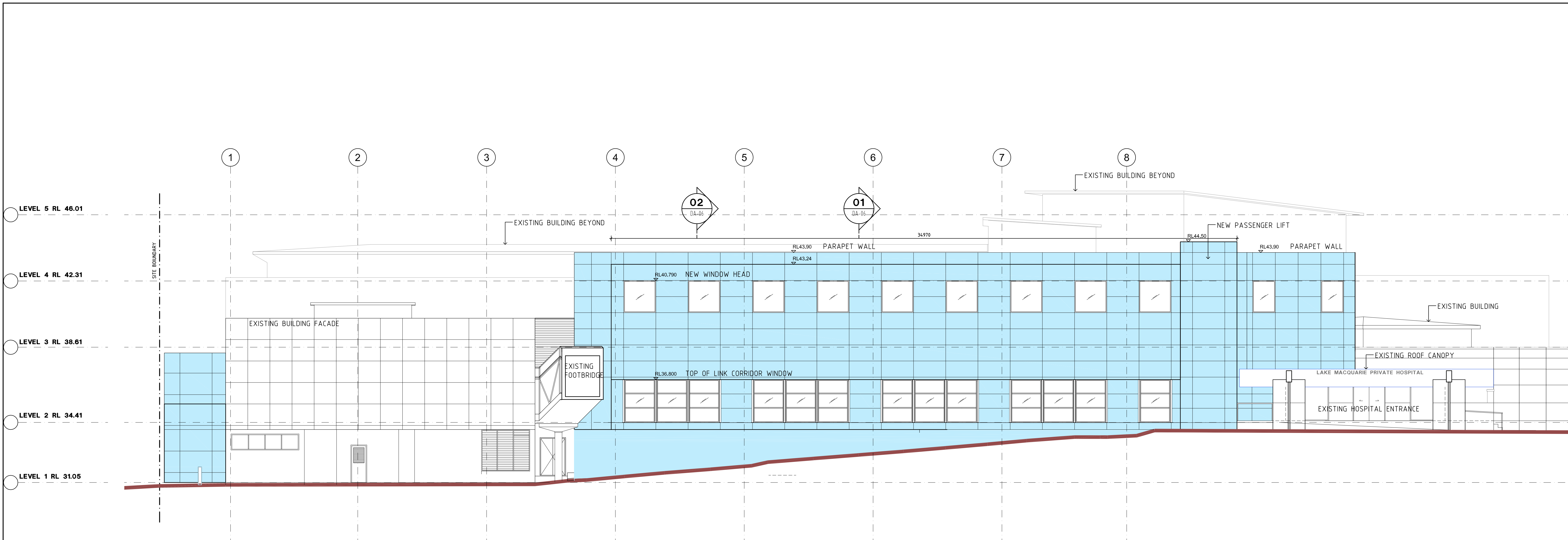
Principal
**RAMSAY HEALTH CARE
PTY LIMITED** ACN 003 184 889



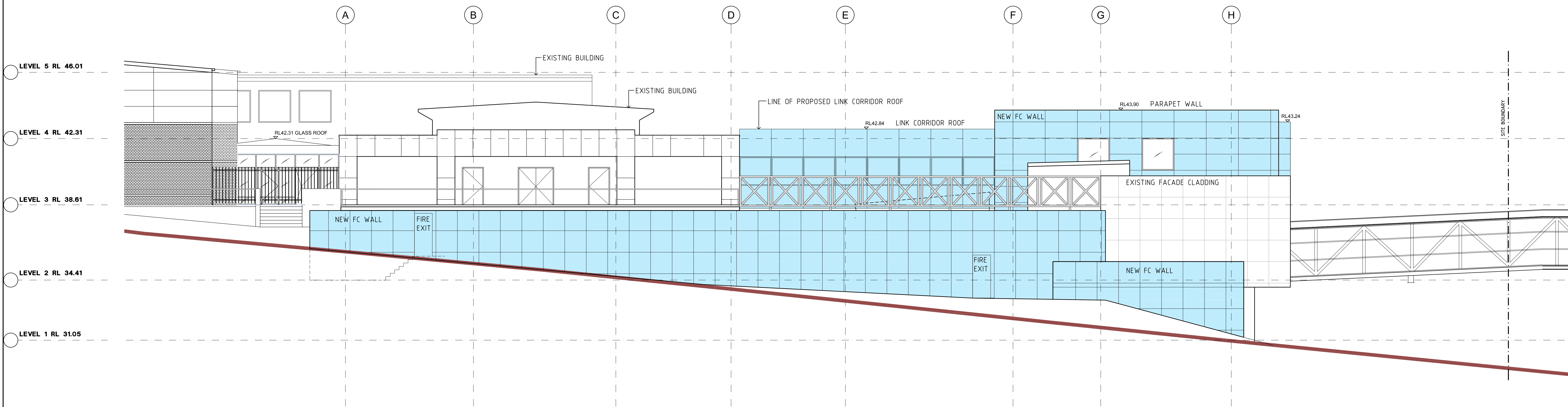
HPI HEALTH PROJECTS INTERNATIONAL
Architects and Health Facility Planners
ACN 060 606 985
Ground Floor Suite 1, 68 Alfred St., Morningside QLD 4017
Ph: (02) 9460 4199 Fax: (02) 9460 4299



KEY PLAN



01 - SYDNEY STREET ELEVATION



02 - O'BRIEN STREET ELEVATION

LEGEND:

- EXISTING BUILDING
- WORK IN ADDITION TO EXISTING FOOTPRINT

| REV | REVISION DESCRIPTION | DATE | BY |
|-----|----------------------|----------|----|
| 1 | FIRST ISSUE | 01/03/18 | CX |

Project: **PRIVATE HOSPITAL LAKE MACQUARIE**

Principal: **RAMSAY HEALTH CARE PTY LIMITED** ACN 003 184 889

Principal: **HEALTH PROJECTS INTERNATIONAL** Architects and Health Facility Planners ACN 000 606 985
Ground Floor Suite 1, 68 Alfred St, Morningside QLD 4017
Ph: (02) 9460 4199 Fax: (02) 9460 4299

KEY PLAN

USE FIGURED DIMENSIONS ONLY. DO NOT SCALE. ALL DIMENSIONS SHALL BE VERIFIED ON SITE AND DISCREPANCIES IMMEDIATELY BROUGHT TO THE ATTENTION OF THE PROJECT MANAGER FOR RESOLUTION.

"CLOUDS" & REVISIONS ARE INTENDED AS GUIDES AND DO NOT NECESSARILY DESCRIBE THE FULL EXTENT OF REVISIONS. ASCERTAIN FULL EXTENT BY COMPARISON WITH PREVIOUS VERSION.

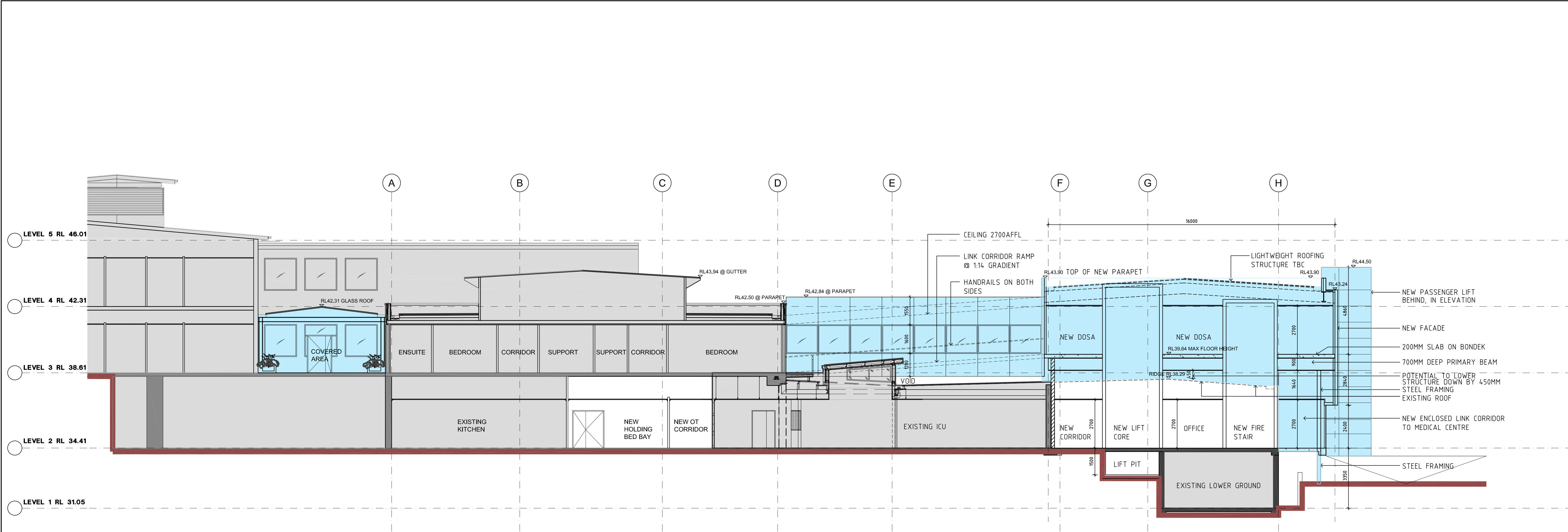
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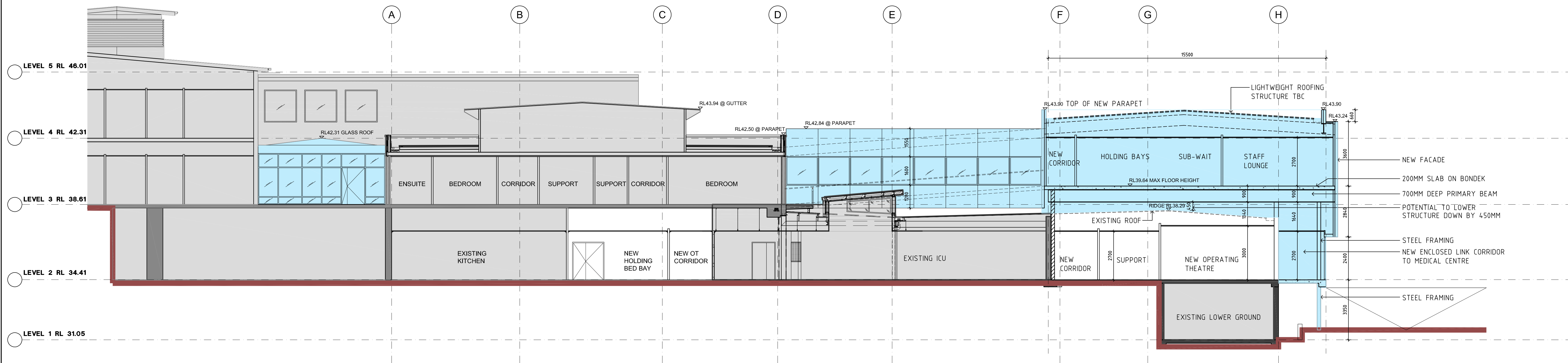
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Reason for Issue: **DA SUBMISSION**

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01 - SECTION THROUGH LIFT AND STAIR CORES

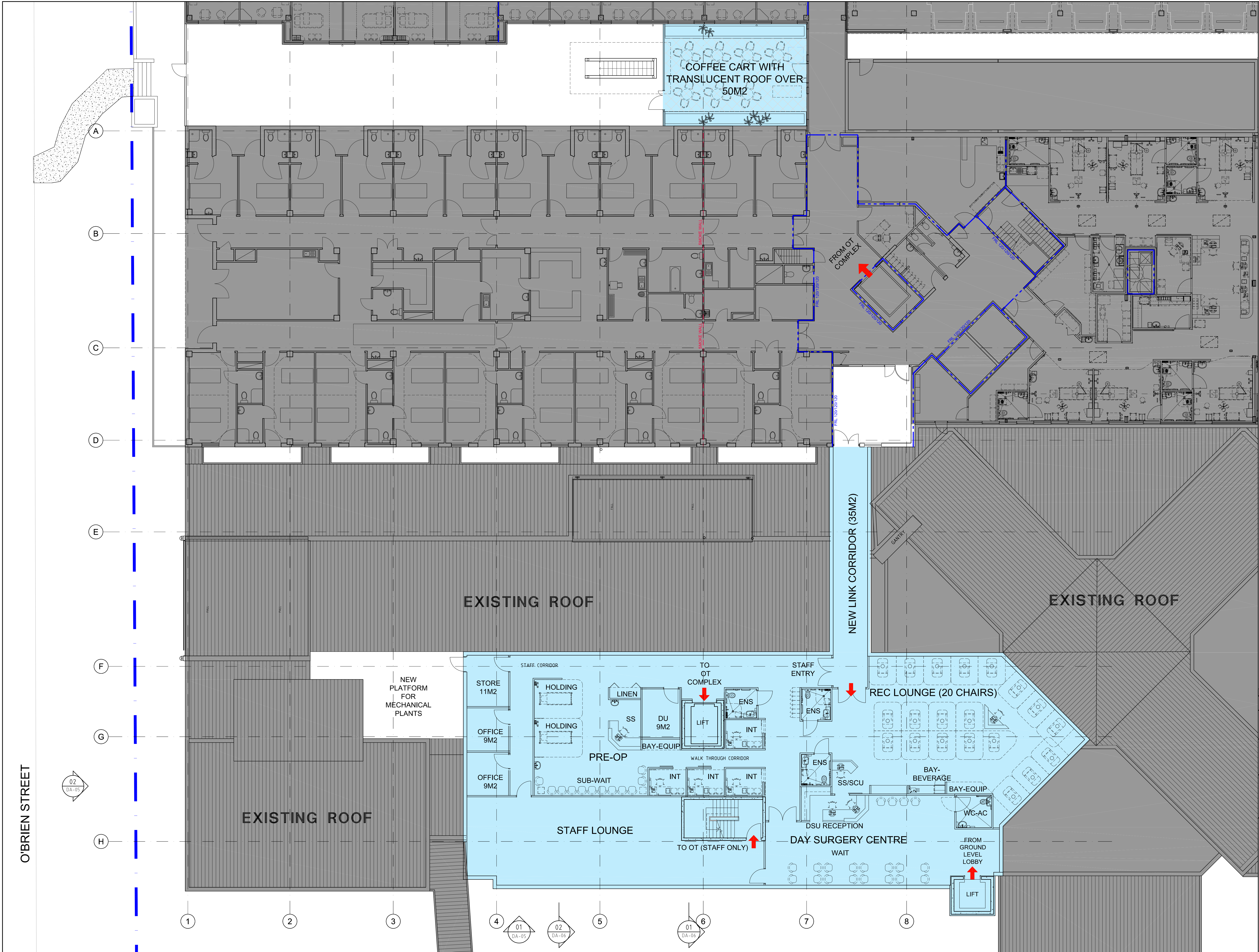


02 - SECTION THROUGH OPERATING THEATRE

LEGEND:

- WORK IN EXISTING FOOTPRINT
- WORK IN ADDITION TO EXISTING FOOTPRINT
- EXISTING BUILDING

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| PRIVATE HOSPITAL LAKE MACQUARIE | | | |
| Principal RAMSAY HEALTH CARE PTY LIMITED ACN 003 184 889 | | | |
| Principal HEALTH PROJECTS INTERNATIONAL Architects and Health Facility Planners ACN 000 606 985 Ground Floor Suite 1, 68 Alfred St, Moore Park 2001 Ph: (02) 9460 4199 Fax: (02) 9460 4299 | | | |
| KEY PLAN | | | |
| | | | |
| Reason for issue DA SUBMISSION | | | |
| CAD File LMPH14-DA-06 | | | |
| Dwg No. LMPH14-DA-06 | | | |
| Issue 1 | | | |



LEGEND:

- WORK IN EXISTING FOOTPRINT
- WORK IN ADDITION TO EXISTING FOOTPRINT
- EXISTING BUILDING
- SITE BOUNDARY
- SMOKE WALL
- SMOKE COMPARTMENT WALL
- 60/60/60 FIRE RATED WALL
- 120/120/120 FIRE RATED WALL

| | | | |
|---|----------------------|--------|----|
| 1 | FIRST ISSUE | 010318 | CX |
| REV | REVISION DESCRIPTION | DATE | BY |
| Project | | | |
| LAKE MACQUARIE PRIVATE HOSPITAL | | | |
| Principal RAMSAY HEALTH CARE PTY LIMITED ACN 003 184 889 | | | |
| HP HEALTH PROJECTS INTERNATIONAL Architects and Health Facility Planners ACN 000 606 985 Ground Floor Suite 1, 68 Alfred St, Moore Park 2001 Ph: (02) 9460 4199 Fax: (02) 9460 4299 | | | |
| | | | |
| KEY PLAN | | | |

USE FIGURED DIMENSIONS ONLY. DO NOT SCALE. ALL DIMENSIONS SHALL BE VERIFIED ON SITE AND DISCREPANCIES IMMEDIATELY BROUGHT TO THE ATTENTION OF THE PROJECT MANAGER FOR RESOLUTION.

"CLOUDS" & REVISIONS ARE INTENDED AS GUIDES AND DO NOT NECESSARILY DESCRIBE THE FULL EXTENT OF REVISIONS. ASCERTAIN FULL EXTENT BY COMPARISON WITH PREVIOUS VERSION.

| | | | | | | | | |
|-----------------|-----------------|-----------------|-------------|-------|---------|----------|---------|------------------|
| Subject By Date | Subject By Date | Subject By Date | Block/ Zone | Drawn | Checked | Date | Scale/s | Reason for Issue |
| RDS | STRUC | PROJ | --- | CX | HST | 01.03.18 | 1:100 | DA SUBMISSION |
| ARCH | SPEC | ARCH | | | | | | |
| AUT | CONC | SERV | | | | | | |

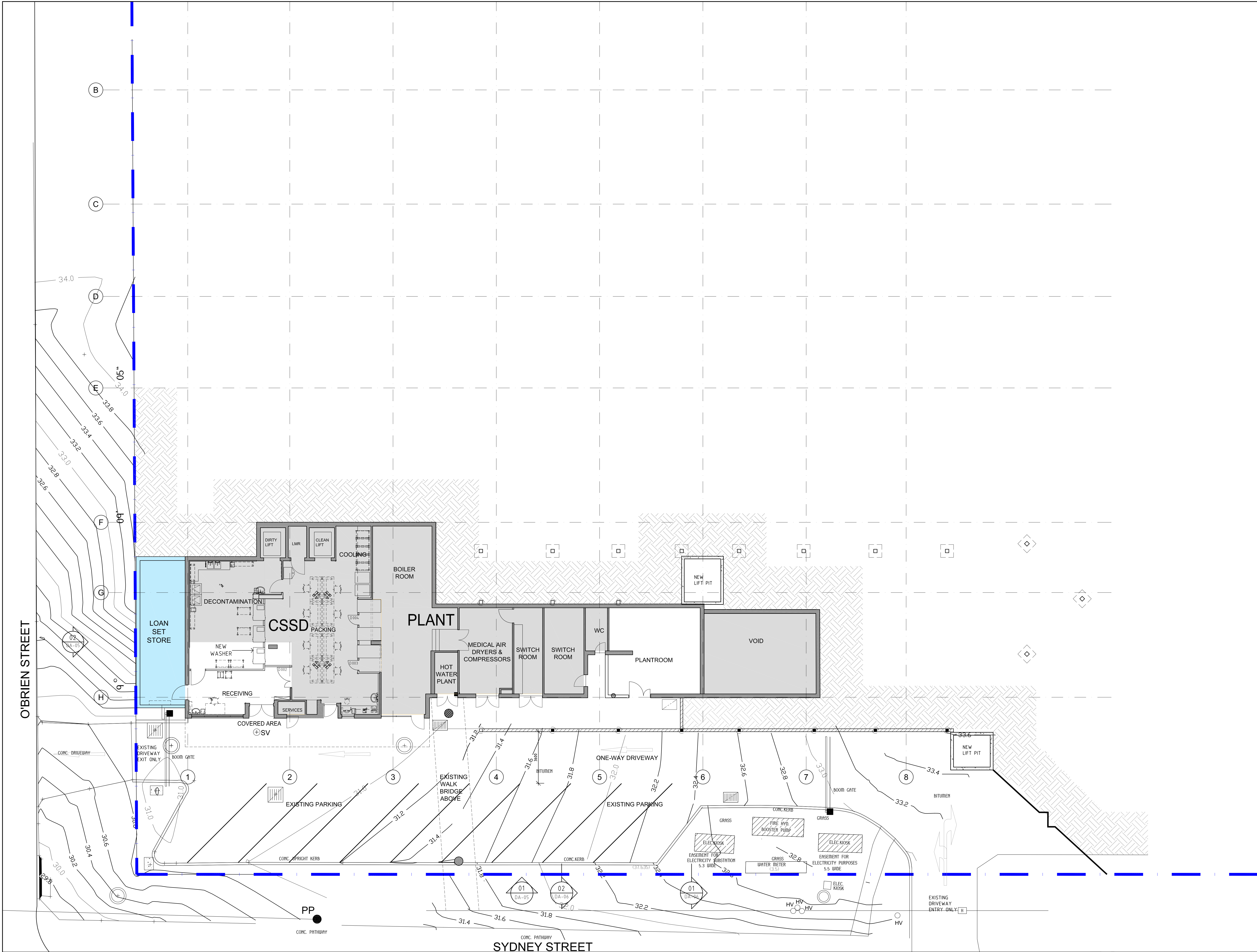
Q4 CHECK

Drawing Title
PLAN - LEVEL 1

CAD File
LMPH14-DA-04

Dwg No.
LMPH14-DA-04

Issue
1



LEGEND:

- WORK IN EXISTING FOOTPRINT
- WORK IN ADDITION TO EXISTING FOOTPRINT
- EXISTING BUILDING
- SITE BOUNDARY
- SMOKE COMPARTMENT WALL
- 60/60/60 FIRE RATED WALL
- 120/120/120 FIRE RATED WALL

| | | | |
|---|----------------------|--------|----|
| 1 | FIRST ISSUE | 010318 | CX |
| REV | REVISION DESCRIPTION | DATE | BY |
| Project | | | |
| LAKE MACQUARIE PRIVATE HOSPITAL | | | |
| Principal RAMSAY HEALTH CARE PTY LIMITED ACN 003 184 889 | | | |
| Principal HEALTH PROJECTS INTERNATIONAL Architects and Health Facility Planners ACN 000 606 985 Ground Floor Suite 1, 68 Alfred St., Morningside QLD 4017 Ph: (02) 9460 4199 Fax: (02) 9460 4299 | | | |
| | | | |
| KEY PLAN | | | |

QA
CHECK

| | | | |
|-----------------|-----------------|-----------------|-------------|
| Subject By Date | Subject By Date | Subject By Date | Block/ Zone |
| RDS | STRUCT | PROJ ARCH | -- |
| ARCH | SPEC CONC | | |
| AUT | SERV | | |

Drawing Title

PLAN - LOWER GROUND

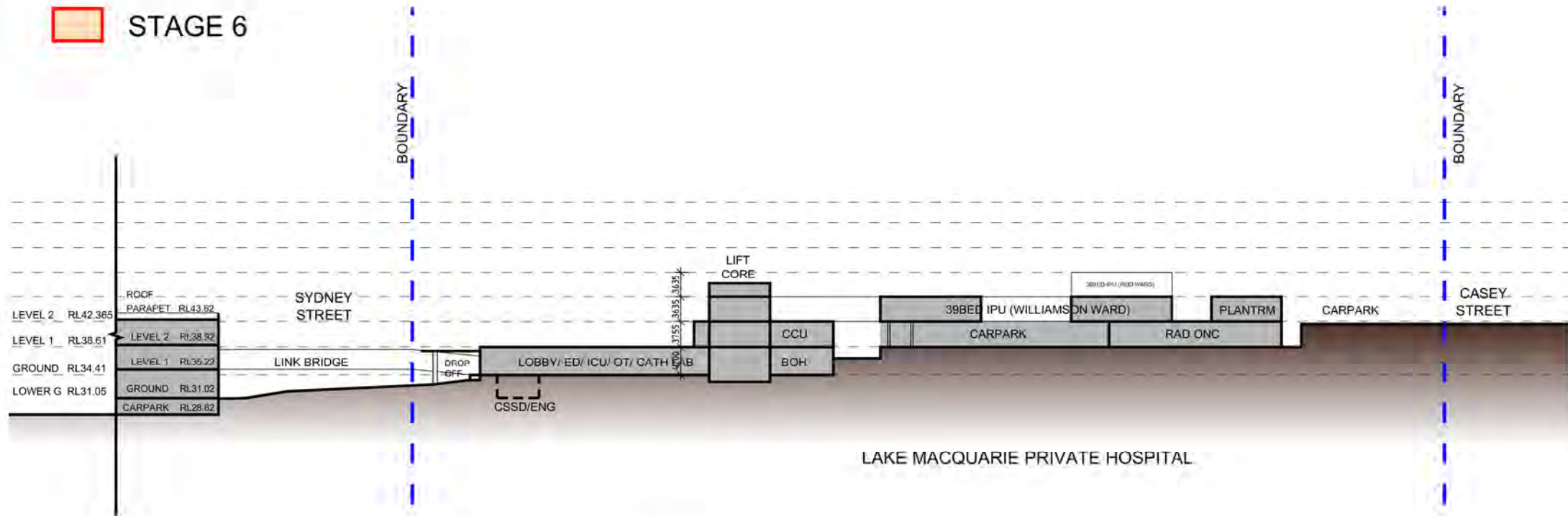
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| Drawn CX | Checked HST | Date 01.03.18 | Scale/s 1:100 |
| Reason for Issue | | | |
| DA SUBMISSION | | | |
| CAD File LMPH14-DA-02 | Dwg No. LMPH14-DA-02 | Issue 1 | |

Appendix B

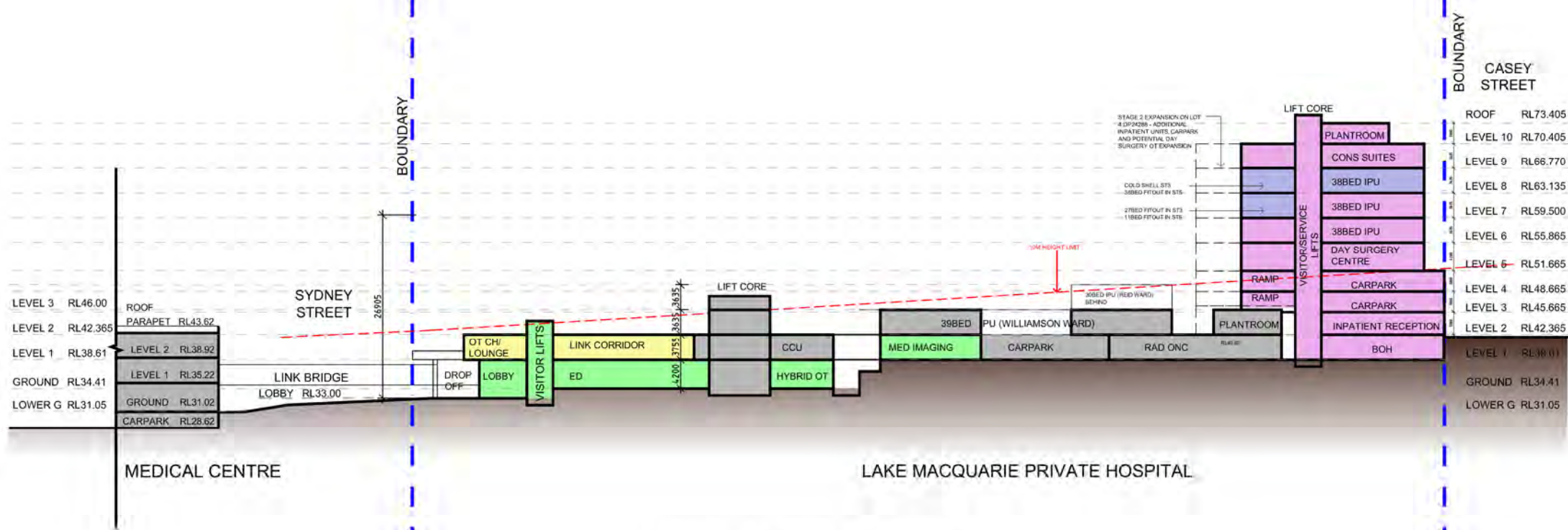
Concept Plans

LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6



CONCEPTUAL SECTION - EXISTING

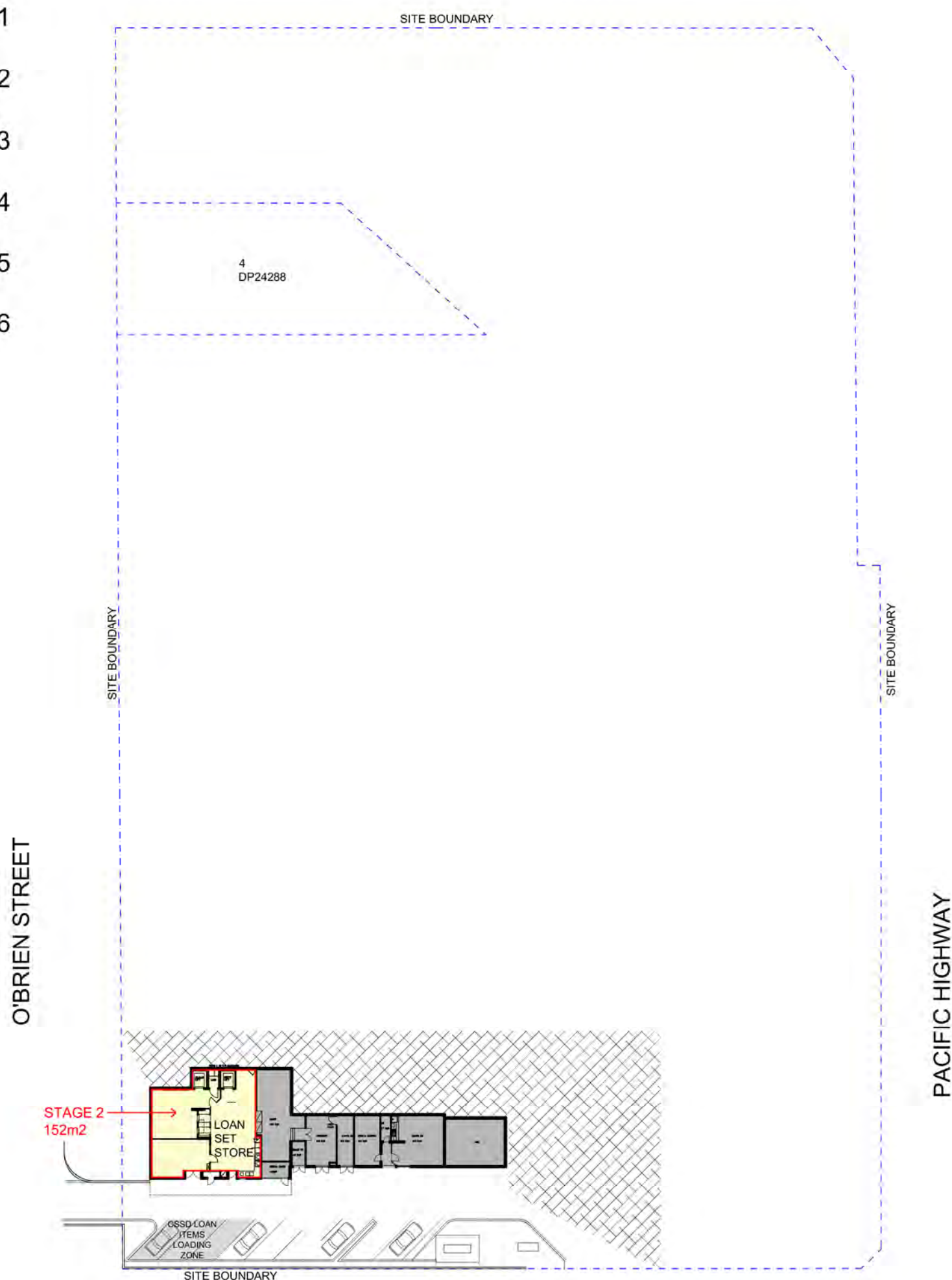


CONCEPTUAL SECTION - PROPOSED

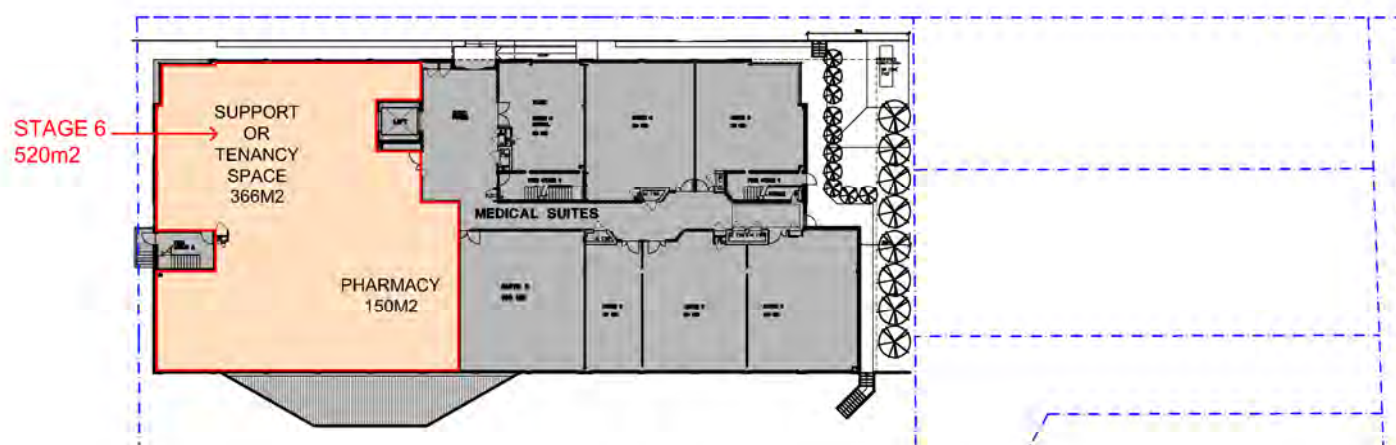
LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6

CASEY STREET



SYDNEY STREET



HUGHES STREET

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LAKE MACQUARIE PRIVATE HOSPITAL MASTERPLAN

LOWER GROUND LEVEL STAGING PLAN - **OPTION 16**

0 5 10 15 20

SCALE 1:600 @ A3

LMPH17-STAGING-1

ISSUE 4 2 October 2021



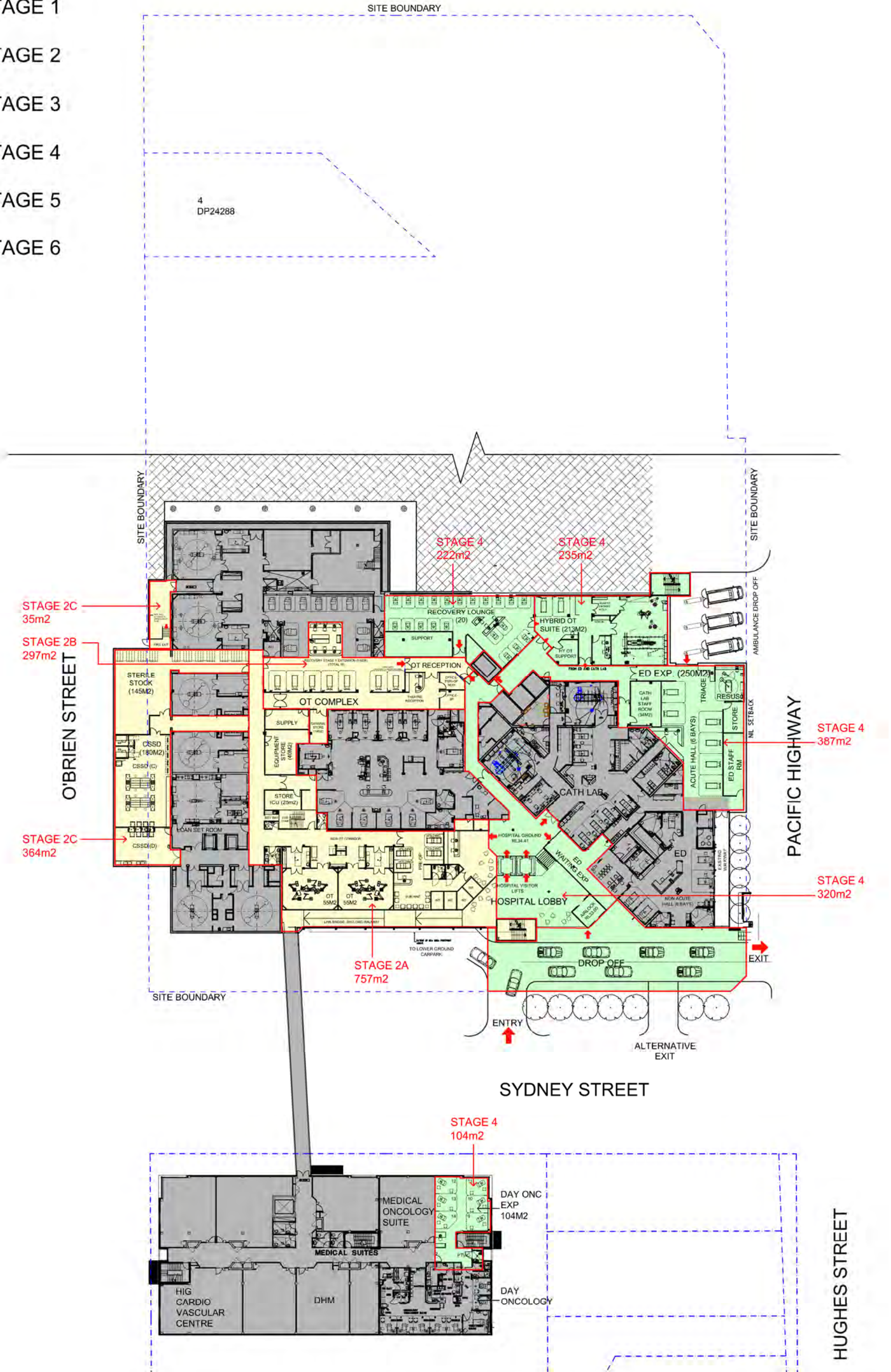
ARCHITECTS AND HEALTH FACILITY PLANNERS



CASEY STREET

LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6



LAKE MACQUARIE PRIVATE HOSPITAL MASTERPLAN

GROUND LEVEL STAGING PLAN - OPTION 16

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0 5 10 15 20

SCALE 1:600 @ A3

LMPH17-STAGING-2

ISSUE 4 2 October 2021



ARCHITECTS AND HEALTH FACILITY PLANNERS



CASEY STREET

LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6

O'BRIEN STREET

STAGE 4
133m²

STAGE 5
760m²

STAGE 4
23m²

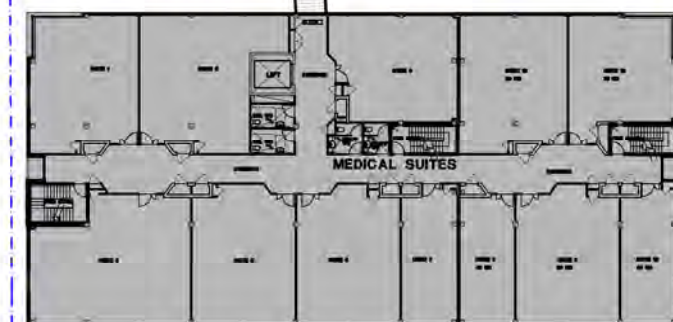
PACIFIC HIGHWAY

STAGE 2
568m²

STAGE 4
302m²

SYDNEY STREET

HUGHES STREET



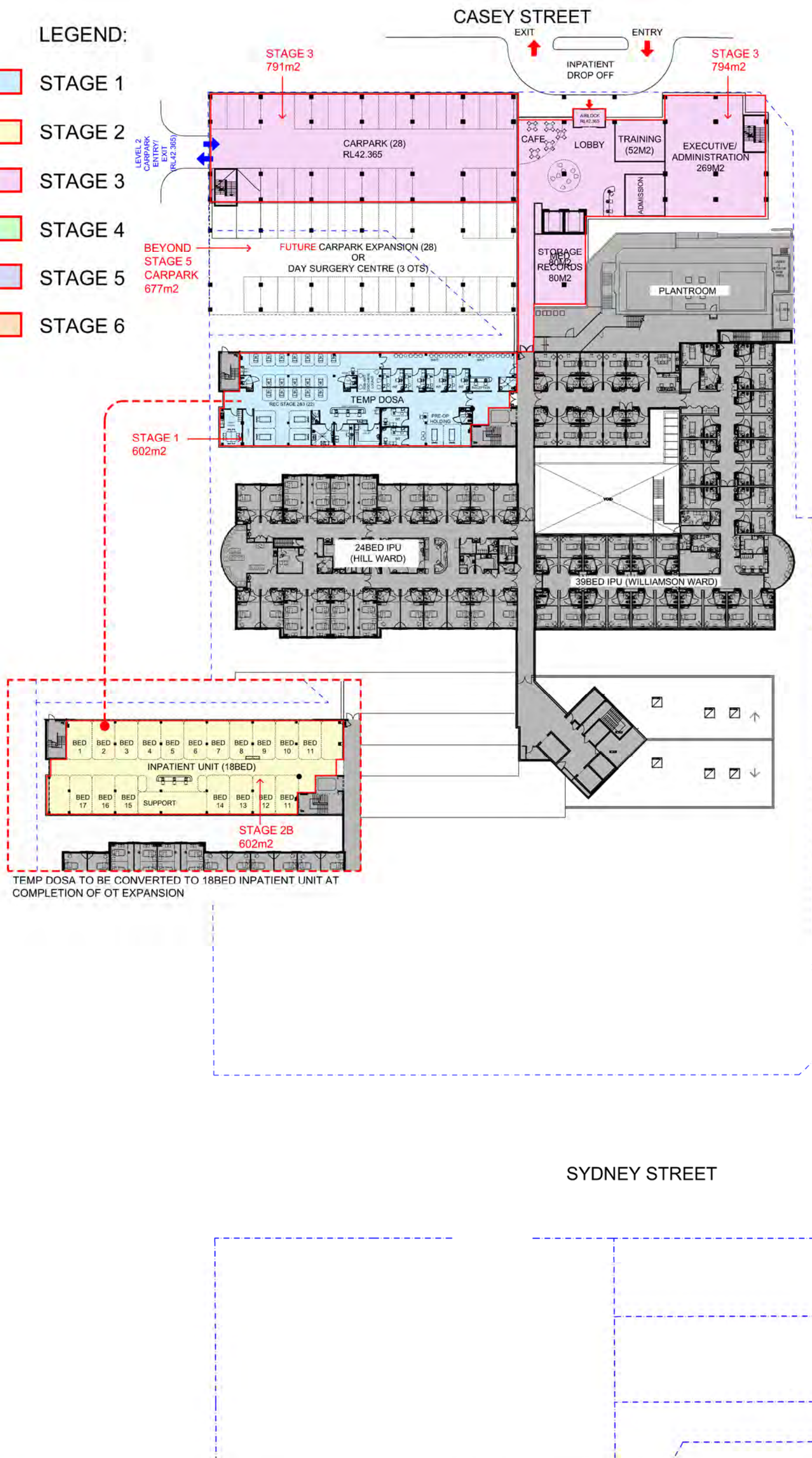
LAKE MACQUARIE PRIVATE HOSPITAL MASTERPLAN

LEVEL 1 STAGING PLAN - OPTION 16



LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6



**LAKE MACQUARIE PRIVATE HOSPITAL
MASTERPLAN**

LEVEL 2 STAGING PLAN - OPTION 16

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0 5 10 15 20

SCALE 1:600 @ A3

LMPH17-STAGING-4

ISSUE 4 2 October 2021

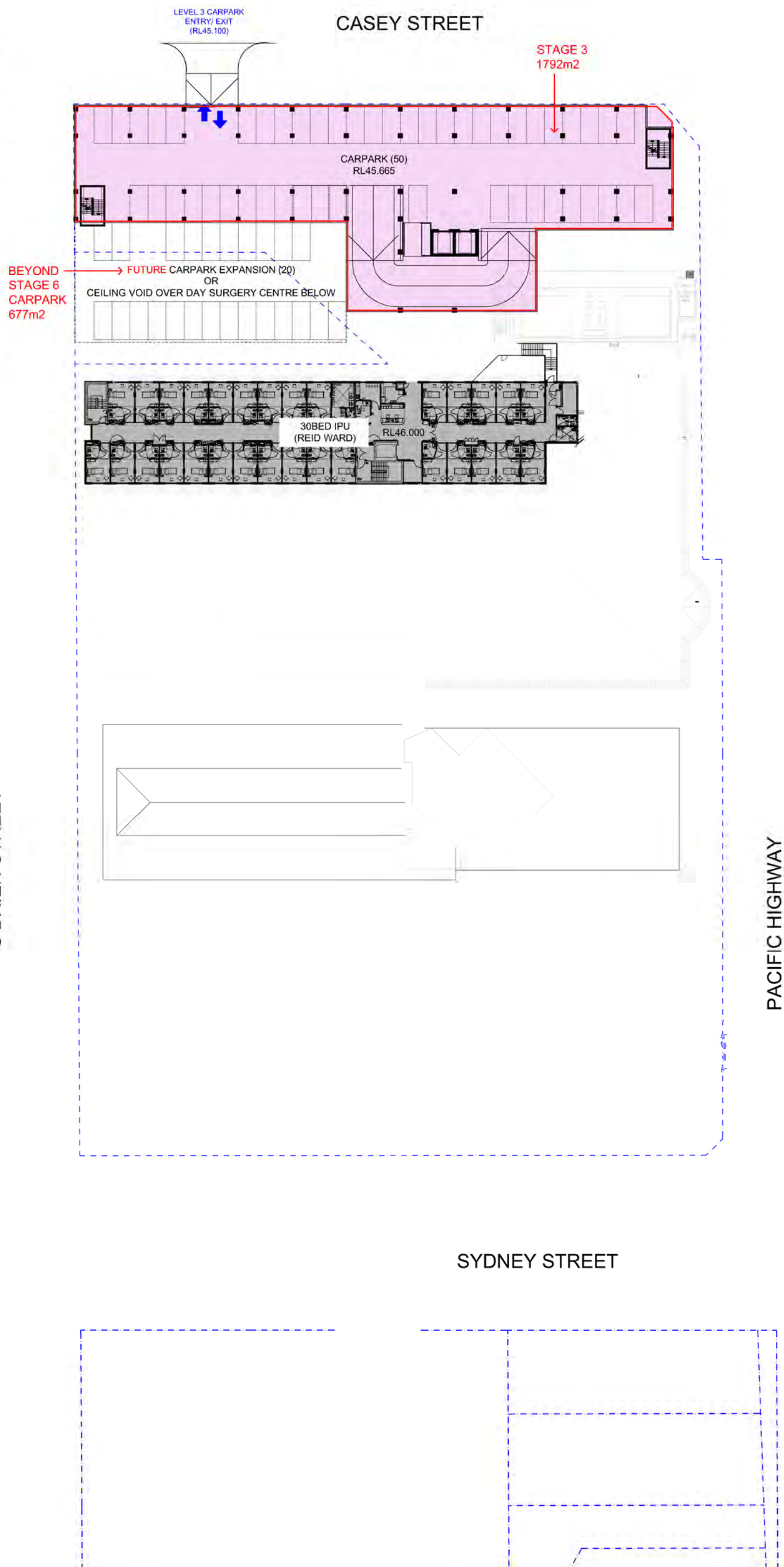


ARCHITECTS AND HEALTH FACILITY PLANNERS



LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6



HUGHES STREET

LAKE MACQUARIE PRIVATE HOSPITAL
MASTERPLAN

LEVEL 3 STAGING PLAN - OPTION 16

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0 5 10 15 20

SCALE 1:600 @ A3

LMPH17-STAGING-5

ISSUE 4 2 October 2021

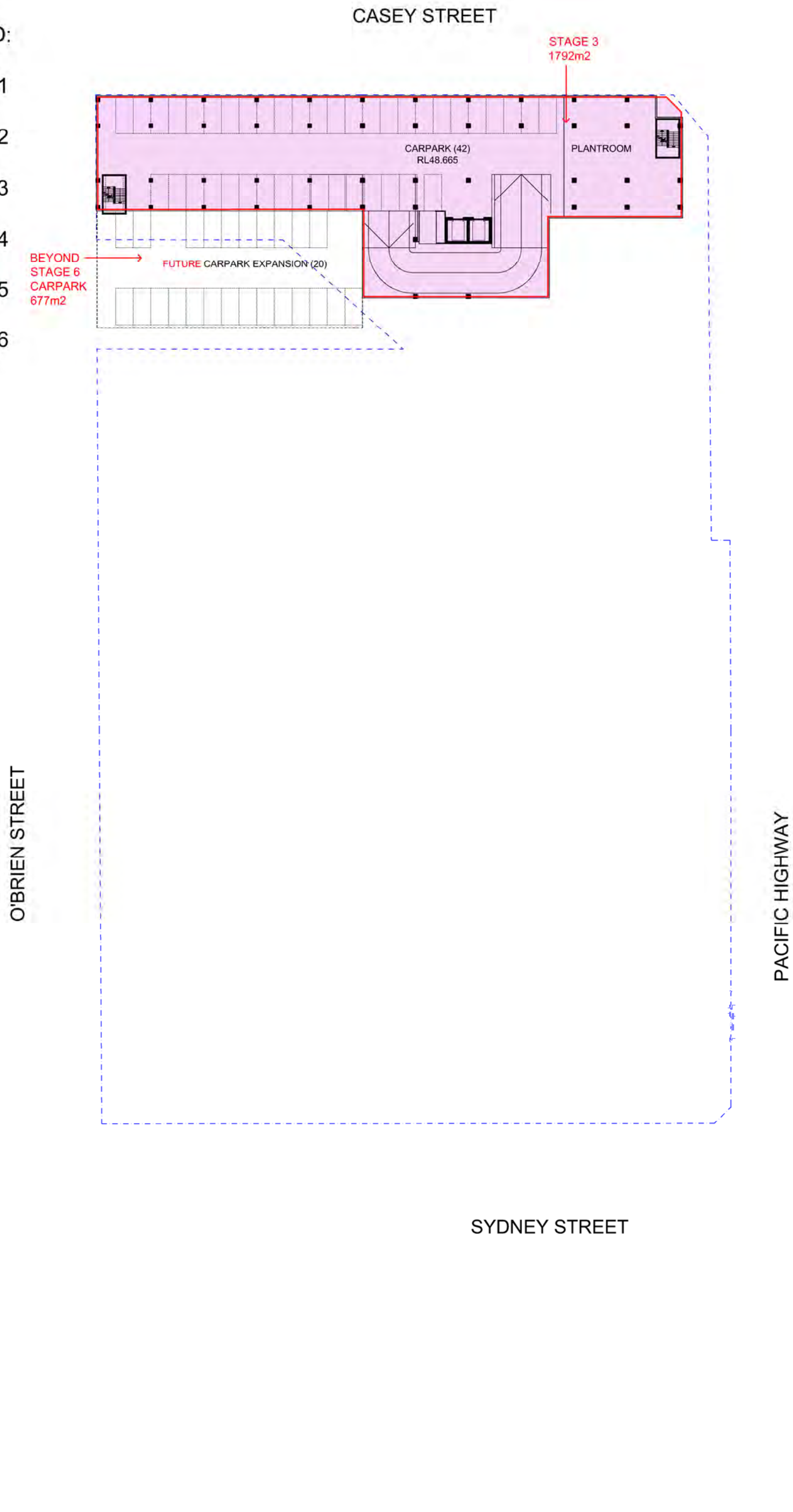


ARCHITECTS AND HEALTH FACILITY PLANNERS



LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6



**LAKE MACQUARIE PRIVATE HOSPITAL
MASTERPLAN**

LEVEL 4 STAGING PLAN - **OPTION 16**

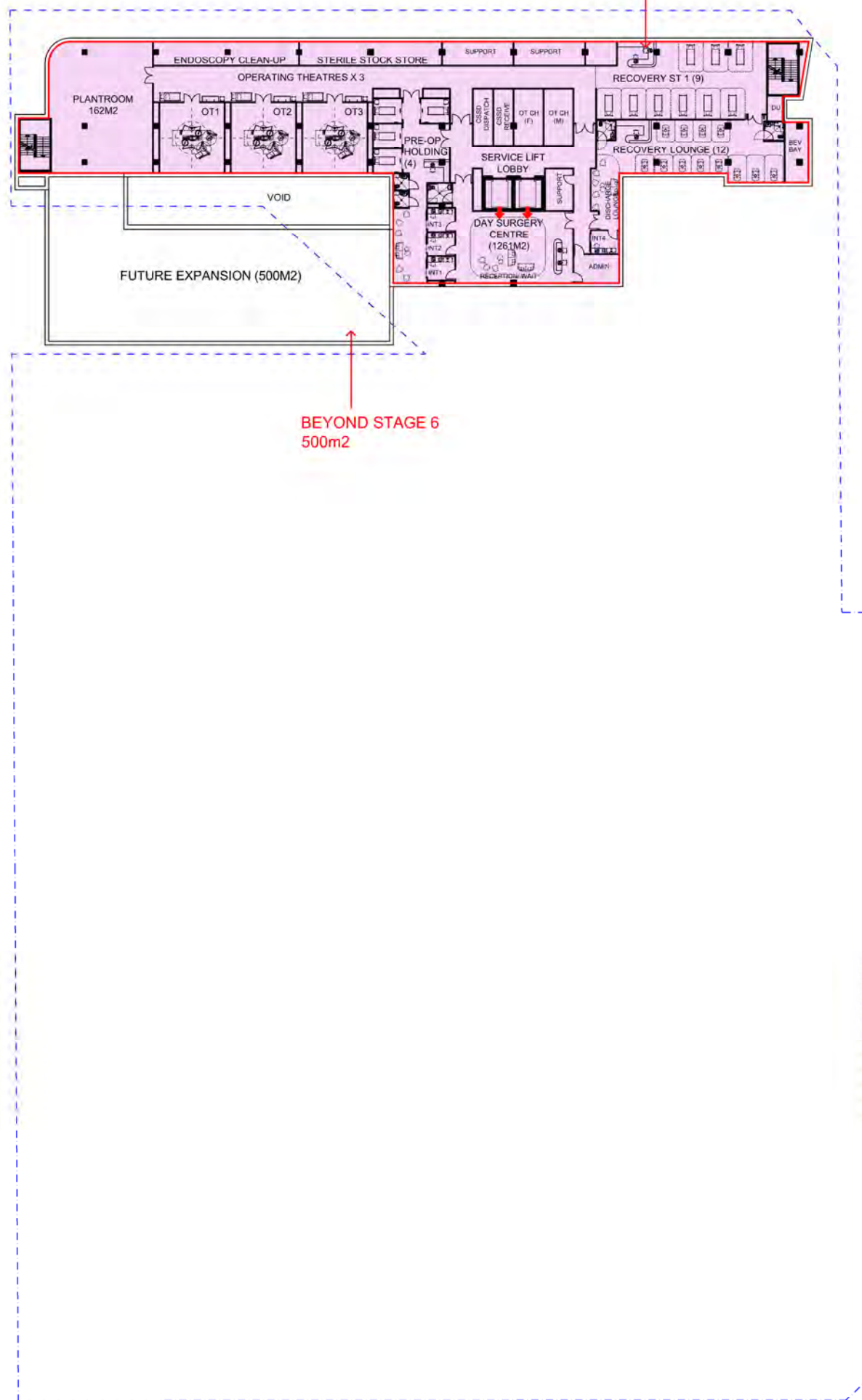


LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6

CASEY STREET

STAGE 3 - COLD SHELL
STAGE 5 - FITOUT (TIMING TBC)
1504m²



BEYOND STAGE 6
500m²

O'BRIEN STREET

PACIFIC HIGHWAY

SYDNEY STREET

LAKE MACQUARIE PRIVATE HOSPITAL
MASTERPLAN

LEVEL 5 STAGING PLAN - OPTION 16

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0 5 10 15 20

SCALE 1:600 @ A3

LMPH17-STAGING-7

ISSUE 4 2 October 2021

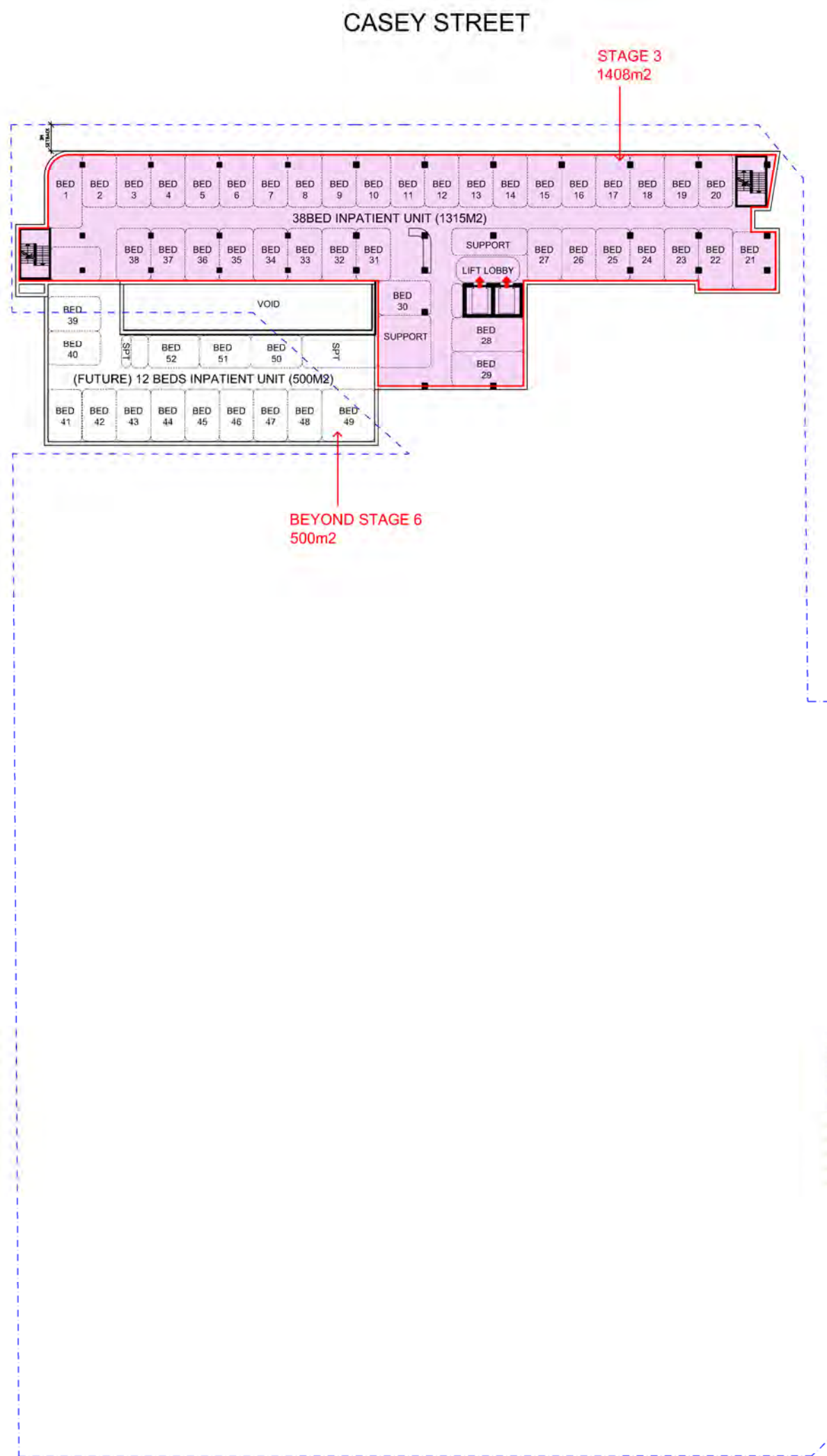


ARCHITECTS AND HEALTH FACILITY PLANNERS



LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6



SYDNEY STREET

LAKE MACQUARIE PRIVATE HOSPITAL
MASTERPLAN

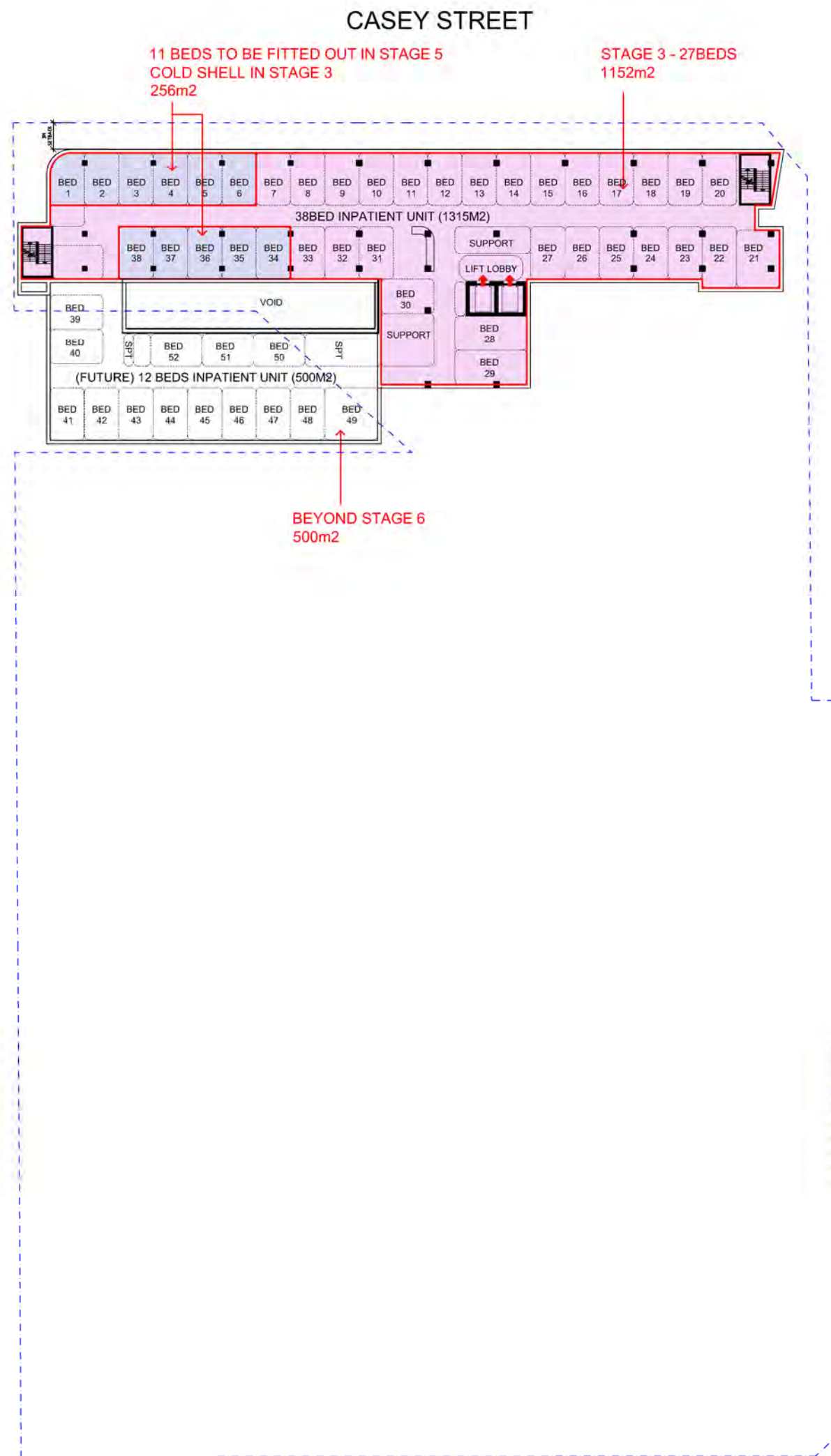
LEVEL 6 STAGING PLAN - OPTION 16



LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6

O'BRIEN STREET



SYDNEY STREET

PACIFIC HIGHWAY

LAKE MACQUARIE PRIVATE HOSPITAL MASTERPLAN

LEVEL 7 STAGING PLAN - **OPTION 16**

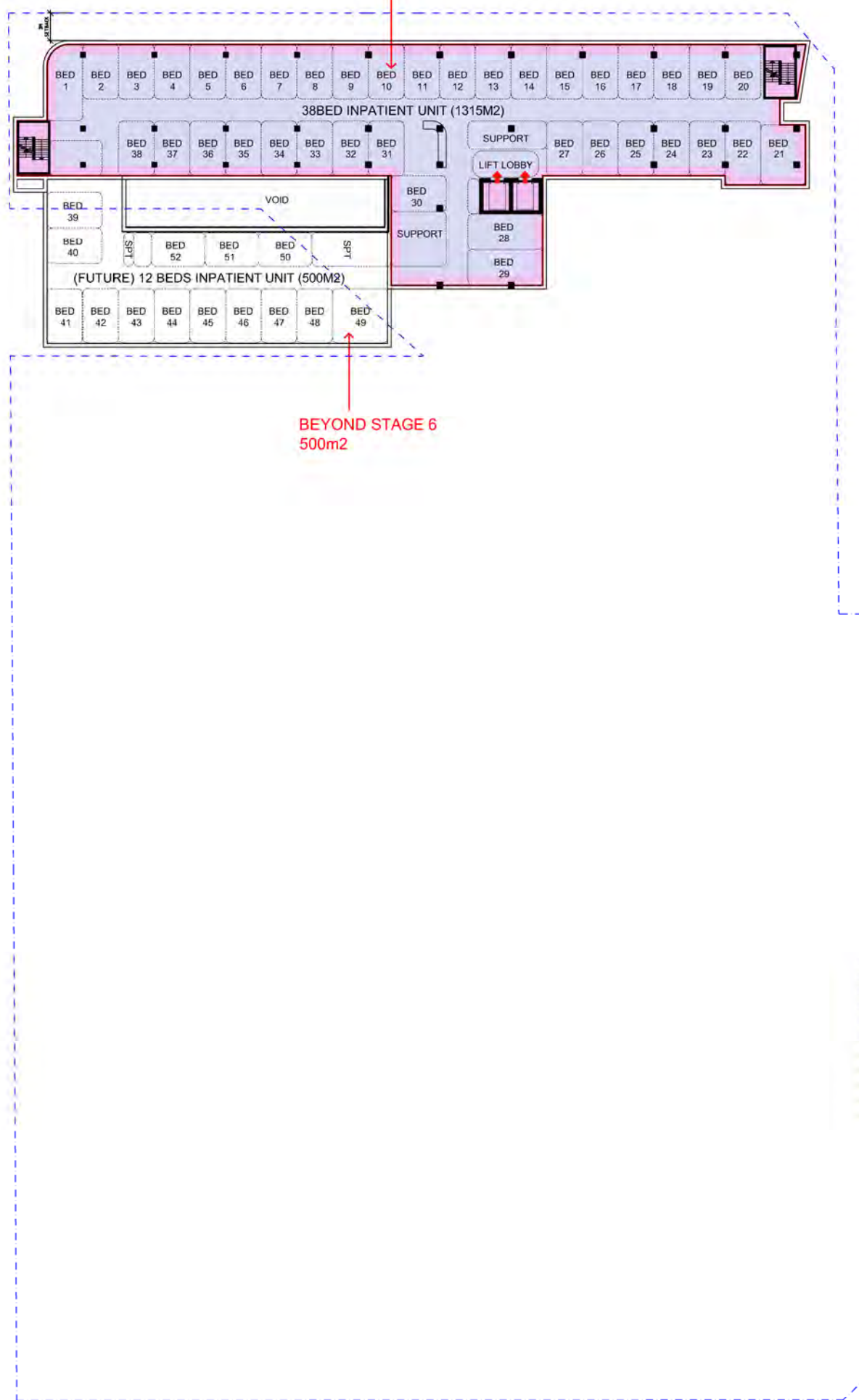


LEGEND:

- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6

CASEY STREET

STAGE 3 COLD SHELL
STAGE 5 - FITOUT 38BEDS (TIMING TBC)
1408m2



BEYOND STAGE 6
500m2

O'BRIEN STREET

PACIFIC HIGHWAY

SYDNEY STREET

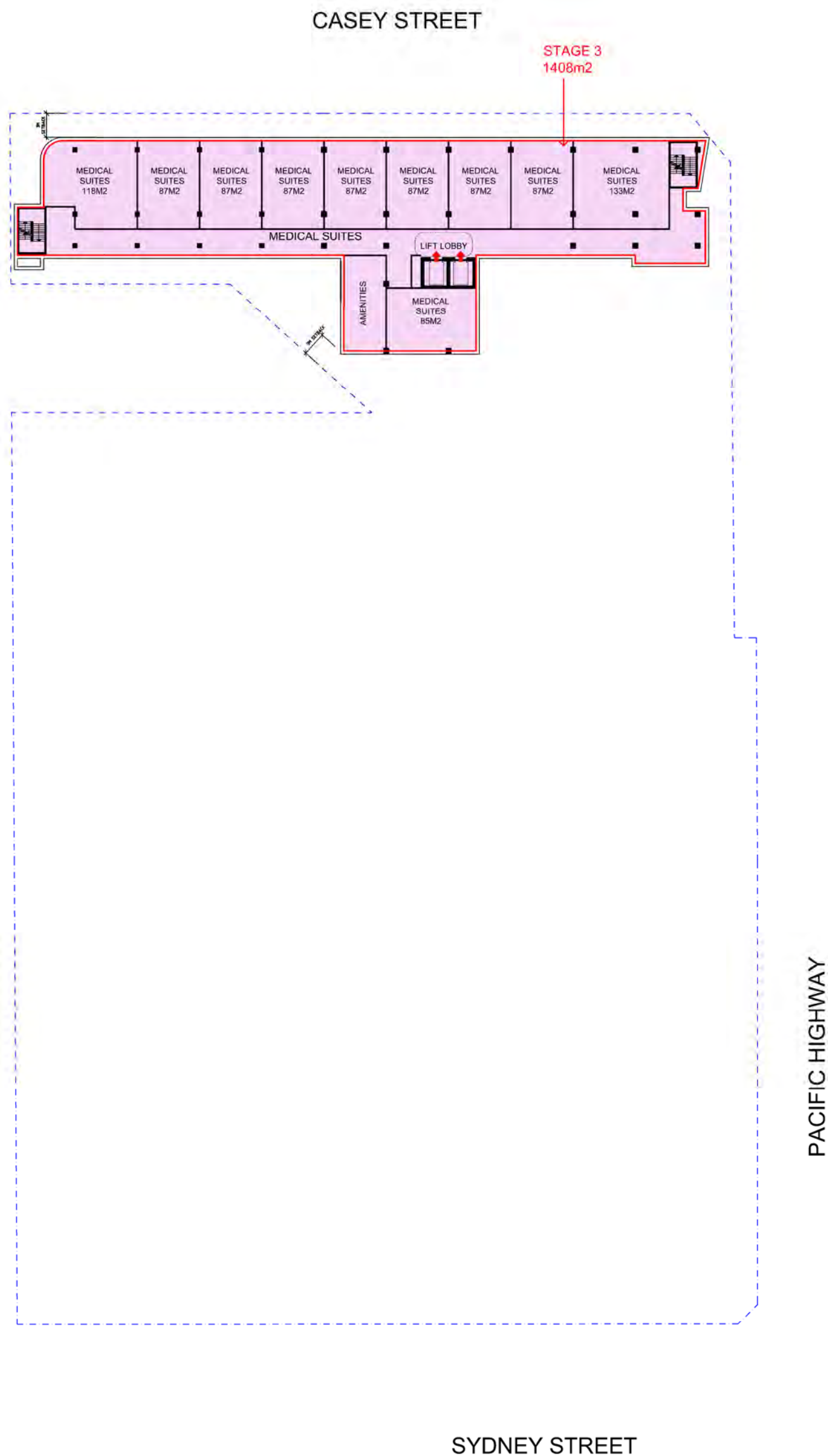
LAKE MACQUARIE PRIVATE HOSPITAL
MASTERPLAN

LEVEL 8 STAGING PLAN - OPTION 16



LEGEND:

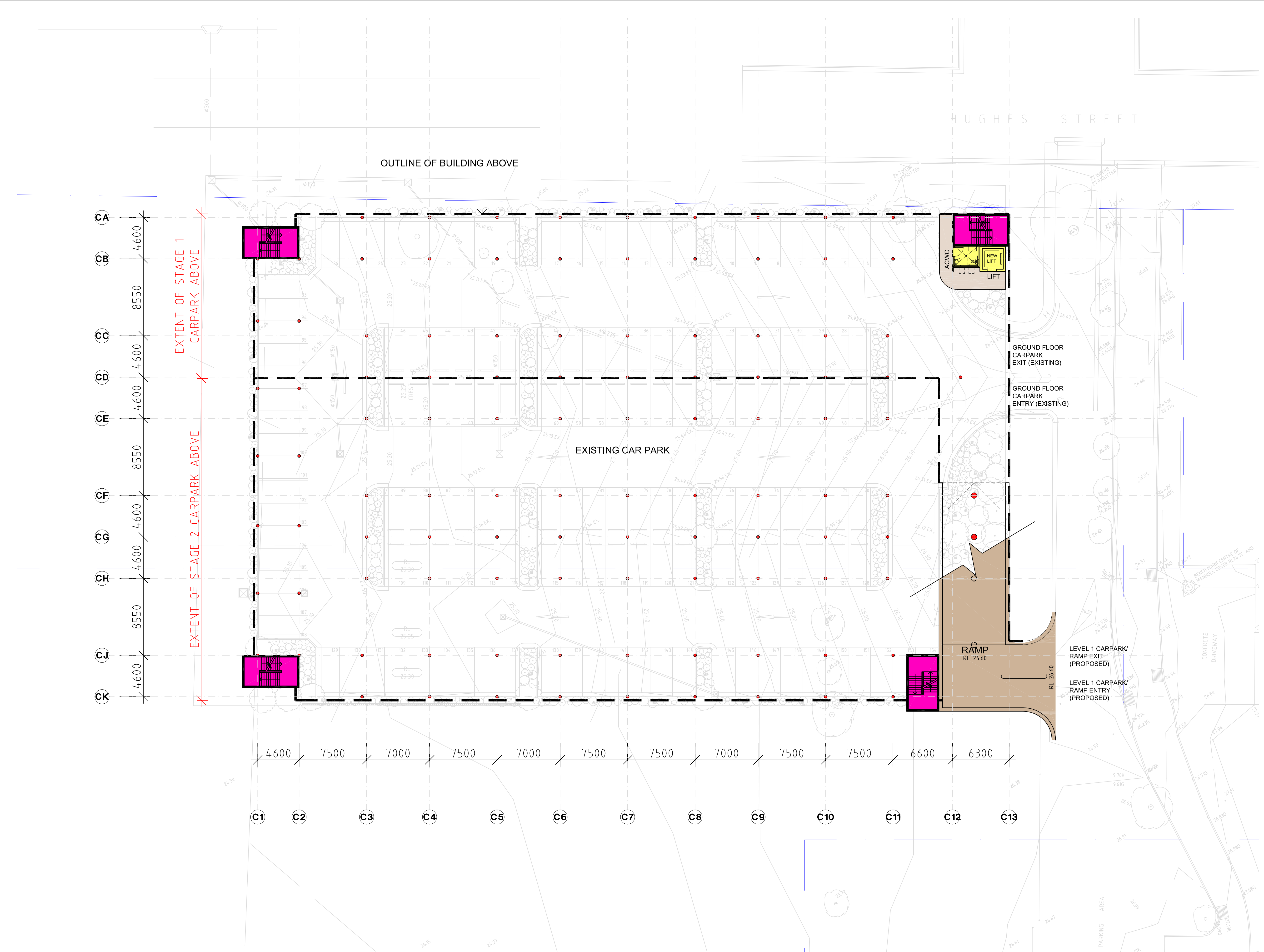
- STAGE 1
- STAGE 2
- STAGE 3
- STAGE 4
- STAGE 5
- STAGE 6



**LAKE MACQUARIE PRIVATE HOSPITAL
MASTERPLAN**

LEVEL 8 STAGING PLAN - **OPTION 16**





LEGEND:

- SITE BOUNDARY
- COLUMN ON GROUND FLOOR

| | | | |
|-----|----------------------|----------|----|
| 1 | FIRST ISSUE | 19.10.21 | HS |
| REV | REVISION DESCRIPTION | DATE | BY |

Project

LAKE MACQUARIE PRIVATE HOSPITAL

Principal

RAMSAY HEALTH CARE PTY LIMITED

KEY PLAN

HEALTH PROJECTS INTERNATIONAL
Architects and Health Facility Planners
ACN 059 859 595
Suite 1, Ground Floor, 68 Milsons Point, NSW 2061
Ph: (02) 9460 4199 Fax: (02) 9460 4299

CAD File

Dwg.No.

Issue

Drawing Title

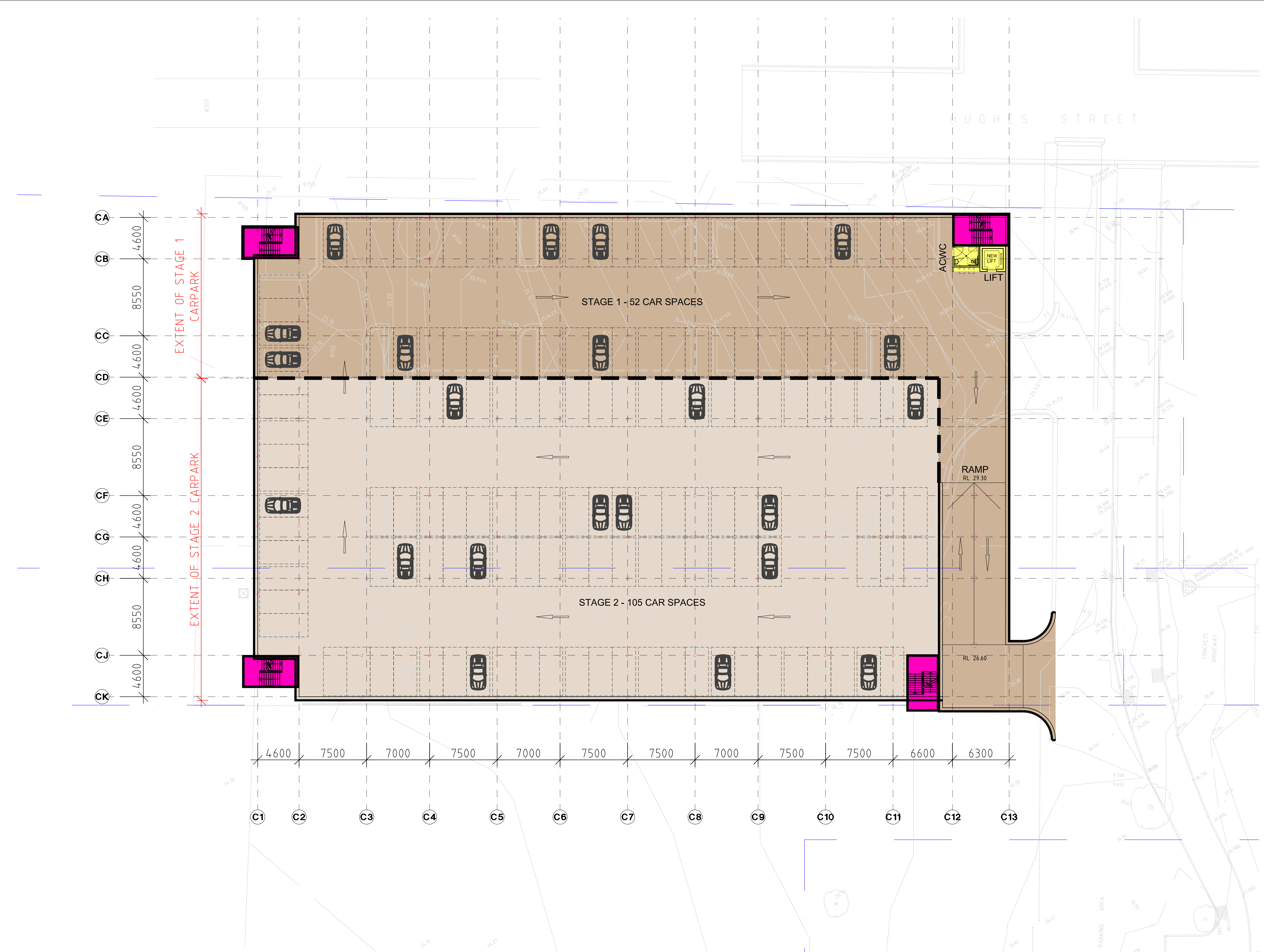
HUGHES STREET CARPARK - GROUND LEVEL

| | | | | |
|-------------|-------|---------|----------|---------|
| Block/ Zone | Drawn | Checked | Date | Scale/s |
| AA | AA | HST | 19.10.21 | 1:200 |

| | | | | | | | | |
|---------|----|------|------------|----|------|------------|----|------|
| Subject | By | Date | Subject | By | Date | Subject | By | Date |
| RDS | | | STRUCT | | | PROJ. ARCH | | |
| ARCH | | | SPEC. CONS | | | | | |
| AUT | | | SERV | | | | | |

Quality Endorsed Company

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ALL DIMENSIONS SHALL BE VERIFIED ON SITE AND
DISCREPANCIES IMMEDIATELY BROUGHT TO THE
ATTENTION OF THE PROJECT MANAGER
FOR RESOLUTION



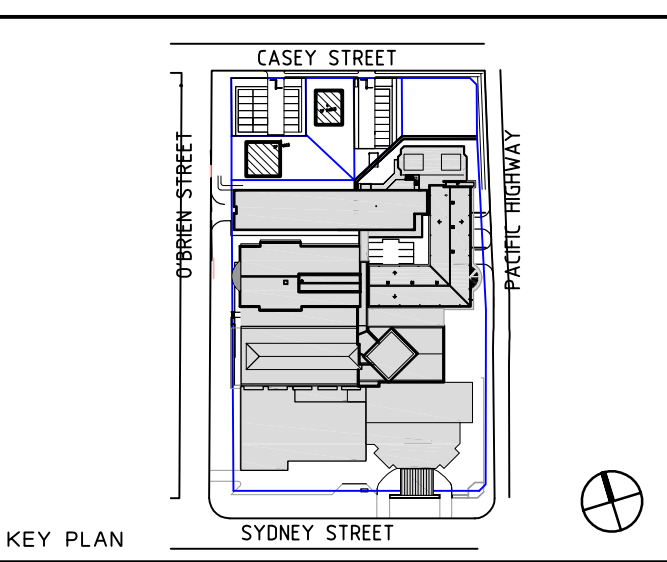
LEGEND:

- SITE BOUNDARY
- COLUMN ON GROUND FLOOR

| | | | |
|-----|----------------------|----------|----|
| 1 | FIRST ISSUE | 18.10.21 | HS |
| REV | REVISION DESCRIPTION | DATE | BY |

Project
LAKE MACQUARIE PRIVATE HOSPITAL

Principal
RAMSAY HEALTH CARE PTY LIMITED



| | | | |
|--|------------------------|------------------------------|-------------------|
| HP HEALTH PROJECTS INTERNATIONAL Architects and Health Facility Planners ACN 059 859 595 Suite 1, Ground Floor, 68 Milsons Point, NSW 2061 Ph: (02) 9460 4199 Fax: (02) 9460 4299 | CAD File LMPH18-CP1 | Dwg.No. LMPH18-CP1 | Issue 1 |
|--|------------------------|------------------------------|-------------------|

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ALL DIMENSIONS SHALL BE VERIFIED ON SITE AND
DISCREPANCIES IMMEDIATELY BROUGHT TO THE
ATTENTION OF THE PROJECT MANAGER
FOR RESOLUTION



| Subject | By | Date | Subject | By | Date | Subject | By | Date |
|---------|----|------|------------|----|------|------------|----|------|
| RDS | | | STRUCT | | | PROJ. ARCH | | |
| ARCH | | | SPEC. CONS | | | | | |
| AUT | | | SERV | | | | | |

| Block/ Zone | Drawn | Checked | Date | Scale/s |
|---|-------|---------|----------|---------|
| AA | AA | HST | 18.10.21 | 1:200 |
| Drawing Title HUGHES STREET CARPARK - LEVEL 1 | | | | |

Appendix C

Traffic Volume Data

TRANS TRAFFIC SURVEY

TURNING MOVEMENT SURVEY

Intersection of The Crescent and Pacific Hwy, Gateshead

GPS: -32.881949, 151.692351

Date: Wed 13/10/21

Weather: Overcast

Suburban: Gateshead

Customer: TTPA

North: Pacific Hwy

East: The Crescent

South: Pacific Hwy

West: Sydney St

Survey Period: AM: 6:30 AM-9:30 AM

PM: 3:00 PM-6:00 PM

Traffic Peak: AM: 8:00 AM-9:00 AM

PM: 3:30 PM-4:30 PM

All Vehicles

| Time | | North Approach Pacific Hwy | | | | East Approach The Crescent | | | | South Approach Pacific Hwy | | | | West Approach Sydney St | | | | Hourly Total | Peak |
|--------------|------------|----------------------------|----|-----|---|----------------------------|---|----|---|----------------------------|---|-----|----|-------------------------|----|----|----|--------------|------|
| Period Start | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L | | |
| 6:30 | 6:45 | 0 | 5 | 65 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 162 | 18 | 0 | 9 | 0 | 11 | 1061 | |
| 6:45 | 7:00 | 0 | 11 | 84 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 146 | 20 | 0 | 17 | 0 | 16 | 1105 | |
| 7:00 | 7:15 | 0 | 4 | 64 | 0 | 0 | 1 | 2 | 0 | 0 | 2 | 119 | 10 | 0 | 4 | 1 | 11 | 1138 | |
| 7:15 | 7:30 | 0 | 6 | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 150 | 7 | 0 | 9 | 1 | 16 | 1271 | |
| 7:30 | 7:45 | 0 | 8 | 100 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 178 | 9 | 0 | 9 | 0 | 10 | 1359 | |
| 7:45 | 8:00 | 0 | 12 | 114 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 150 | 19 | 0 | 21 | 0 | 11 | 1440 | |
| 8:00 | 8:15 | 0 | 17 | 96 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 181 | 26 | 0 | 14 | 1 | 15 | 1459 | Peak |
| 8:15 | 8:30 | 0 | 12 | 106 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 188 | 17 | 0 | 14 | 1 | 20 | 1445 | |
| 8:30 | 8:45 | 1 | 12 | 123 | 1 | 0 | 1 | 0 | 1 | 0 | 3 | 205 | 19 | 0 | 18 | 2 | 10 | 1396 | |
| 8:45 | 9:00 | 0 | 17 | 125 | 2 | 0 | 2 | 0 | 0 | 0 | 1 | 163 | 17 | 0 | 13 | 0 | 9 | | |
| 9:00 | 9:15 | 0 | 11 | 102 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 165 | 29 | 0 | 17 | 1 | 9 | | |
| 9:15 | 9:30 | 0 | 4 | 114 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 128 | 31 | 0 | 25 | 0 | 10 | | |
| 15:00 | 15:15 | 0 | 11 | 173 | 3 | 0 | 1 | 2 | 1 | 0 | 2 | 145 | 43 | 0 | 24 | 0 | 19 | 1722 | |
| 15:15 | 15:30 | 0 | 14 | 188 | 2 | 0 | 2 | 1 | 0 | 0 | 0 | 154 | 22 | 0 | 33 | 0 | 8 | 1730 | |
| 15:30 | 15:45 | 0 | 12 | 178 | 2 | 0 | 2 | 0 | 0 | 0 | 1 | 161 | 21 | 0 | 27 | 1 | 11 | 1761 | Peak |
| 15:45 | 16:00 | 0 | 12 | 231 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 143 | 23 | 0 | 25 | 0 | 20 | 1747 | |
| 16:00 | 16:15 | 0 | 14 | 187 | 1 | 0 | 1 | 4 | 1 | 0 | 3 | 159 | 19 | 0 | 30 | 1 | 12 | 1705 | |
| 16:15 | 16:30 | 0 | 11 | 219 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 155 | 18 | 0 | 26 | 3 | 18 | 1659 | |
| 16:30 | 16:45 | 0 | 5 | 190 | 1 | 0 | 1 | 1 | 2 | 0 | 4 | 153 | 19 | 0 | 19 | 1 | 6 | 1635 | |
| 16:45 | 17:00 | 0 | 5 | 210 | 4 | 0 | 1 | 2 | 0 | 0 | 1 | 159 | 11 | 0 | 16 | 1 | 6 | 1610 | |
| 17:00 | 17:15 | 0 | 8 | 171 | 2 | 0 | 1 | 2 | 0 | 0 | 3 | 151 | 18 | 0 | 26 | 0 | 4 | 1525 | |
| 17:15 | 17:30 | 0 | 11 | 232 | 1 | 0 | 0 | 2 | 1 | 0 | 2 | 137 | 12 | 0 | 23 | 1 | 9 | | |
| 17:30 | 17:45 | 0 | 6 | 164 | 1 | 0 | 2 | 1 | 1 | 0 | 0 | 163 | 13 | 0 | 21 | 1 | 4 | | |
| 17:45 | 18:00 | 0 | 9 | 176 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 107 | 18 | 0 | 11 | 1 | 5 | | |

| Peak Time | | North Approach Pacific Hwy | | | | East Approach The Crescent | | | | South Approach Pacific Hwy | | | | West Approach Sydney St | | | | Peak total |
|--------------|------------|----------------------------|----|-----|---|----------------------------|---|----|---|----------------------------|---|-----|----|-------------------------|-----|----|----|------------|
| Period Start | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L | |
| 8:00 | 9:00 | 1 | 58 | 450 | 4 | 0 | 5 | 0 | 1 | 2 | 5 | 737 | 79 | 0 | 59 | 4 | 54 | 1459 |
| 15:30 | 16:30 | 0 | 49 | 815 | 8 | 0 | 5 | 5 | 1 | 0 | 5 | 618 | 81 | 0 | 108 | 5 | 61 | 1761 |

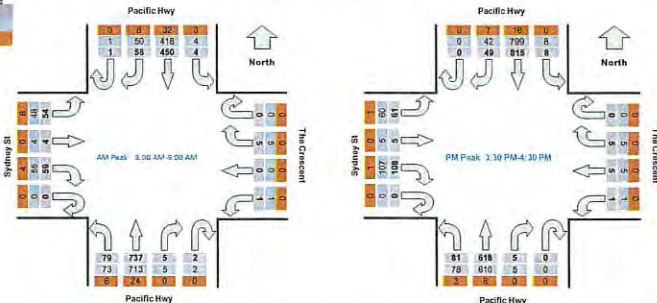
Note: Site sketch is for illustrating traffic flows. Direction is indicative only, drawing is not to scale and not an exact streets configuration.

Graphic

Total

Light

Heavy



Light Vehicles

| Time | | North Approach Pacific Hwy | | | | East Approach The Crescent | | | | South Approach Pacific Hwy | | | | West Approach Sydney St | | | |
|--------------|------------|----------------------------|----|-----|---|----------------------------|---|----|---|----------------------------|---|-----|----|-------------------------|----|----|----|
| Period Start | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L |
| 6:30 | 6:45 | 0 | 4 | 62 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 156 | 18 | 0 | 9 | 0 | 11 |
| 6:45 | 7:00 | 0 | 11 | 82 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 139 | 20 | 0 | 17 | 0 | 16 |
| 7:00 | 7:15 | 0 | 4 | 62 | 0 | 0 | 1 | 2 | 0 | 0 | 2 | 115 | 10 | 0 | 4 | 1 | 11 |
| 7:15 | 7:30 | 0 | 6 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 148 | 7 | 0 | 9 | 1 | 14 |
| 7:30 | 7:45 | 0 | 8 | 96 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 170 | 9 | 0 | 8 | 0 | 10 |
| 7:45 | 8:00 | 0 | 12 | 107 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 144 | 19 | 0 | 20 | 0 | 11 |
| 8:00 | 8:15 | 0 | 14 | 90 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 176 | 23 | 0 | 13 | 1 | 14 |
| 8:15 | 8:30 | 0 | 8 | 97 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 181 | 16 | 0 | 12 | 1 | 18 |
| 8:30 | 8:45 | 1 | 11 | 112 | 1 | 0 | 1 | 0 | 1 | 0 | 3 | 199 | 18 | 0 | 18 | 2 | 8 |
| 8:45 | 9:00 | 0 | 17 | 119 | 2 | 0 | 2 | 0 | 0 | 0 | 1 | 157 | 16 | 0 | 12 | 0 | 8 |
| 9:00 | 9:15 | 0 | 10 | 95 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 161 | 29 | 0 | 15 | 1 | 6 |
| 9:15 | 9:30 | 0 | 4 | 110 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 123 | 31 | 0 | 23 | 0 | 9 |
| 15:00 | 15:15 | 0 | 11 | 167 | 3 | 0 | 1 | 2 | 1 | 0 | 2 | 138 | 42 | 0 | 24 | 0 | 19 |
| 15:15 | 15:30 | 0 | 14 | 180 | 2 | 0 | 2 | 1 | 0 | 0 | 0 | 149 | 21 | 0 | 32 | 0 | 7 |
| 15:30 | 15:45 | 0 | 11 | 174 | 2 | 0 | 2 | 0 | 0 | 0 | 1 | 161 | 19 | 0 | 27 | 1 | 10 |
| 15:45 | 16:00 | 0 | 6 | 227 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 139 | 22 | 0 | 25 | 0 | 20 |
| 16:00 | 16:15 | 0 | 14 | 183 | 1 | 0 | 1 | 4 | 1 | 0 | 3 | 155 | 19 | 0 | 29 | 1 | 12 |
| 16:15 | 16:30 | 0 | 11 | 215 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 155 | 18 | 0 | 26 | 3 | 18 |
| 16:30 | 16:45 | 0 | 5 | 189 | 1 | 0 | 1 | 1 | 2 | 0 | 4 | 150 | 19 | 0 | 19 | 1 | 6 |
| 16:45 | 17:00 | 0 | 5 | 209 | 4 | 0 | 1 | 2 | 0 | 0 | 1 | 156 | 11 | 0 | 16 | 1 | 6 |
| 17:00 | 17:15 | 0 | 8 | 169 | 2 | 0 | 1 | 2 | 0 | 0 | 3 | 151 | 18 | 0 | 26 | 0 | 4 |
| 17:15 | 17:30 | 0 | 11 | 229 | 1 | 0 | 0 | 2 | 1 | 0 | 2 | 137 | 12 | 0 | 23 | 1 | 9 |
| 17:30 | 17:45 | 0 | 6 | 162 | 1 | 0 | 2 | 1 | 1 | 0 | 0 | 162 | 13 | 0 | 21 | 1 | 4 |
| 17:45 | 18:00 | 0 | 9 | 173 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 105 | 18 | 0 | 11 | 1 | 5 |

| Peak Time | | North Approach Pacific Hwy | | | | East Approach The Crescent | | | | South Approach Pacific Hwy | | | | West Approach Sydney St | | | | Peak total |
|--------------|------------|----------------------------|----|-----|---|----------------------------|---|----|---|----------------------------|---|-----|----|-------------------------|-----|----|----|------------|
| Period Start | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L | |
| 8:00 | 9:00 | 1 | 50 | 418 | 4 | 0 | 5 | 0 | 1 | 2 | 5 | 713 | 73 | 0 | 55 | 4 | 48 | 1379 |
| 15:30 | 16:30 | 0 | 42 | 799 | 8 | 0 | 5 | 5 | 1 | 0 | 5 | 610 | 78 | 0 | 107 | 5 | 60 | 1725 |

Heavy Vehicles

| Time | | North Approach Pacific Hwy | | | | East Approach The Crescent | | | | South Approach Pacific Hwy | | | | West Approach Sydney St | | | |
|--------------|------------|----------------------------|---|----|---|----------------------------|---|----|---|----------------------------|---|----|---|-------------------------|---|----|---|
| Period Start | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L |
| 6:30 | 6:45 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 |
| 6:45 | 7:00 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 |
| 7:00 | 7:15 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 |
| 7:15 | 7:30 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:30 | 7:45 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 1 | 0 | 0 |
| 7:45 | 8:00 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 1 | 0 | 0 |
| 8:00 | 8:15 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 1 | 0 | 1 |
| 8:15 | 8:30 | 0 | 4 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 2 | 0 | 2 |
| 8:30 | 8:45 | 0 | 1 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 2 |
| 8:45 | 9:00 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 1 | 0 | 1 |
| 9:00 | 9:15 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 2 | 0 | 3 |
| 9:15 | 9:30 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 2 | 0 | 1 |
| 15:00 | 15:15 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 |
| 15:15 | 15:30 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 1 | 0 | 1 |
| 15:30 | 15:45 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 |
| 15:45 | 16:00 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 |
| 16:00 | 16:15 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 1 | 0 | 0 |
| 16:15 | 16:30 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 |
| 16:45 | 17:00 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 |
| 17:00 | 17:15 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15 | 17:30 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:30 | 17:45 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |

| Peak Time | | North Approach Pacific Hwy | | | | East Approach The Crescent | | | | South Approach Pacific Hwy | | | | West Approach Sydney St | | | | Peak total |
|--------------|------------|----------------------------|---|----|---|----------------------------|---|----|---|----------------------------|---|----|---|-------------------------|---|----|---|------------|
| Period Start | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L | |
| 8:00 | 9:00 | 0 | 8 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 6 | 0 | 4 | 0 | 6 | 80 |
| 15:30 | 16:30 | 0 | 7 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 1 | 0 | 1 | 36 |

TRANS TRAFFIC SURVEY

TURNING MOVEMENT SURVEY

trafficsurvey.com.au



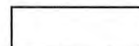
Carpark Access off Hughes St, Gateshead

GPS -32.982678, 151.690775

| | |
|-----------|--------------|
| Date: | Wed 13/10/21 |
| Weather: | Overcast |
| Suburban: | Gateshead |
| Customer: | TTPA |

All Vehicles

| Time | | In | Out |
|--------------|------------|----|-----|
| Period Start | Period End | | |
| 6:30 | 6:45 | 8 | 1 |
| 6:45 | 7:00 | 19 | 0 |
| 7:00 | 7:15 | 4 | 0 |
| 7:15 | 7:30 | 7 | 0 |
| 7:30 | 7:45 | 8 | 0 |
| 7:45 | 8:00 | 16 | 0 |
| 8:00 | 8:15 | 15 | 0 |
| 8:15 | 8:30 | 19 | 1 |
| 8:30 | 8:45 | 6 | 0 |
| 8:45 | 9:00 | 10 | 0 |
| 9:00 | 9:15 | 3 | 1 |
| 9:15 | 9:30 | 4 | 0 |
| 15:00 | 15:15 | 1 | 8 |
| 15:15 | 15:30 | 1 | 7 |
| 15:30 | 15:45 | 1 | 6 |
| 15:45 | 16:00 | 1 | 6 |
| 16:00 | 16:15 | 0 | 12 |
| 16:15 | 16:30 | 0 | 14 |
| 16:30 | 16:45 | 1 | 11 |
| 16:45 | 17:00 | 0 | 8 |
| 17:00 | 17:15 | 0 | 19 |
| 17:15 | 17:30 | 0 | 6 |
| 17:30 | 17:45 | 0 | 6 |
| 17:45 | 18:00 | 1 | 2 |



TRANS TRAFFIC SURVEY

TURNING MOVEMENT SURVEY

trafficsurvey.com.au



Lake Macquarie Private Hospital Entrance from Sydney St, Gateshead

GPS -32.981727, 151.691712

| | |
|-----------|--------------|
| Date: | Wed 13/10/21 |
| Weather: | Overcast |
| Suburban: | Gateshead |
| Customer: | TTPA |

All Vehicles (N.B. right turn IN, not left which is to doctors car park)

| Time | | Entry | Exit |
|--------------|------------|-------|------|
| Period Start | Period End | | |
| 6:30 | 6:45 | 0 | 0 |
| 6:45 | 7:00 | 3 | 3 |
| 7:00 | 7:15 | 3 | 3 |
| 7:15 | 7:30 | 1 | 1 |
| 7:30 | 7:45 | 2 | 2 |
| 7:45 | 8:00 | 3 | 3 |
| 8:00 | 8:15 | 1 | 1 |
| 8:15 | 8:30 | 3 | 3 |
| 8:30 | 8:45 | 2 | 1 |
| 8:45 | 9:00 | 3 | 4 |
| 9:00 | 9:15 | 3 | 3 |
| 9:15 | 9:30 | 1 | 1 |
| 15:00 | 15:15 | 5 | 3 |
| 15:15 | 15:30 | 3 | 5 |
| 15:30 | 15:45 | 1 | 1 |
| 15:45 | 16:00 | 4 | 3 |
| 16:00 | 16:15 | 5 | 5 |
| 16:15 | 16:30 | 1 | 1 |
| 16:30 | 16:45 | 2 | 3 |
| 16:45 | 17:00 | 0 | 0 |
| 17:00 | 17:15 | 2 | 2 |
| 17:15 | 17:30 | 1 | 1 |
| 17:30 | 17:45 | 3 | 3 |
| 17:45 | 18:00 | 2 | 1 |
| 18:00 | 18:15 | 3 | 3 |
| 18:15 | 18:30 | 2 | 3 |
| 18:30 | 18:45 | 3 | 2 |
| 18:45 | 19:00 | 1 | 1 |
| 19:00 | 19:15 | 0 | 0 |
| 19:15 | 19:30 | 0 | 1 |
| 19:30 | 19:45 | 2 | 1 |
| 19:45 | 20:00 | 1 | 1 |
| 20:00 | 20:15 | 1 | 2 |
| 20:15 | 20:30 | 1 | 1 |

Appendix D

SIDRA Results

SITE LAYOUT

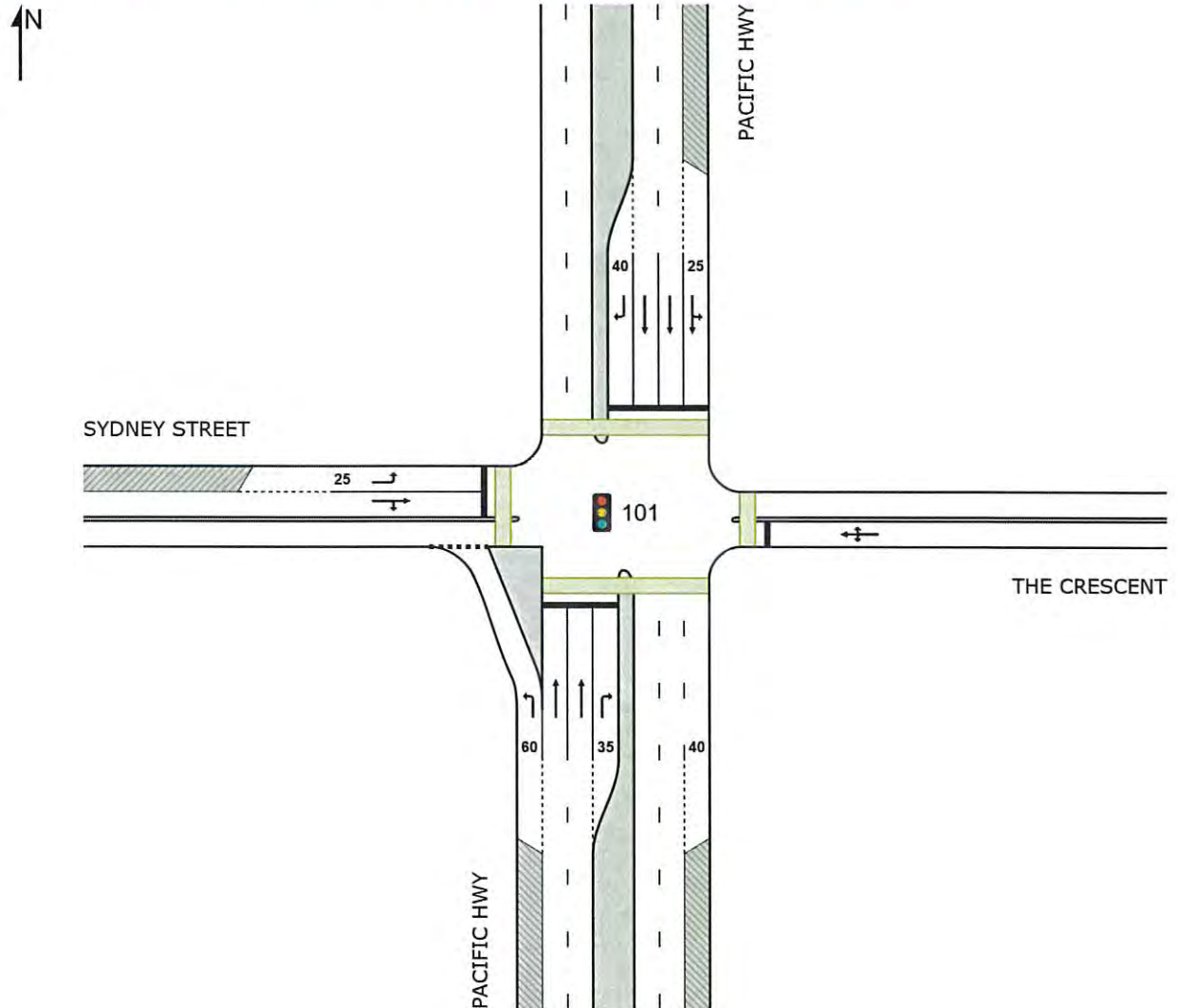
 Site: 101 [PACIFIC HWY & SYDNEY ST/THE CRESCENT]
EXISTING LAYOUT (Site Folder: General)]

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



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Organisation: TRANSPORT AND TRAFFIC PLANNING ASSOCIATES | Licence: NETWORK / 1PC | Created: Monday, 18 October 2021 4:55:39 PM

Project: T:\WORK21\21297 - LAKE MACQUARIE PRIVATE HOSPITAL - 3 SYDNEY ST, GATESHEAD\MODEL\PACIFIC HWY, SYDNEY STREET AND THE CRESCENT_2.sip9

**Site: 101 [PACIFIC HWY & SYDNEY ST/THE CRESCENT
EXISTING AM PEAK (Site Folder: General)]**

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 130 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|--------|---------------|--------|-----------|-------------|------------------|-------------------|----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV] % | [Total veh/h | HV] % | | | | [Veh. veh | Dist] m | | | | |
| South: PACIFIC HWY | | | | | | | | | | | | | | |
| 1 | L2 | 80 | 6.0 | 84 | 6.0 | 0.060 | 6.2 | LOS A | 0.3 | 2.5 | 0.14 | 0.58 | 0.14 | 47.8 |
| 2 | T1 | 1320 | 6.0 | 1389 | 6.0 | * 0.909 | 50.0 | LOS D | 47.6 | 350.5 | 0.96 | 1.01 | 1.13 | 26.6 |
| 3 | R2 | 50 | 6.0 | 53 | 6.0 | 0.092 | 21.8 | LOS B | 1.6 | 11.9 | 0.61 | 0.69 | 0.61 | 35.4 |
| Approach | | 1450 | 6.0 | 1526 | 6.0 | 0.909 | 46.6 | LOS D | 47.6 | 350.5 | 0.91 | 0.97 | 1.06 | 27.5 |
| East: THE CRESCENT | | | | | | | | | | | | | | |
| 4 | L2 | 15 | 4.0 | 16 | 4.0 | * 0.156 | 38.7 | LOS C | 1.6 | 11.9 | 0.86 | 0.72 | 0.86 | 24.3 |
| 5 | T1 | 10 | 4.0 | 11 | 4.0 | 0.156 | 34.7 | LOS C | 1.6 | 11.9 | 0.86 | 0.72 | 0.86 | 27.4 |
| 6 | R2 | 20 | 4.0 | 21 | 4.0 | 0.156 | 38.0 | LOS C | 1.6 | 11.9 | 0.86 | 0.72 | 0.86 | 27.4 |
| Approach | | 45 | 4.0 | 47 | 4.0 | 0.156 | 37.5 | LOS C | 1.6 | 11.9 | 0.86 | 0.72 | 0.86 | 26.4 |
| North: PACIFIC HWY | | | | | | | | | | | | | | |
| 7 | L2 | 28 | 6.0 | 29 | 6.0 | * 0.148 | 25.3 | LOS B | 2.1 | 15.1 | 0.79 | 0.66 | 0.79 | 36.3 |
| 8 | T1 | 610 | 6.0 | 642 | 6.0 | 0.542 | 20.7 | LOS B | 9.5 | 70.0 | 0.87 | 0.73 | 0.87 | 39.4 |
| 9 | R2 | 90 | 6.0 | 95 | 6.0 | 0.340 | 37.2 | LOS C | 3.8 | 28.2 | 0.93 | 0.75 | 0.93 | 30.6 |
| Approach | | 728 | 6.0 | 766 | 6.0 | 0.542 | 23.0 | LOS B | 9.5 | 70.0 | 0.87 | 0.73 | 0.87 | 37.8 |
| West: SYDNEY STREET | | | | | | | | | | | | | | |
| 10 | L2 | 54 | 4.0 | 57 | 4.0 | 0.072 | 25.7 | LOS B | 2.0 | 14.8 | 0.61 | 0.65 | 0.61 | 31.8 |
| 11 | T1 | 10 | 4.0 | 11 | 4.0 | 0.552 | 52.5 | LOS D | 8.0 | 57.9 | 0.95 | 0.79 | 0.95 | 22.7 |
| 12 | R2 | 120 | 4.0 | 126 | 4.0 | 0.552 | 55.8 | LOS D | 8.0 | 57.9 | 0.95 | 0.79 | 0.95 | 21.3 |
| Approach | | 184 | 4.0 | 194 | 4.0 | 0.552 | 46.8 | LOS D | 8.0 | 57.9 | 0.85 | 0.75 | 0.85 | 23.8 |
| All Vehicles | | 2407 | 5.8 | 2534 | 5.8 | 0.909 | 39.3 | LOS C | 47.6 | 350.5 | 0.89 | 0.88 | 0.98 | 29.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

- * Critical Movement (Signal Timing)

| Pedestrian Movement Performance | | | | | | | | | | | | |
|---------------------------------|----------|------------|-----------|-------------|------------------|-----------------------|----------|-----------|---------------------|-------------|--------------|-------------|
| Mov ID | Crossing | Input Vol. | Dem. Flow | Aver. Delay | Level of Service | AVERAGE BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Travel Time | Travel Dist. | Aver. Speed |
| | | ped/h | ped/h | sec | | [Ped ped | Dist] m | | | sec | m | m/sec |
| South: PACIFIC HWY | | | | | | | | | | | | |
| P1 | Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 231.4 | 223.8 | 0.97 |
| East: THE CRESCENT | | | | | | | | | | | | |
| P2 | Full | 50 | 53 | 27.6 | LOS C | 0.1 | 0.1 | 0.91 | 0.91 | 188.1 | 208.7 | 1.11 |
| North: PACIFIC HWY | | | | | | | | | | | | |

| | | | | | | | | | | | |
|---------------------|-----|-----|------|-------|-----|-----|------|------|-------|-------|------|
| P3 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 231.4 | 223.8 | 0.97 |
| West: SYDNEY STREET | | | | | | | | | | | |
| P4 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 222.3 | 212.0 | 0.95 |
| All Pedestrians | 200 | 211 | 51.4 | LOS E | 0.2 | 0.2 | 0.94 | 0.94 | 218.3 | 217.1 | 0.99 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Project: T:\WORK21\21297 - LAKE MACQUARIE PRIVATE HOSPITAL - 3 SYDNEY ST, GATESHEAD\MODEL\PACIFIC HWY, SYDNEY STREET AND THE CRESCENT_2.sip9

**Site: 101 [PACIFIC HWY & SYDNEY ST/THE CRESCENT
EXISTING PM PEAK (Site Folder: General)]**

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 130 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|--------|---------------|--------|-----------|-------------|------------------|-------------------|----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV] % | [Total veh/h | HV] % | | | | [Veh. veh | Dist] m | | | | |
| South: PACIFIC HWY | | | | | | | | | | | | | | |
| 1 | L2 | 120 | 6.0 | 126 | 6.0 | 0.090 | 6.1 | LOS A | 0.5 | 3.9 | 0.12 | 0.58 | 0.12 | 47.9 |
| 2 | T1 | 880 | 6.0 | 926 | 6.0 | 0.715 | 34.9 | LOS C | 24.4 | 179.6 | 0.88 | 0.77 | 0.88 | 32.0 |
| 3 | R2 | 50 | 6.0 | 53 | 6.0 | 0.164 | 31.0 | LOS C | 1.8 | 13.3 | 0.85 | 0.73 | 0.85 | 31.0 |
| Approach | | 1050 | 6.0 | 1105 | 6.0 | 0.715 | 31.4 | LOS C | 24.4 | 179.6 | 0.79 | 0.75 | 0.79 | 33.2 |
| East: THE CRESCENT | | | | | | | | | | | | | | |
| 4 | L2 | 15 | 4.0 | 16 | 4.0 | * 0.102 | 32.0 | LOS C | 1.4 | 10.5 | 0.83 | 0.66 | 0.83 | 26.5 |
| 5 | T1 | 10 | 4.0 | 11 | 4.0 | 0.102 | 27.1 | LOS B | 1.4 | 10.5 | 0.83 | 0.66 | 0.83 | 30.0 |
| 6 | R2 | 10 | 4.0 | 11 | 4.0 | 0.102 | 30.4 | LOS C | 1.4 | 10.5 | 0.83 | 0.66 | 0.83 | 30.0 |
| Approach | | 35 | 4.0 | 37 | 4.0 | 0.102 | 30.1 | LOS C | 1.4 | 10.5 | 0.83 | 0.66 | 0.83 | 28.5 |
| North: PACIFIC HWY | | | | | | | | | | | | | | |
| 7 | L2 | 30 | 6.0 | 32 | 6.0 | 0.264 | 21.5 | LOS B | 5.8 | 42.9 | 0.70 | 0.61 | 0.70 | 39.3 |
| 8 | T1 | 1410 | 6.0 | 1484 | 6.0 | * 0.965 | 53.0 | LOS D | 45.8 | 337.4 | 0.94 | 1.05 | 1.25 | 25.8 |
| 9 | R2 | 60 | 6.0 | 63 | 6.0 | 0.118 | 26.3 | LOS B | 2.1 | 15.7 | 0.73 | 0.72 | 0.73 | 35.0 |
| Approach | | 1500 | 6.0 | 1579 | 6.0 | 0.965 | 51.3 | LOS D | 45.8 | 337.4 | 0.92 | 1.03 | 1.22 | 26.3 |
| West: SYDNEY STREET | | | | | | | | | | | | | | |
| 10 | L2 | 61 | 4.0 | 64 | 4.0 | 0.072 | 21.7 | LOS B | 2.1 | 15.2 | 0.55 | 0.64 | 0.55 | 33.4 |
| 11 | T1 | 20 | 4.0 | 21 | 4.0 | 0.567 | 50.0 | LOS D | 9.0 | 65.4 | 0.94 | 0.79 | 0.94 | 23.3 |
| 12 | R2 | 130 | 4.0 | 137 | 4.0 | 0.567 | 53.3 | LOS D | 9.0 | 65.4 | 0.94 | 0.79 | 0.94 | 21.8 |
| Approach | | 211 | 4.0 | 222 | 4.0 | 0.567 | 43.8 | LOS D | 9.0 | 65.4 | 0.83 | 0.75 | 0.83 | 24.5 |
| All Vehicles | | 2796 | 5.8 | 2943 | 5.8 | 0.965 | 43.0 | LOS D | 45.8 | 337.4 | 0.86 | 0.90 | 1.02 | 28.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

- * Critical Movement (Signal Timing)

| Pedestrian Movement Performance | | | | | | | | | | | | |
|---------------------------------|----------------|-----------|-------------|------------------|-----------------------|-----------|-----------|---------------------|-------------|--------------|-------------|-------|
| Mov ID | Input Crossing | Dem. Flow | Aver. Delay | Level of Service | AVERAGE BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Travel Time | Travel Dist. | Aver. Speed | |
| | | ped/h | ped/h | sec | | [Ped ped | Dist] m | | | sec | m | m/sec |
| South: PACIFIC HWY | | | | | | | | | | | | |
| P1 | Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 231.4 | 223.8 | 0.97 |
| East: THE CRESCENT | | | | | | | | | | | | |
| P2 | Full | 50 | 53 | 30.9 | LOS D | 0.1 | 0.1 | 0.91 | 0.91 | 191.5 | 208.7 | 1.09 |
| North: PACIFIC HWY | | | | | | | | | | | | |

| | | | | | | | | | | | |
|---------------------|-----|-----|------|-------|-----|-----|------|------|-------|-------|------|
| P3 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 231.4 | 223.8 | 0.97 |
| West: SYDNEY STREET | | | | | | | | | | | |
| P4 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 222.3 | 212.0 | 0.95 |
| All Pedestrians | 200 | 211 | 52.2 | LOS E | 0.2 | 0.2 | 0.94 | 0.94 | 219.2 | 217.1 | 0.99 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
 Pedestrian movement LOS values are based on average delay per pedestrian movement.
 Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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 Organisation: TRANSPORT AND TRAFFIC PLANNING ASSOCIATES | Licence: NETWORK / 1PC | Processed: Monday, 18 October 2021 4:55:33 PM
 Project: T:\WORK21\21297 - LAKE MACQUARIE PRIVATE HOSPITAL - 3 SYDNEY ST, GATESHEAD\MODEL\PACIFIC HWY, SYDNEY STREET AND THE CRESCENT_2.sip9

MOVEMENT SUMMARY

**Site: 101 [PACIFIC HWY & SYDNEY ST/THE CRESCENT
FUTURE AM PEAK (Site Folder: General)]**

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 130 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|--------|---------------|--------|-----------|-------------|------------------|-------------------|----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV] % | [Total veh/h | HV] % | | | | [Veh. veh | Dist] m | | | | |
| South: PACIFIC HWY | | | | | | | | | | | | | | |
| 1 | L2 | 120 | 6.0 | 126 | 6.0 | 0.092 | 6.6 | LOS A | 0.7 | 5.4 | 0.18 | 0.60 | 0.18 | 47.6 |
| 2 | T1 | 1320 | 6.0 | 1389 | 6.0 | * 0.927 | 55.1 | LOS D | 51.1 | 376.5 | 0.96 | 1.05 | 1.18 | 25.2 |
| 3 | R2 | 50 | 6.0 | 53 | 6.0 | 0.092 | 21.8 | LOS B | 1.6 | 11.9 | 0.61 | 0.69 | 0.61 | 35.4 |
| Approach | | 1490 | 6.0 | 1568 | 6.0 | 0.927 | 50.0 | LOS D | 51.1 | 376.5 | 0.89 | 1.00 | 1.08 | 26.5 |
| East: THE CRESCENT | | | | | | | | | | | | | | |
| 4 | L2 | 15 | 4.0 | 16 | 4.0 | * 0.156 | 38.7 | LOS C | 1.6 | 11.9 | 0.86 | 0.72 | 0.86 | 24.3 |
| 5 | T1 | 10 | 4.0 | 11 | 4.0 | 0.156 | 34.7 | LOS C | 1.6 | 11.9 | 0.86 | 0.72 | 0.86 | 27.4 |
| 6 | R2 | 20 | 4.0 | 21 | 4.0 | 0.156 | 38.0 | LOS C | 1.6 | 11.9 | 0.86 | 0.72 | 0.86 | 27.4 |
| Approach | | 45 | 4.0 | 47 | 4.0 | 0.156 | 37.5 | LOS C | 1.6 | 11.9 | 0.86 | 0.72 | 0.86 | 26.4 |
| North: PACIFIC HWY | | | | | | | | | | | | | | |
| 7 | L2 | 28 | 6.0 | 29 | 6.0 | * 0.148 | 25.3 | LOS B | 2.1 | 15.1 | 0.79 | 0.66 | 0.79 | 36.3 |
| 8 | T1 | 610 | 6.0 | 642 | 6.0 | 0.542 | 20.7 | LOS B | 9.5 | 70.0 | 0.87 | 0.73 | 0.87 | 39.4 |
| 9 | R2 | 130 | 6.0 | 137 | 6.0 | 0.491 | 44.6 | LOS D | 5.6 | 41.2 | 0.96 | 0.82 | 0.96 | 28.2 |
| Approach | | 768 | 6.0 | 808 | 6.0 | 0.542 | 24.9 | LOS B | 9.5 | 70.0 | 0.88 | 0.75 | 0.88 | 36.6 |
| West: SYDNEY STREET | | | | | | | | | | | | | | |
| 10 | L2 | 65 | 4.0 | 68 | 4.0 | 0.086 | 25.9 | LOS B | 2.5 | 18.0 | 0.61 | 0.66 | 0.61 | 31.7 |
| 11 | T1 | 10 | 4.0 | 11 | 4.0 | 0.614 | 53.0 | LOS D | 8.7 | 62.9 | 0.96 | 0.80 | 0.96 | 22.6 |
| 12 | R2 | 130 | 4.0 | 137 | 4.0 | 0.614 | 56.3 | LOS D | 8.7 | 62.9 | 0.96 | 0.80 | 0.96 | 21.2 |
| Approach | | 205 | 4.0 | 216 | 4.0 | 0.614 | 46.5 | LOS D | 8.7 | 62.9 | 0.85 | 0.76 | 0.85 | 23.9 |
| All Vehicles | | 2508 | 5.8 | 2640 | 5.8 | 0.927 | 41.8 | LOS C | 51.1 | 376.5 | 0.88 | 0.90 | 1.00 | 28.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

- * Critical Movement (Signal Timing)

| Pedestrian Movement Performance | | | | | | | | | | | |
|---------------------------------|----------------|-----------|-------------|------------------|-----------------------|-----------|-----------|---------------------|-------------|--------------|-------------|
| Mov ID | Input Crossing | Dem. Flow | Aver. Delay | Level of Service | AVERAGE BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Travel Time | Travel Dist. | Aver. Speed |
| | | ped/h | ped/h | sec | | [Ped ped | Dist] m | | | sec | m m/sec |
| South: PACIFIC HWY | | | | | | | | | | | |
| P1 | Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 231.4 | 223.8 0.97 |
| East: THE CRESCENT | | | | | | | | | | | |
| P2 | Full | 50 | 53 | 27.6 | LOS C | 0.1 | 0.1 | 0.91 | 0.91 | 188.1 | 208.7 1.11 |
| North: PACIFIC HWY | | | | | | | | | | | |

| | | | | | | | | | | | |
|---------------------|-----|-----|------|-------|-----|-----|------|------|-------|-------|------|
| P3 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 231.4 | 223.8 | 0.97 |
| West: SYDNEY STREET | | | | | | | | | | | |
| P4 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 222.3 | 212.0 | 0.95 |
| All | 200 | 211 | 51.4 | LOS E | 0.2 | 0.2 | 0.94 | 0.94 | 218.3 | 217.1 | 0.99 |
| Pedestrians | | | | | | | | | | | |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Project: T:\WORK\21\21297 - LAKE MACQUARIE PRIVATE HOSPITAL - 3 SYDNEY ST, GATESHEAD\MODEL\PACIFIC HWY, SYDNEY STREET AND THE CRESCENT_2.sip9

**Site: 101 [PACIFIC HWY & SYDNEY ST/THE CRESCENT
FUTURE PM PEAK (Site Folder: General)]**

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 130 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|--------|---------------|--------|-----------|-------------|------------------|-------------------|----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV] % | [Total veh/h | HV] % | | | | [Veh. veh | Dist] m | | | | |
| South: PACIFIC HWY | | | | | | | | | | | | | | |
| 1 | L2 | 130 | 6.0 | 137 | 6.0 | 0.099 | 6.3 | LOS A | 0.7 | 4.8 | 0.14 | 0.59 | 0.14 | 47.8 |
| 2 | T1 | 880 | 6.0 | 926 | 6.0 | 0.718 | 34.9 | LOS C | 24.6 | 180.8 | 0.88 | 0.77 | 0.88 | 32.0 |
| 3 | R2 | 50 | 6.0 | 53 | 6.0 | 0.163 | 31.0 | LOS C | 1.8 | 13.3 | 0.85 | 0.73 | 0.85 | 31.0 |
| Approach | | 1060 | 6.0 | 1116 | 6.0 | 0.718 | 31.2 | LOS C | 24.6 | 180.8 | 0.79 | 0.75 | 0.79 | 33.3 |
| East: THE CRESCENT | | | | | | | | | | | | | | |
| 4 | L2 | 15 | 4.0 | 16 | 4.0 | * 0.102 | 32.0 | LOS C | 1.4 | 10.5 | 0.83 | 0.66 | 0.83 | 26.5 |
| 5 | T1 | 10 | 4.0 | 11 | 4.0 | 0.102 | 27.1 | LOS B | 1.4 | 10.5 | 0.83 | 0.66 | 0.83 | 30.0 |
| 6 | R2 | 10 | 4.0 | 11 | 4.0 | 0.102 | 30.4 | LOS C | 1.4 | 10.5 | 0.83 | 0.66 | 0.83 | 30.0 |
| Approach | | 35 | 4.0 | 37 | 4.0 | 0.102 | 30.1 | LOS C | 1.4 | 10.5 | 0.83 | 0.66 | 0.83 | 28.5 |
| North: PACIFIC HWY | | | | | | | | | | | | | | |
| 7 | L2 | 30 | 6.0 | 32 | 6.0 | 0.266 | 21.5 | LOS B | 5.9 | 43.3 | 0.70 | 0.61 | 0.70 | 39.3 |
| 8 | T1 | 1410 | 6.0 | 1484 | 6.0 | * 0.973 | 56.3 | LOS D | 46.6 | 343.1 | 0.94 | 1.07 | 1.27 | 24.9 |
| 9 | R2 | 80 | 6.0 | 84 | 6.0 | 0.157 | 27.2 | LOS B | 2.9 | 21.5 | 0.75 | 0.74 | 0.75 | 34.6 |
| Approach | | 1520 | 6.0 | 1600 | 6.0 | 0.973 | 54.0 | LOS D | 46.6 | 343.1 | 0.92 | 1.04 | 1.24 | 25.5 |
| West: SYDNEY STREET | | | | | | | | | | | | | | |
| 10 | L2 | 80 | 4.0 | 84 | 4.0 | 0.095 | 21.9 | LOS B | 2.8 | 20.1 | 0.56 | 0.65 | 0.56 | 33.3 |
| 11 | T1 | 20 | 4.0 | 21 | 4.0 | 0.694 | 52.3 | LOS D | 10.9 | 78.9 | 0.96 | 0.84 | 1.01 | 22.8 |
| 12 | R2 | 154 | 4.0 | 162 | 4.0 | 0.694 | 55.6 | LOS D | 10.9 | 78.9 | 0.96 | 0.84 | 1.01 | 21.3 |
| Approach | | 254 | 4.0 | 267 | 4.0 | 0.694 | 44.7 | LOS D | 10.9 | 78.9 | 0.83 | 0.78 | 0.87 | 24.3 |
| All Vehicles | | 2869 | 5.8 | 3020 | 5.8 | 0.973 | 44.5 | LOS D | 46.6 | 343.1 | 0.86 | 0.91 | 1.03 | 27.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

- * Critical Movement (Signal Timing)

| Pedestrian Movement Performance | | | | | | | | | | | |
|---------------------------------|----------------|----------------|-------------|------------------|-----------------------|-----------|-----------|---------------------|-------------|--------------|-------------|
| Mov ID | Input Crossing | Dem. Flow Vol. | Aver. Delay | Level of Service | AVERAGE BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Travel Time | Travel Dist. | Aver. Speed |
| | | ped/h | ped/h | sec | | [Ped ped | Dist] m | | | sec | m m/sec |
| South: PACIFIC HWY | | | | | | | | | | | |
| P1 | Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 231.4 | 223.8 0.97 |
| East: THE CRESCENT | | | | | | | | | | | |
| P2 | Full | 50 | 53 | 30.9 | LOS D | 0.1 | 0.1 | 0.91 | 0.91 | 191.5 | 208.7 1.09 |
| North: PACIFIC HWY | | | | | | | | | | | |

| | | | | | | | | | | | |
|---------------------|-----|-----|------|-------|-----|-----|------|------|-------|-------|------|
| P3 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 231.4 | 223.8 | 0.97 |
| West: SYDNEY STREET | | | | | | | | | | | |
| P4 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 222.3 | 212.0 | 0.95 |
| All Pedestrians | 200 | 211 | 52.2 | LOS E | 0.2 | 0.2 | 0.94 | 0.94 | 219.2 | 217.1 | 0.99 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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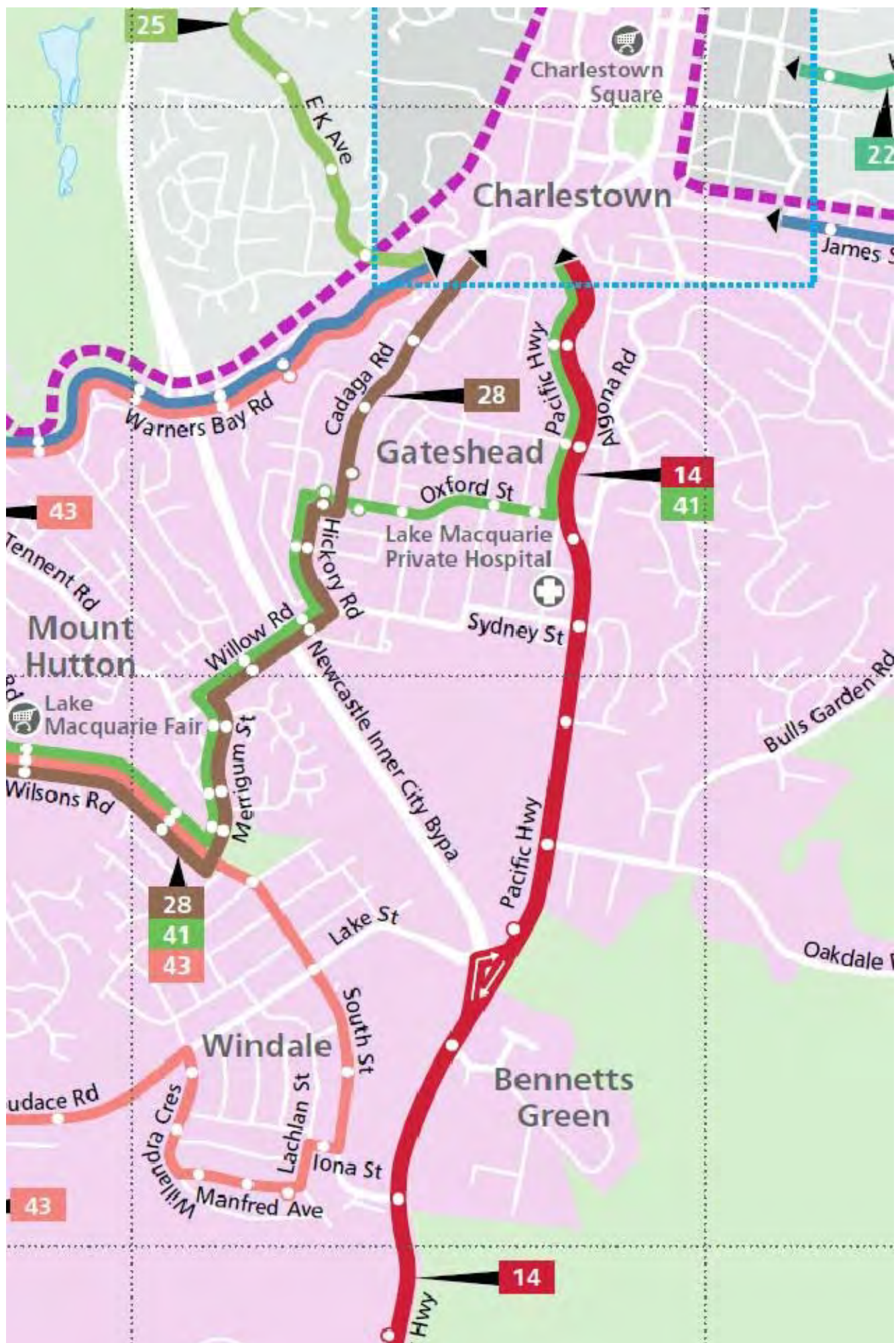
Organisation: TRANSPORT AND TRAFFIC PLANNING ASSOCIATES | Licence: NETWORK / 1PC | Processed: Monday, 18 October 2021 4:55:34 PM

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Appendix E

Bus Services

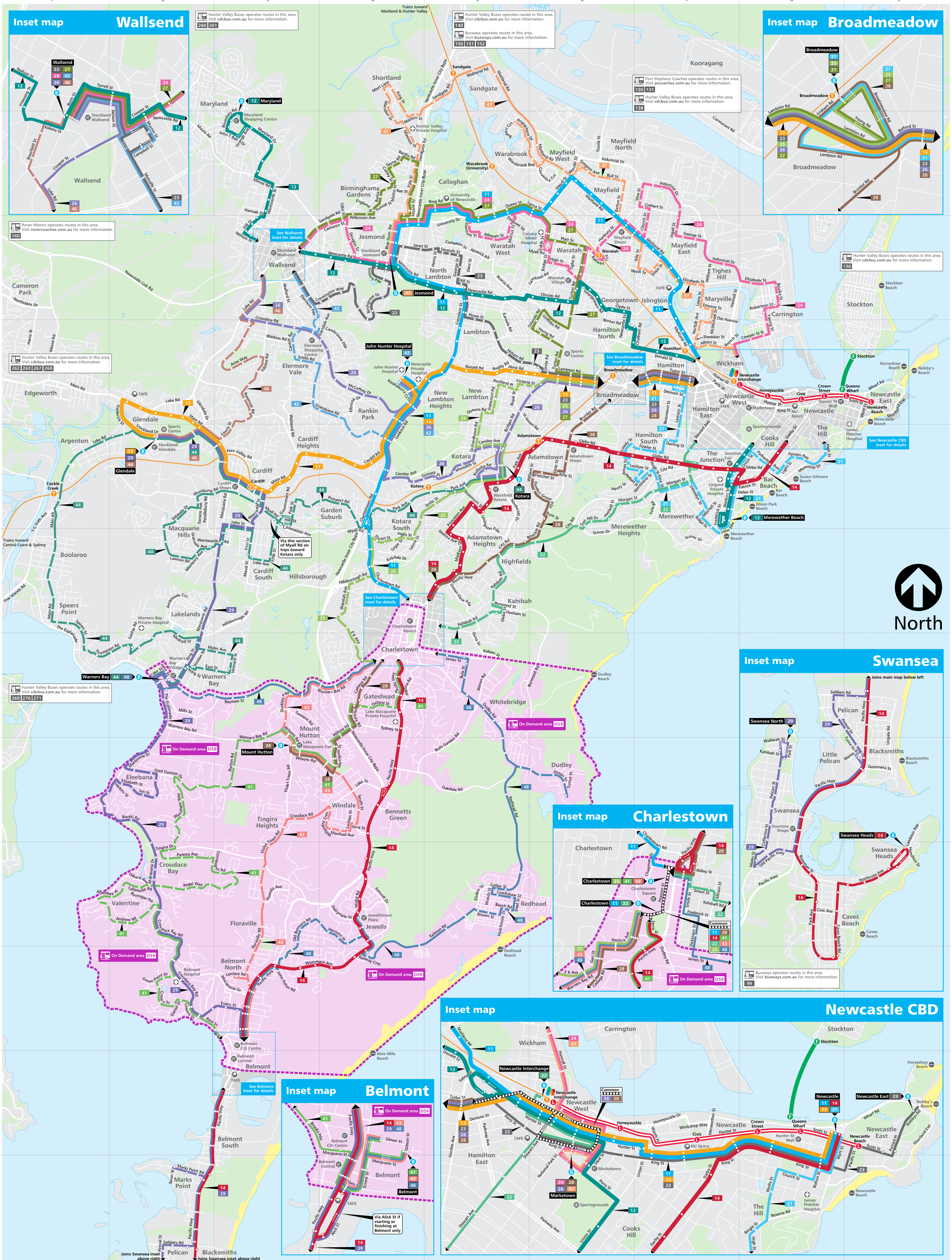




Legend

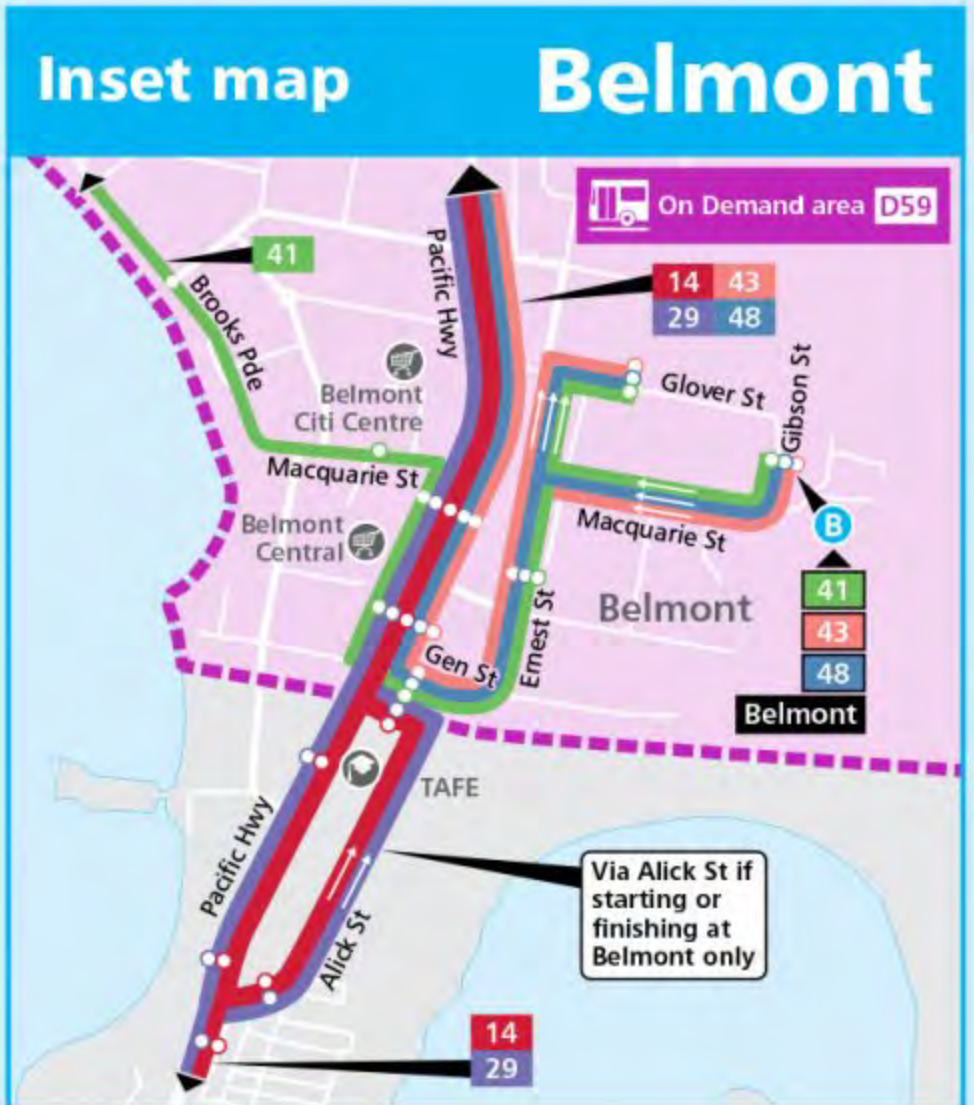
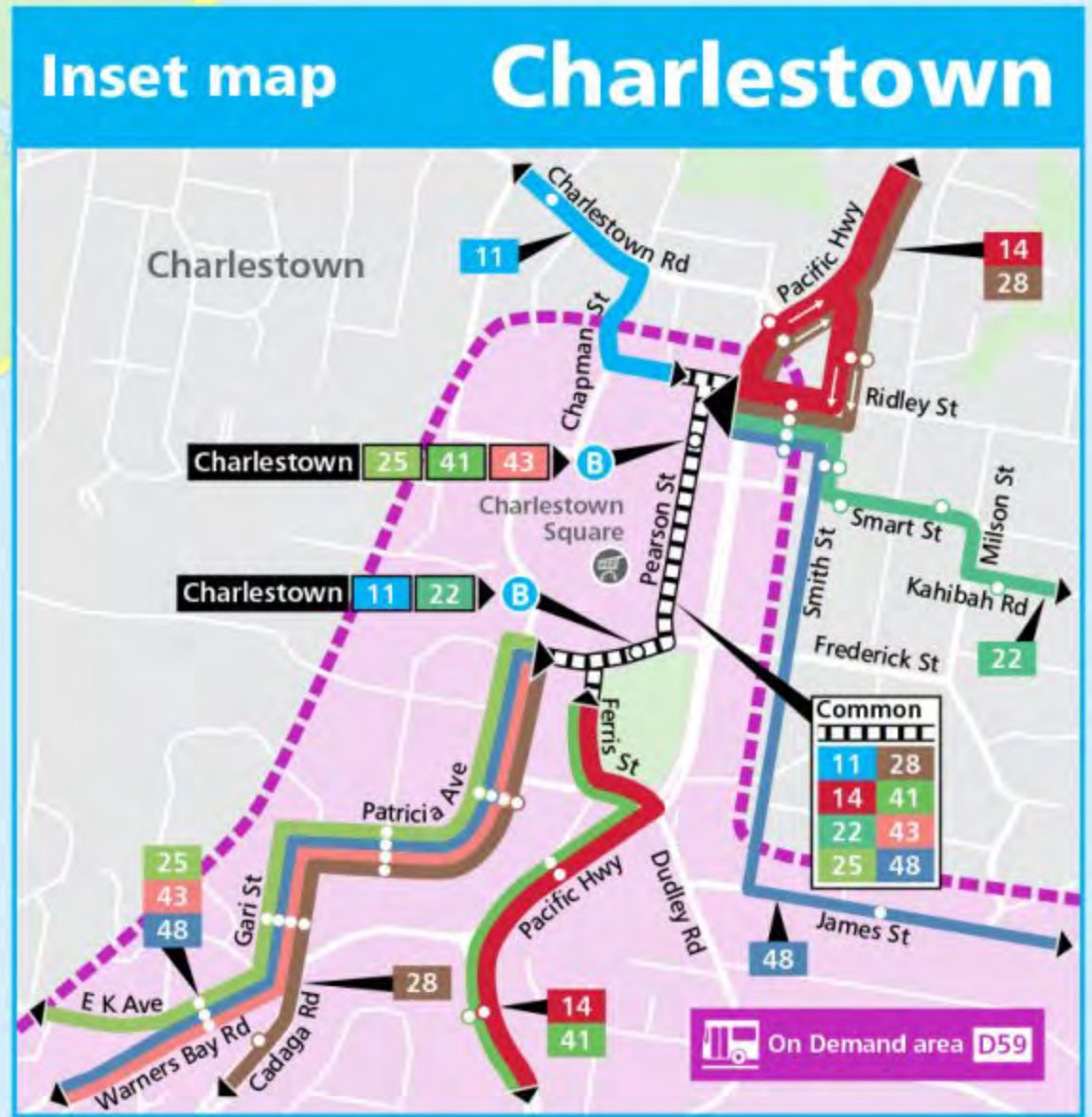
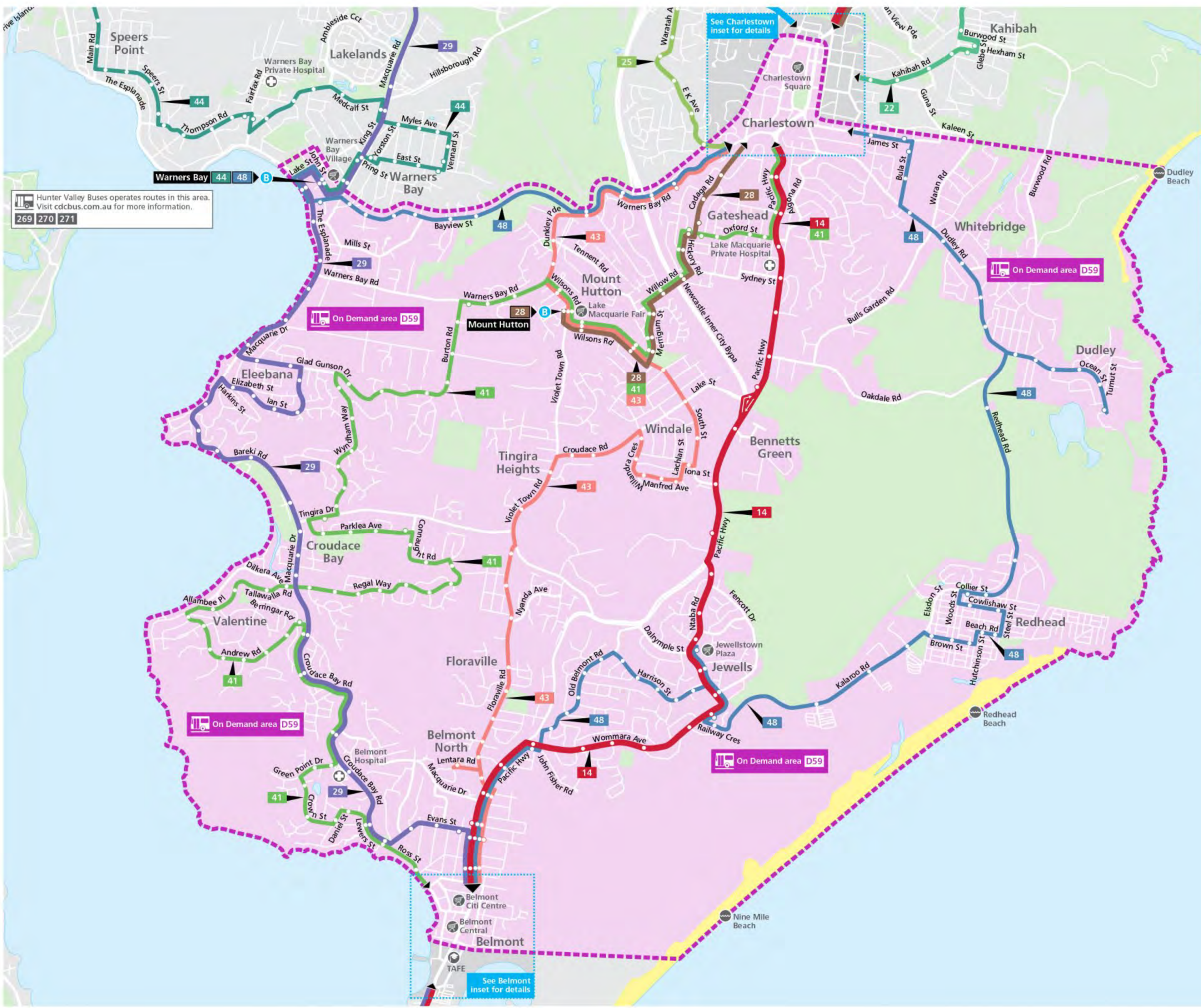
| | | | |
|---|---|---|---|
| — Frequent bus route | — Standard bus route | — Bus stop | 11 Bus route number |
| — Frequent bus route extension | — Tailored bus route | — Bus stop this side only | B Bus terminus |

Newcastle Transport network effective 13 December 2020



Newcastle Transport On Demand area

effective 30 June 2019



**COVID-19 Updates:**

A permit is required to travel between Greater Sydney and regional NSW, including Shellharbour and the Central Coast. Public transport services are running to a reduced timetable for Greater Sydney, including Intercity train services. [See latest travel information \(/covid-19/covid-19-safer-travel-guidance\)](#).



Lake Macquarie On Demand service



From 13 December, Lake Macquarie On Demand customers will be able to access Opal Connect, including travel credit. Opal Pay will no longer be available on these services from 1 April 2021. [Find out more about Opal Connect.](#)

The Lake Macquarie On Demand service area covers Charlestown, Dudley, Whitebridge, Gateshead, Redhead, Warners Bay, Mount Hutton, Windale, Tingira Heights, Eleebana, Croudace Bay, Valentine, Belmont North and Belmont areas.

From key activity centres such as Charlestown, Warners Bay, Mount Hutton and Belmont you can connect with bus routes to continue your journey beyond the On Demand area.

The On Demand service runs in addition to existing regular timetabled services. An On Demand bus will pick you up near your home or a convenient nearby location, and take you to where you want to go within the On Demand area.

The service is operated by Newcastle Transport and began Sunday 14 January 2018.

Find out more at newcastletransport.info.

Book via the app

To book, you can download the Newcastle Transport On Demand App from the [App Store](#) or [Google Play](#) and then log in with your [Opal Connect](#) credentials.

App store



Google Play



[Booking information](#)



[Another way to book](#)



Fares

A one-way trip is equivalent to [Opal peak and off-peak \(/tickets-opal/opal/fares-payments/opal-peak-off-peak-fares\)](#) bus fares.

Adult

| | |
|----------|----------|
| Distance | 0 - 3 km |
| Peak | \$3.20 |
| Off peak | \$2.24 |

| | |
|----------|----------|
| Distance | 3 - 8 km |
|----------|----------|

| | |
|----------|--------------|
| Peak | \$3.79 |
| Off peak | \$2.65 |
| Distance | 8+ km |
| Peak | \$4.87 |
| Off peak | \$3.40 |

Concession

Concession fare eligibility: concession card holders, including pensioners, seniors, students and apprentices.

| | |
|----------|-----------------|
| Distance | 0 - 3 km |
| Peak | \$1.60 |
| Off peak | \$1.12 |
| Distance | 3 - 8 km |
| Peak | \$1.89 |
| Off peak | \$1.32 |
| Distance | 8+ km |
| Peak | \$2.43 |
| Off peak | \$1.70 |

Hours of operation

Monday to Friday

9am-4pm

Saturday

7am-6pm

Sunday

9am-6pm

Sunday hours of operation will be in place on all public holidays.

What is travel credit?

With **Opal Connect**, you can earn up to **\$2 in travel credit** every time you transfer within 60 minutes between Opal and On Demand services.

You will need an Opal Connect account to start earning travel credit. [Sign up for an Opal Connect account](#) , link your Opal card and add a payment card. Get the Newcastle Transport On Demand app from the [App Store](#) or [Google Play](#) , or if you have it, make sure it is up-to-date. Then log in to the app using your Opal Connect account username and password to complete your setup

Once you've completed these steps, any travel credit you earn will be added to your Opal Connect account. When you have accumulated enough credit, you can use it to pay for your next On Demand trip.

For more details, see the [Opal Connect travel credit help page](#) ([/opal-connect-help](#)).

Map

The Lake Macquarie On Demand service area covers Dudley, Whitebridge, Mount Hutton, Windale, Tingira Heights, Eleebana, Warners Bay, Bennetts Green, Gateshead and Charlestown. From 30 June 2019 this area has been expanded to include Belmont, Belmont North, Croudace Bay, Valentine, Floraville, Jewells, and Redhead.

[Download the Newcastle Transport On Demand trial area map from June 30 2019 \(pdf 633KB\) \(/document/4214/lake-macquarie-on-demand-map-20190630.pdf\)](#)



Share



Tweet

[✉ \(mailto:?subject=Lake%20Macquarie%20On%20Demand%20service&body=I would like to share something with you%0D%0A%0D%0Ahttp%3A%2F%2Ftransportnsw.gov.au%2Ftravel-credit\)](mailto:?subject=Lake%20Macquarie%20On%20Demand%20service&body=I%20would%20like%20to%20share%20something%20with%20you%20D%20A%20D%20A%20http%3A%2F%2Ftransportnsw.gov.au%2Ftravel-credit)

How to use this timetable

This timetable provides a snapshot of service information in 24-hour time (e.g. 5am = 05:00, 5pm = 17:00). Information contained in this timetable is subject to change without notice. Please note that timetables do not include minor stops, additional trips for special events, short term changes, holiday timetable changes, real-time information or any disruption alerts.

For the most up-to-date times, use the Trip Planner or Departures at transportnsw.info

Real-time planning


You can plan your trip with real-time information using the Trip Planner or Departures at transportnsw.info or by downloading travel apps on your smartphone or tablet.

The Trip Planner, Departures and travel apps offer various features:

- favourite your regular trips
- see where your service is on the route
- get estimated pick-up and arrival times
- receive service updates
- find nearby stations, stops, wharves and routes
- check accessibility information.

Find the latest apps at transportnsw.info/apps

Accessible services

All new buses are wheelchair-accessible with low-level floors and space for wheelchairs, prams or strollers. Look for the  symbol in this timetable. Some older buses may not have all the features you need. There will be more accessible services as older buses are replaced.

Who is providing my bus services?

The bus services shown in this timetable are run by Newcastle Transport.

Fares

In Sydney and surrounding regions, fares are based on:

- the distance you travel from tap on to tap off
- the mode of transport you choose
- whether you're eligible for a concession fare or free travel
- any Opal benefits such as discounts and capped fares that apply.

You can use an Opal card or a contactless payment to pay for your travel.

Opal cards

An Opal card is a smartcard you keep and reuse. Add value before you travel, and tap on and tap off to pay your fares throughout Sydney, the Blue Mountains, the Central Coast, the Hunter and the Illawarra.

Which Opal card is right for you?

Adult – Customers 16 years or older who are not entitled to any concessions and normally pay full fare.

Child/Youth – For customers aged 4-15 (inclusive), or customers 16 years or older who hold a NSW/ACT Senior Secondary Student Concession Card.

Gold Senior/Pensioner – For eligible NSW and interstate seniors, pensioners, war widows/ers and asylum seekers.

Concession – For eligible tertiary students, job seekers, apprentices and trainees.

How to get an Opal card

You can get an Adult or Child/Youth Opal card over the counter at Opal retailers that display the Opal sign . To find your nearest retailer visit transportnsw.info/opal.

If you are eligible to travel with concession fares, you can apply for a Gold Senior/Pensioner or Concession Opal card online. Visit transportnsw.info/opal for more information.

Contactless payments

If you have an American Express, Mastercard, Visa card or linked device, you can use it to pay for all public transport on the Opal network. Just make sure to tap on and tap off at Opal readers at the beginning and end of your trip.

Always separate your cards when you tap on and tap off so your preferred card is charged.

You will receive the same travel benefits of an Adult Opal card when you tap on and tap off consistently with the same credit card, debit card or linked device. This includes daily, weekly and weekend travel caps, and a \$2 transfer discount when you change between metro/train, ferry, bus and light rail services within 60 minutes. Adult Opal fare pricing applies.

Find out more at transportnsw.info/contactless

Explanation of definitions and symbols



Wheelchair Accessible

F

Friday only

C

Operates Early Saturday morning only

Valid from: 12 July 2021

Creation date: 15 Oct 2021

NOTE: Information is correct on date of download.

| Monday to Friday | | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Customs House, Watt St, Newcastle | 05:17 | 05:47 | 06:10 | 06:29 | 06:56 | 07:14 | 07:29 | 07:44 | 07:59 |
| Darby St before Bull St, Cooks Hill | 05:23 | 05:53 | 06:16 | 06:35 | 07:02 | 07:20 | 07:35 | 07:50 | 08:05 |
| Junction Fair, Glebe Rd, The Junction | 05:29 | 05:59 | 06:22 | 06:41 | 07:08 | 07:27 | 07:42 | 07:57 | 08:12 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 05:36 | 06:06 | 06:29 | 06:48 | 07:15 | 07:34 | 07:49 | 08:04 | 08:19 |
| Westfield Kotara, Park Ave, Kotara | 05:41 | 06:11 | 06:34 | 06:53 | 07:20 | 07:39 | 07:54 | 08:09 | 08:24 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 05:50 | 06:20 | 06:44 | 07:03 | 07:30 | 07:51 | 08:05 | 08:20 | 08:34 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 05:51 | 06:21 | 06:45 | 07:04 | 07:31 | 07:52 | 08:08 | 08:21 | 08:36 |
| Pacific Hwy after Oxford St, Gateshead | 05:56 | 06:26 | 06:50 | 07:09 | 07:37 | 07:58 | - | 08:28 | - |
| Jewells Plaza, Ntaba Rd, Jewells | 06:02 | 06:32 | 06:57 | 07:16 | 07:45 | 08:06 | - | 08:36 | - |
| Pacific Hwy at Cobbin Pde, Belmont | 06:07 | 06:37 | 07:02 | 07:21 | 07:52 | 08:12 | - | 08:42 | - |
| Pacific Hwy opp Macquarie St, Belmont | 06:10 | 06:40 | 07:05 | 07:24 | 07:55 | 08:15 | - | 08:45 | - |
| Pacific Hwy opp Marks Point Rd, Marks Point | 06:14 | 06:44 | - | 07:28 | 08:00 | 08:20 | - | 08:50 | - |
| Bowman St opp Lake Rd, Swansea | 06:20 | 06:50 | - | 07:34 | 08:07 | 08:26 | - | 08:56 | - |
| Park Ave opp Swansea High School, Caves Beach | 06:23 | 06:53 | - | 07:38 | 08:11 | 08:30 | - | 09:00 | - |
| Lambton Pde at Hamilton St, Swansea Heads | 06:30 | 07:00 | - | 07:45 | 08:18 | 08:37 | - | 09:07 | - |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | 07:07 | - | - | - | - | - | - |
| Monday to Friday | | | | | | | | | |
| Customs House, Watt St, Newcastle | 08:14 | 08:27 | 08:42 | 08:54 | 09:09 | 09:24 | 09:39 | 09:54 | 10:09 |
| Darby St before Bull St, Cooks Hill | 08:20 | 08:33 | 08:48 | 09:00 | 09:15 | 09:30 | 09:45 | 10:00 | 10:15 |
| Junction Fair, Glebe Rd, The Junction | 08:27 | 08:40 | 08:55 | 09:07 | 09:22 | 09:37 | 09:52 | 10:07 | 10:22 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 08:34 | 08:47 | 09:02 | 09:14 | 09:29 | 09:44 | 09:59 | 10:14 | 10:29 |
| Westfield Kotara, Park Ave, Kotara | 08:39 | 08:52 | 09:07 | 09:19 | 09:34 | 09:49 | 10:04 | 10:19 | 10:34 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 08:50 | 09:03 | 09:17 | 09:29 | 09:43 | 09:59 | 10:14 | 10:29 | 10:43 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 08:53 | 09:04 | 09:19 | 09:31 | 09:44 | 10:01 | 10:15 | 10:31 | 10:44 |
| Pacific Hwy after Oxford St, Gateshead | - | 09:11 | - | - | 09:51 | - | 10:21 | - | 10:51 |
| Jewells Plaza, Ntaba Rd, Jewells | - | 09:19 | - | - | 09:58 | - | 10:28 | - | 10:58 |
| Pacific Hwy at Cobbin Pde, Belmont | - | 09:25 | - | - | 10:04 | - | 10:34 | - | 11:04 |
| Pacific Hwy opp Macquarie St, Belmont | - | 09:28 | - | - | 10:07 | - | 10:37 | - | 11:07 |
| Pacific Hwy opp Marks Point Rd, Marks Point | - | 09:33 | - | - | 10:12 | - | - | - | 11:12 |
| Bowman St opp Lake Rd, Swansea | - | 09:39 | - | - | 10:18 | - | - | - | 11:18 |
| Park Ave opp Swansea High School, Caves Beach | - | 09:43 | - | - | 10:22 | - | - | - | 11:22 |
| Lambton Pde at Hamilton St, Swansea Heads | - | 09:50 | - | - | 10:29 | - | - | - | 11:29 |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | - | - | - | - | 10:39 | - | - |

| Monday to Friday | | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Customs House, Watt St, Newcastle | 10:24 | 10:39 | 10:54 | 11:09 | 11:24 | 11:39 | 11:54 | 12:09 | 12:24 |
| Darby St before Bull St, Cooks Hill | 10:30 | 10:45 | 11:00 | 11:15 | 11:30 | 11:45 | 12:00 | 12:15 | 12:30 |
| Junction Fair, Glebe Rd, The Junction | 10:37 | 10:52 | 11:07 | 11:22 | 11:37 | 11:52 | 12:07 | 12:22 | 12:37 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 10:44 | 10:59 | 11:14 | 11:29 | 11:44 | 11:59 | 12:14 | 12:29 | 12:44 |
| Westfield Kotara, Park Ave, Kotara | 10:49 | 11:04 | 11:19 | 11:34 | 11:49 | 12:04 | 12:19 | 12:34 | 12:49 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 10:59 | 11:14 | 11:29 | 11:43 | 11:59 | 12:14 | 12:29 | 12:44 | 12:59 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 11:01 | 11:15 | 11:31 | 11:44 | 12:01 | 12:15 | 12:31 | 12:45 | 13:01 |
| Pacific Hwy after Oxford St, Gateshead | - | 11:21 | - | 11:51 | - | 12:21 | - | 12:51 | - |
| Jewells Plaza, Ntaba Rd, Jewells | - | 11:28 | - | 11:58 | - | 12:28 | - | 12:58 | - |
| Pacific Hwy at Cobbin Pde, Belmont | - | 11:34 | - | 12:04 | - | 12:34 | - | 13:04 | - |
| Pacific Hwy opp Macquarie St, Belmont | - | 11:37 | - | 12:07 | - | 12:37 | - | 13:07 | - |
| Pacific Hwy opp Marks Point Rd, Marks Point | - | - | - | 12:12 | - | - | - | 13:12 | - |
| Bowman St opp Lake Rd, Swansea | - | - | - | 12:18 | - | - | - | 13:18 | - |
| Park Ave opp Swansea High School, Caves Beach | - | - | - | 12:22 | - | - | - | 13:22 | - |
| Lambton Pde at Hamilton St, Swansea Heads | - | - | - | 12:29 | - | - | - | 13:29 | - |
| Alick St opp Spinnakers Leisure Park, Belmont | - | 11:39 | - | - | - | 12:39 | - | - | - |
| Monday to Friday | | | | | | | | | |
| Customs House, Watt St, Newcastle | 12:39 | 12:54 | 13:09 | 13:24 | 13:39 | 13:54 | 14:09 | 14:24 | 14:39 |
| Darby St before Bull St, Cooks Hill | 12:45 | 13:00 | 13:15 | 13:30 | 13:45 | 14:00 | 14:15 | 14:30 | 14:45 |
| Junction Fair, Glebe Rd, The Junction | 12:52 | 13:07 | 13:22 | 13:37 | 13:52 | 14:07 | 14:22 | 14:37 | 14:52 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 12:59 | 13:14 | 13:29 | 13:44 | 13:59 | 14:14 | 14:29 | 14:44 | 14:59 |
| Westfield Kotara, Park Ave, Kotara | 13:04 | 13:19 | 13:34 | 13:49 | 14:04 | 14:19 | 14:34 | 14:49 | 15:04 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 13:14 | 13:29 | 13:43 | 13:59 | 14:14 | 14:29 | 14:44 | 14:58 | 15:15 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 13:15 | 13:31 | 13:44 | 14:01 | 14:15 | 14:31 | 14:46 | 14:59 | 15:16 |
| Pacific Hwy after Oxford St, Gateshead | 13:21 | - | 13:51 | - | 14:21 | - | - | 15:06 | 15:22 |
| Jewells Plaza, Ntaba Rd, Jewells | 13:28 | - | 13:58 | - | 14:28 | - | - | 15:13 | 15:32 |
| Pacific Hwy at Cobbin Pde, Belmont | 13:34 | - | 14:04 | - | 14:34 | - | - | 15:19 | 15:38 |
| Pacific Hwy opp Macquarie St, Belmont | 13:37 | - | 14:07 | - | 14:37 | - | - | 15:22 | 15:41 |
| Pacific Hwy opp Marks Point Rd, Marks Point | - | - | 14:12 | - | - | - | - | 15:27 | 15:46 |
| Bowman St opp Lake Rd, Swansea | - | - | 14:18 | - | - | - | - | 15:33 | 15:52 |
| Park Ave opp Swansea High School, Caves Beach | - | - | 14:22 | - | - | - | - | 15:37 | 15:56 |
| Lambton Pde at Hamilton St, Swansea Heads | - | - | 14:29 | - | - | - | - | 15:44 | 16:03 |
| Alick St opp Spinnakers Leisure Park, Belmont | 13:39 | - | - | - | 14:39 | - | - | - | - |
| Monday to Friday | | | | | | | | | |
| Customs House, Watt St, Newcastle | 14:54 | 15:09 | 15:24 | 15:39 | 15:54 | 16:09 | 16:24 | 16:39 | 16:54 |
| Darby St before Bull St, Cooks Hill | 15:01 | 15:15 | 15:30 | 15:45 | 16:00 | 16:15 | 16:30 | 16:45 | 17:00 |
| Junction Fair, Glebe Rd, The Junction | 15:09 | 15:22 | 15:37 | 15:52 | 16:07 | 16:22 | 16:37 | 16:52 | 17:07 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 15:16 | 15:29 | 15:44 | 15:58 | 16:13 | 16:28 | 16:43 | 16:58 | 17:13 |
| Westfield Kotara, Park Ave, Kotara | 15:21 | 15:34 | 15:49 | 16:03 | 16:18 | 16:33 | 16:48 | 17:03 | 17:18 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 15:33 | 15:44 | 15:58 | 16:13 | 16:28 | 16:43 | 16:58 | 17:12 | 17:28 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 15:34 | 15:46 | 15:59 | 16:15 | 16:29 | 16:45 | 17:00 | 17:13 | 17:30 |
| Pacific Hwy after Oxford St, Gateshead | 15:40 | - | 16:06 | - | 16:35 | - | - | 17:19 | - |
| Jewells Plaza, Ntaba Rd, Jewells | 15:49 | - | 16:13 | - | 16:42 | - | - | 17:27 | - |
| Pacific Hwy at Cobbin Pde, Belmont | 15:55 | - | 16:19 | - | 16:48 | - | - | 17:33 | - |
| Pacific Hwy opp Macquarie St, Belmont | 15:58 | - | 16:22 | - | 16:51 | - | - | 17:36 | - |
| Pacific Hwy opp Marks Point Rd, Marks Point | - | - | 16:27 | - | 16:56 | - | - | 17:41 | - |
| Bowman St opp Lake Rd, Swansea | - | - | 16:33 | - | 17:03 | - | - | 17:48 | - |
| Park Ave opp Swansea High School, Caves Beach | - | - | 16:37 | - | 17:07 | - | - | 17:52 | - |
| Lambton Pde at Hamilton St, Swansea Heads | - | - | 16:44 | - | 17:14 | - | - | 17:59 | - |
| Alick St opp Spinnakers Leisure Park, Belmont | 16:00 | - | - | - | - | - | - | - | - |

| Monday to Friday | | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Customs House, Watt St, Newcastle | 17:09 | 17:24 | 17:32 | 17:47 | 18:02 | 18:17 | 18:32 | 18:47 | 19:02 |
| Darby St before Bull St, Cooks Hill | 17:17 | 17:32 | 17:39 | 17:53 | 18:11 | 18:23 | 18:38 | 18:52 | 19:07 |
| Junction Fair, Glebe Rd, The Junction | 17:25 | 17:39 | 17:46 | 17:59 | 18:19 | 18:29 | 18:44 | 18:58 | 19:13 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 17:32 | 17:46 | 17:53 | 18:06 | 18:27 | 18:36 | 18:51 | 19:05 | 19:20 |
| Westfield Kotara, Park Ave, Kotara | 17:37 | 17:50 | 17:58 | 18:11 | 18:31 | 18:41 | 18:56 | 19:09 | 19:24 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 17:46 | 18:00 | 18:08 | 18:21 | 18:42 | 18:51 | 19:05 | 19:18 | 19:33 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 17:47 | 18:01 | 18:09 | 18:21 | 18:44 | 18:52 | 19:06 | 19:20 | 19:35 |
| Pacific Hwy after Oxford St, Gateshead | 17:54 | 18:06 | - | 18:26 | - | - | 19:11 | - | - |
| Jewells Plaza, Ntaba Rd, Jewells | 18:02 | 18:11 | - | 18:31 | - | - | 19:16 | - | - |
| Pacific Hwy at Cobbin Pde, Belmont | 18:08 | 18:16 | - | 18:36 | - | - | 19:21 | - | - |
| Pacific Hwy opp Macquarie St, Belmont | 18:11 | 18:19 | - | 18:39 | - | - | 19:24 | - | - |
| Pacific Hwy opp Marks Point Rd, Marks Point | 18:16 | 18:23 | - | 18:43 | - | - | 19:28 | - | - |
| Bowman St opp Lake Rd, Swansea | 18:22 | 18:29 | - | 18:49 | - | - | 19:34 | - | - |
| Park Ave opp Swansea High School, Caves Beach | 18:26 | 18:32 | - | 18:53 | - | - | 19:37 | - | - |
| Lambton Pde at Hamilton St, Swansea Heads | 18:32 | 18:39 | - | 18:59 | - | - | 19:44 | - | - |

| Monday to Friday | | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|--------|
| Day Restrictions | | | | | | | | | F |
| Customs House, Watt St, Newcastle | 19:29 | 19:59 | 20:29 | 20:59 | 21:34 | 21:59 | 22:29 | 23:29 | C01:05 |
| Darby St before Bull St, Cooks Hill | 19:34 | 20:04 | 20:34 | 21:04 | 21:39 | 22:04 | 22:34 | 23:34 | C01:09 |
| Junction Fair, Glebe Rd, The Junction | 19:40 | 20:10 | 20:40 | 21:10 | 21:45 | 22:10 | 22:40 | 23:40 | C01:13 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 19:47 | 20:17 | 20:47 | 21:17 | 21:52 | 22:17 | 22:47 | 23:47 | C01:18 |
| Westfield Kotara, Park Ave, Kotara | 19:51 | 20:21 | 20:51 | 21:21 | 21:56 | 22:21 | 22:51 | 23:51 | C01:22 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 20:01 | 20:30 | 21:01 | 21:31 | 22:05 | 22:30 | 23:00 | 00:01 | C01:29 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 20:01 | 20:32 | 21:01 | 21:32 | 22:06 | 22:32 | 23:01 | 00:01 | C01:29 |
| Pacific Hwy after Oxford St, Gateshead | 20:06 | - | 21:06 | - | 22:11 | - | 23:06 | 00:06 | C01:34 |
| Jewells Plaza, Ntaba Rd, Jewells | 20:11 | - | 21:11 | - | 22:16 | - | 23:11 | 00:11 | C01:39 |
| Pacific Hwy at Cobbin Pde, Belmont | 20:16 | - | 21:16 | - | 22:21 | - | 23:17 | 00:16 | C01:44 |
| Pacific Hwy opp Macquarie St, Belmont | 20:18 | - | 21:18 | - | 22:23 | - | 23:18 | 00:18 | C01:46 |
| Pacific Hwy opp Marks Point Rd, Marks Point | 20:22 | - | 21:22 | - | 22:27 | - | - | - | C01:49 |
| Bowman St opp Lake Rd, Swansea | 20:28 | - | 21:28 | - | 22:33 | - | - | - | C01:53 |
| Park Ave opp Swansea High School, Caves Beach | 20:31 | - | 21:31 | - | 22:36 | - | - | - | C01:56 |
| Lambton Pde at Hamilton St, Swansea Heads | 20:38 | - | 21:38 | - | 22:43 | - | - | - | C02:01 |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | - | - | - | - | 23:19 | 00:19 | - |

| Monday to Friday | | | | | | | | | |
|--|--------|--------|--|--|--|--|--|--|--|
| | F | F | | | | | | | |
| Customs House, Watt St, Newcastle | C02:05 | C03:05 | | | | | | | |
| Darby St before Bull St, Cooks Hill | C02:09 | C03:09 | | | | | | | |
| Junction Fair, Glebe Rd, The Junction | C02:13 | C03:13 | | | | | | | |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | C02:18 | C03:18 | | | | | | | |
| Westfield Kotara, Park Ave, Kotara | C02:22 | C03:22 | | | | | | | |
| Charlestown Square, Pearson St, Stand B, Charlestown | C02:29 | C03:29 | | | | | | | |
| Charlestown Square, Frederick St, Stand D, Charlestown | C02:29 | C03:29 | | | | | | | |
| Pacific Hwy after Oxford St, Gateshead | C02:34 | C03:34 | | | | | | | |
| Jewells Plaza, Ntaba Rd, Jewells | C02:39 | C03:39 | | | | | | | |
| Pacific Hwy at Cobbin Pde, Belmont | C02:44 | C03:44 | | | | | | | |
| Pacific Hwy opp Macquarie St, Belmont | C02:46 | C03:46 | | | | | | | |
| Pacific Hwy opp Marks Point Rd, Marks Point | C02:49 | C03:49 | | | | | | | |
| Bowman St opp Lake Rd, Swansea | C02:53 | C03:53 | | | | | | | |
| Park Ave opp Swansea High School, Caves Beach | C02:56 | C03:56 | | | | | | | |
| Lambton Pde at Hamilton St, Swansea Heads | C03:01 | C04:01 | | | | | | | |

| Saturday | | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Customs House, Watt St, Newcastle | 05:10 | 06:10 | 06:40 | 07:10 | 07:40 | 08:10 | 08:40 | 09:10 | 09:40 |
| Darby St before Bull St, Cooks Hill | 05:15 | 06:15 | 06:45 | 07:15 | 07:46 | 08:16 | 08:46 | 09:16 | 09:46 |
| Junction Fair, Glebe Rd, The Junction | 05:20 | 06:20 | 06:52 | 07:21 | 07:52 | 08:22 | 08:52 | 09:22 | 09:52 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 05:26 | 06:26 | 06:58 | 07:27 | 07:59 | 08:29 | 09:00 | 09:30 | 10:00 |
| Westfield Kotara, Park Ave, Kotara | 05:30 | 06:30 | 07:03 | 07:31 | 08:03 | 08:33 | 09:05 | 09:35 | 10:05 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 05:39 | 06:39 | 07:12 | 07:40 | 08:12 | 08:42 | 09:15 | 09:44 | 10:15 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 05:40 | 06:40 | 07:13 | 07:41 | 08:13 | 08:43 | 09:16 | 09:45 | 10:16 |
| Pacific Hwy after Oxford St, Gateshead | 05:45 | 06:45 | 07:18 | 07:46 | 08:19 | 08:50 | 09:22 | 09:52 | 10:22 |
| Jewells Plaza, Ntaba Rd, Jewells | 05:51 | 06:51 | 07:24 | 07:52 | 08:25 | 08:56 | 09:29 | 09:59 | 10:29 |
| Pacific Hwy at Cobbin Pde, Belmont | 05:56 | 06:56 | 07:29 | 07:57 | 08:31 | 09:02 | 09:35 | 10:04 | 10:35 |
| Pacific Hwy opp Macquarie St, Belmont | 05:59 | 06:59 | 07:32 | 08:00 | 08:34 | 09:05 | 09:38 | 10:08 | 10:38 |
| Pacific Hwy opp Marks Point Rd, Marks Point | - | - | 07:36 | - | 08:39 | - | 09:43 | - | 10:43 |
| Bowman St opp Lake Rd, Swansea | - | - | 07:42 | - | 08:45 | - | 09:49 | - | 10:49 |
| Park Ave opp Swansea High School, Caves Beach | - | - | 07:46 | - | 08:49 | - | 09:53 | - | 10:53 |
| Lambton Pde at Hamilton St, Swansea Heads | - | - | 07:53 | - | 08:56 | - | 10:00 | - | 11:00 |
| Alick St opp Spinnakers Leisure Park, Belmont | 06:02 | 07:02 | - | 08:03 | - | 09:08 | - | 10:11 | - |

| Saturday | | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Customs House, Watt St, Newcastle | 10:10 | 10:40 | 11:10 | 11:40 | 12:10 | 12:40 | 13:10 | 13:40 | 14:10 |
| Darby St before Bull St, Cooks Hill | 10:16 | 10:46 | 11:16 | 11:46 | 12:16 | 12:46 | 13:16 | 13:46 | 14:16 |
| Junction Fair, Glebe Rd, The Junction | 10:22 | 10:52 | 11:22 | 11:52 | 12:22 | 12:52 | 13:22 | 13:52 | 14:22 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 10:30 | 11:00 | 11:30 | 12:00 | 12:30 | 13:00 | 13:30 | 14:00 | 14:30 |
| Westfield Kotara, Park Ave, Kotara | 10:35 | 11:05 | 11:35 | 12:05 | 12:35 | 13:05 | 13:35 | 14:05 | 14:35 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 10:45 | 11:15 | 11:45 | 12:15 | 12:45 | 13:15 | 13:45 | 14:15 | 14:45 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 10:46 | 11:16 | 11:46 | 12:16 | 12:46 | 13:16 | 13:46 | 14:16 | 14:46 |
| Pacific Hwy after Oxford St, Gateshead | 10:52 | 11:22 | 11:52 | 12:22 | 12:52 | 13:22 | 13:52 | 14:23 | 14:53 |
| Jewells Plaza, Ntaba Rd, Jewells | 10:59 | 11:29 | 11:59 | 12:29 | 12:59 | 13:29 | 13:59 | 14:30 | 15:00 |
| Pacific Hwy at Cobbin Pde, Belmont | 11:04 | 11:35 | 12:04 | 12:35 | 13:04 | 13:35 | 14:04 | 14:36 | 15:05 |
| Pacific Hwy opp Macquarie St, Belmont | 11:08 | 11:38 | 12:08 | 12:38 | 13:08 | 13:38 | 14:08 | 14:39 | 15:09 |
| Pacific Hwy opp Marks Point Rd, Marks Point | - | 11:43 | - | 12:43 | - | 13:43 | - | 14:44 | - |
| Bowman St opp Lake Rd, Swansea | - | 11:49 | - | 12:49 | - | 13:49 | - | 14:50 | - |
| Park Ave opp Swansea High School, Caves Beach | - | 11:53 | - | 12:53 | - | 13:53 | - | 14:54 | - |
| Lambton Pde at Hamilton St, Swansea Heads | - | 12:00 | - | 13:00 | - | 14:00 | - | 15:01 | - |
| Alick St opp Spinnakers Leisure Park, Belmont | 11:11 | - | 12:11 | - | 13:11 | - | 14:11 | - | 15:12 |

| Saturday | | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Customs House, Watt St, Newcastle | 14:40 | 15:10 | 15:40 | 16:10 | 16:40 | 17:10 | 17:40 | 18:10 | 18:40 |
| Darby St before Bull St, Cooks Hill | 14:46 | 15:16 | 15:47 | 16:16 | 16:46 | 17:16 | 17:46 | 18:16 | 18:46 |
| Junction Fair, Glebe Rd, The Junction | 14:52 | 15:22 | 15:53 | 16:22 | 16:52 | 17:22 | 17:52 | 18:22 | 18:52 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 15:00 | 15:30 | 16:00 | 16:29 | 16:59 | 17:29 | 17:59 | 18:29 | 18:58 |
| Westfield Kotara, Park Ave, Kotara | 15:05 | 15:35 | 16:05 | 16:34 | 17:04 | 17:34 | 18:04 | 18:34 | 19:03 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 15:15 | 15:45 | 16:14 | 16:43 | 17:13 | 17:43 | 18:13 | 18:43 | 19:11 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 15:16 | 15:46 | 16:15 | 16:44 | 17:14 | 17:44 | 18:14 | 18:44 | 19:12 |
| Pacific Hwy after Oxford St, Gateshead | 15:23 | 15:53 | 16:22 | 16:50 | 17:20 | 17:50 | 18:19 | 18:50 | 19:17 |
| Jewells Plaza, Ntaba Rd, Jewells | 15:30 | 16:00 | 16:28 | 16:56 | 17:26 | 17:56 | 18:25 | 18:56 | 19:23 |
| Pacific Hwy at Cobbin Pde, Belmont | 15:36 | 16:05 | 16:34 | 17:01 | 17:32 | 18:01 | 18:30 | 19:01 | 19:28 |
| Pacific Hwy opp Macquarie St, Belmont | 15:39 | 16:09 | 16:37 | 17:05 | 17:35 | 18:04 | 18:33 | 19:04 | 19:31 |
| Pacific Hwy opp Marks Point Rd, Marks Point | 15:44 | - | 16:42 | - | 17:40 | - | 18:38 | - | 19:35 |
| Bowman St opp Lake Rd, Swansea | 15:50 | - | 16:48 | - | 17:46 | - | 18:43 | - | 19:40 |
| Park Ave opp Swansea High School, Caves Beach | 15:54 | - | 16:52 | - | 17:50 | - | 18:47 | - | 19:44 |
| Lambton Pde at Hamilton St, Swansea Heads | 16:01 | - | 16:59 | - | 17:57 | - | 18:53 | - | 19:50 |
| Alick St opp Spinnakers Leisure Park, Belmont | - | 16:12 | - | 17:08 | - | 18:07 | - | 19:07 | - |

| Saturday | | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|--------|--------|--------|
| Customs House, Watt St, Newcastle | 19:10 | 20:10 | 21:10 | 22:10 | 23:10 | 00:10 | C01:05 | C02:05 | C03:05 |
| Darby St before Bull St, Cooks Hill | 19:16 | 20:16 | 21:16 | 22:16 | 23:16 | 00:16 | C01:09 | C02:09 | C03:09 |
| Junction Fair, Glebe Rd, The Junction | 19:22 | 20:22 | 21:22 | 22:22 | 23:22 | 00:22 | C01:13 | C02:13 | C03:13 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 19:28 | 20:28 | 21:28 | 22:28 | 23:28 | 00:28 | C01:18 | C02:18 | C03:18 |
| Westfield Kotara, Park Ave, Kotara | 19:33 | 20:33 | 21:33 | 22:33 | 23:33 | 00:33 | C01:22 | C02:22 | C03:22 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 19:41 | 20:40 | 21:40 | 22:40 | 23:40 | 00:40 | C01:29 | C02:29 | C03:29 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 19:42 | 20:41 | 21:41 | 22:41 | 23:41 | 00:41 | C01:29 | C02:29 | C03:29 |
| Pacific Hwy after Oxford St, Gateshead | 19:47 | 20:47 | 21:47 | 22:47 | 23:47 | 00:47 | C01:34 | C02:34 | C03:34 |
| Jewells Plaza, Ntaba Rd, Jewells | 19:53 | 20:53 | 21:53 | 22:53 | 23:53 | 00:53 | C01:39 | C02:39 | C03:39 |
| Pacific Hwy at Cobbin Pde, Belmont | 19:58 | 20:58 | 21:58 | 22:58 | 23:58 | 00:58 | C01:44 | C02:44 | C03:44 |
| Pacific Hwy opp Macquarie St, Belmont | 20:01 | 21:01 | 22:01 | 23:01 | 00:01 | 01:01 | C01:46 | C02:46 | C03:46 |
| Pacific Hwy opp Marks Point Rd, Marks Point | - | 21:05 | 22:05 | 23:05 | 00:05 | - | C01:49 | C02:49 | C03:49 |
| Bowman St opp Lake Rd, Swansea | - | 21:10 | 22:10 | 23:10 | 00:10 | - | C01:53 | C02:53 | C03:53 |
| Park Ave opp Swansea High School, Caves Beach | - | 21:14 | 22:14 | 23:14 | 00:14 | - | C01:56 | C02:56 | C03:56 |
| Lambton Pde at Hamilton St, Swansea Heads | - | 21:20 | 22:20 | 23:20 | 00:20 | - | C02:01 | C03:01 | C04:01 |
| Alick St opp Spinnakers Leisure Park, Belmont | 20:04 | - | - | - | - | 01:04 | - | - | - |
| Sunday & Public Holidays | | | | | | | | | |
| Customs House, Watt St, Newcastle | 06:10 | 06:40 | 07:10 | 07:40 | 08:10 | 08:40 | 09:10 | 09:40 | 10:10 |
| Darby St before Bull St, Cooks Hill | 06:15 | 06:45 | 07:15 | 07:46 | 08:16 | 08:46 | 09:16 | 09:46 | 10:16 |
| Junction Fair, Glebe Rd, The Junction | 06:20 | 06:52 | 07:21 | 07:52 | 08:22 | 08:52 | 09:22 | 09:52 | 10:22 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 06:26 | 06:58 | 07:27 | 07:59 | 08:29 | 09:00 | 09:30 | 10:00 | 10:30 |
| Westfield Kotara, Park Ave, Kotara | 06:30 | 07:03 | 07:31 | 08:03 | 08:33 | 09:05 | 09:35 | 10:05 | 10:35 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 06:39 | 07:12 | 07:40 | 08:12 | 08:42 | 09:14 | 09:44 | 10:15 | 10:44 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 06:41 | 07:13 | 07:42 | 08:13 | 08:44 | 09:15 | 09:46 | 10:16 | 10:46 |
| Pacific Hwy after Oxford St, Gateshead | - | 07:18 | - | 08:19 | - | 09:22 | - | 10:22 | - |
| Jewells Plaza, Ntaba Rd, Jewells | - | 07:24 | - | 08:25 | - | 09:29 | - | 10:29 | - |
| Pacific Hwy at Cobbin Pde, Belmont | - | 07:29 | - | 08:31 | - | 09:35 | - | 10:35 | - |
| Pacific Hwy opp Macquarie St, Belmont | - | 07:32 | - | 08:34 | - | 09:38 | - | 10:38 | - |
| Pacific Hwy opp Marks Point Rd, Marks Point | - | 07:36 | - | 08:39 | - | 09:43 | - | 10:43 | - |
| Bowman St opp Lake Rd, Swansea | - | 07:42 | - | 08:45 | - | 09:49 | - | 10:49 | - |
| Park Ave opp Swansea High School, Caves Beach | - | 07:46 | - | 08:49 | - | 09:53 | - | 10:53 | - |
| Lambton Pde at Hamilton St, Swansea Heads | - | 07:53 | - | 08:56 | - | 10:00 | - | 11:00 | - |
| Sunday & Public Holidays | | | | | | | | | |
| Customs House, Watt St, Newcastle | 10:40 | 11:10 | 11:40 | 12:10 | 12:40 | 13:10 | 13:40 | 14:10 | 14:40 |
| Darby St before Bull St, Cooks Hill | 10:46 | 11:16 | 11:46 | 12:16 | 12:46 | 13:16 | 13:46 | 14:16 | 14:46 |
| Junction Fair, Glebe Rd, The Junction | 10:52 | 11:22 | 11:52 | 12:22 | 12:52 | 13:22 | 13:52 | 14:22 | 14:52 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 11:00 | 11:30 | 12:00 | 12:30 | 13:00 | 13:30 | 14:00 | 14:30 | 15:00 |
| Westfield Kotara, Park Ave, Kotara | 11:05 | 11:35 | 12:05 | 12:35 | 13:05 | 13:35 | 14:05 | 14:35 | 15:05 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 11:15 | 11:45 | 12:15 | 12:44 | 13:15 | 13:44 | 14:15 | 14:44 | 15:15 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 11:16 | 11:46 | 12:16 | 12:46 | 13:16 | 13:46 | 14:16 | 14:46 | 15:16 |
| Pacific Hwy after Oxford St, Gateshead | 11:22 | - | 12:22 | - | 13:22 | - | 14:22 | - | 15:22 |
| Jewells Plaza, Ntaba Rd, Jewells | 11:29 | - | 12:29 | - | 13:29 | - | 14:29 | - | 15:29 |
| Pacific Hwy at Cobbin Pde, Belmont | 11:35 | - | 12:35 | - | 13:35 | - | 14:35 | - | 15:35 |
| Pacific Hwy opp Macquarie St, Belmont | 11:38 | - | 12:38 | - | 13:38 | - | 14:38 | - | 15:38 |
| Pacific Hwy opp Marks Point Rd, Marks Point | 11:43 | - | 12:43 | - | 13:43 | - | 14:43 | - | 15:43 |
| Bowman St opp Lake Rd, Swansea | 11:49 | - | 12:49 | - | 13:49 | - | 14:49 | - | 15:49 |
| Park Ave opp Swansea High School, Caves Beach | 11:53 | - | 12:53 | - | 13:53 | - | 14:53 | - | 15:53 |
| Lambton Pde at Hamilton St, Swansea Heads | 12:00 | - | 13:00 | - | 14:00 | - | 15:00 | - | 16:00 |

| Sunday & Public Holidays | | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Customs House, Watt St, Newcastle | 15:10 | 15:40 | 16:10 | 16:40 | 17:10 | 17:40 | 18:10 | 18:40 | 19:10 |
| Darby St before Bull St, Cooks Hill | 15:16 | 15:46 | 16:16 | 16:46 | 17:16 | 17:46 | 18:16 | 18:46 | 19:16 |
| Junction Fair, Glebe Rd, The Junction | 15:22 | 15:52 | 16:22 | 16:52 | 17:22 | 17:52 | 18:22 | 18:52 | 19:22 |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 15:30 | 16:00 | 16:30 | 16:59 | 17:29 | 17:59 | 18:29 | 18:58 | 19:28 |
| Westfield Kotara, Park Ave, Kotara | 15:35 | 16:05 | 16:35 | 17:04 | 17:34 | 18:04 | 18:34 | 19:03 | 19:33 |
| Charlestown Square, Pearson St, Stand B, Charlestown | 15:44 | 16:15 | 16:44 | 17:13 | 17:42 | 18:13 | 18:42 | 19:11 | 19:41 |
| Charlestown Square, Frederick St, Stand D, Charlestown | 15:46 | 16:16 | 16:46 | 17:14 | 17:44 | 18:14 | 18:44 | 19:12 | 19:42 |
| Pacific Hwy after Oxford St, Gateshead | - | 16:22 | - | 17:20 | - | 18:19 | - | 19:17 | - |
| Jewells Plaza, Ntaba Rd, Jewells | - | 16:29 | - | 17:26 | - | 18:25 | - | 19:23 | - |
| Pacific Hwy at Cobbin Pde, Belmont | - | 16:35 | - | 17:32 | - | 18:30 | - | 19:28 | - |
| Pacific Hwy opp Macquarie St, Belmont | - | 16:38 | - | 17:35 | - | 18:33 | - | 19:31 | - |
| Pacific Hwy opp Marks Point Rd, Marks Point | - | 16:43 | - | 17:40 | - | 18:37 | - | 19:35 | - |
| Bowman St opp Lake Rd, Swansea | - | 16:49 | - | 17:46 | - | 18:43 | - | 19:40 | - |
| Park Ave opp Swansea High School, Caves Beach | - | 16:53 | - | 17:50 | - | 18:47 | - | 19:44 | - |
| Lambton Pde at Hamilton St, Swansea Heads | - | 17:00 | - | 17:57 | - | 18:53 | - | 19:50 | - |
| Sunday & Public Holidays | | | | | | | | | |
| Customs House, Watt St, Newcastle | 19:40 | 20:40 | 21:40 | 22:40 | | | | | |
| Darby St before Bull St, Cooks Hill | 19:46 | 20:46 | 21:46 | 22:46 | | | | | |
| Junction Fair, Glebe Rd, The Junction | 19:52 | 20:52 | 21:52 | 22:52 | | | | | |
| Glebe Rd opp Adamstown Uniting Church, Adamstown | 19:58 | 20:58 | 21:58 | 22:58 | | | | | |
| Westfield Kotara, Park Ave, Kotara | 20:03 | 21:03 | 22:03 | 23:03 | | | | | |
| Charlestown Square, Pearson St, Stand B, Charlestown | 20:13 | 21:10 | 22:10 | 23:10 | | | | | |
| Charlestown Square, Frederick St, Stand D, Charlestown | 20:13 | 21:11 | 22:11 | 23:11 | | | | | |
| Pacific Hwy after Oxford St, Gateshead | 20:17 | 21:17 | 22:17 | 23:17 | | | | | |
| Jewells Plaza, Ntaba Rd, Jewells | 20:23 | 21:23 | 22:23 | 23:23 | | | | | |
| Pacific Hwy at Cobbin Pde, Belmont | 20:28 | 21:28 | 22:28 | 23:28 | | | | | |
| Pacific Hwy opp Macquarie St, Belmont | 20:31 | 21:31 | 22:31 | 23:31 | | | | | |
| Pacific Hwy opp Marks Point Rd, Marks Point | 20:35 | - | - | - | | | | | |
| Bowman St opp Lake Rd, Swansea | 20:40 | - | - | - | | | | | |
| Park Ave opp Swansea High School, Caves Beach | 20:44 | - | - | - | | | | | |
| Lambton Pde at Hamilton St, Swansea Heads | 20:50 | - | - | - | | | | | |
| Alick St opp Spinnakers Leisure Park, Belmont | - | 21:34 | 22:34 | 23:34 | | | | | |

| Monday to Friday | | | | | | | | | |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lambton Pde at Hamilton St, Swansea Heads | 05:03 | 05:33 | - | 06:29 | - | 06:45 | - | - | 07:18 |
| Swansea High School, Park Ave, Caves Beach | 05:09 | 05:39 | - | 06:35 | - | 06:52 | - | - | 07:25 |
| Pacific Hwy after Lake Rd, Swansea | 05:13 | 05:43 | - | 06:39 | - | 06:56 | - | - | 07:30 |
| Pacific Hwy at Marks Point Rd, Marks Point | 05:19 | 05:49 | - | 06:45 | - | 07:02 | - | - | 07:36 |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | 06:17 | - | - | - | - | - | - |
| Pacific Hwy before Macquarie St, Belmont | 05:22 | 05:52 | 06:20 | 06:49 | - | 07:06 | - | - | 07:41 |
| Ntaba Rd opp Jewells Plaza, Jewells | 05:31 | 06:01 | 06:31 | 07:00 | - | 07:18 | - | - | 07:55 |
| Pacific Hwy at Oxford St, Gateshead | 05:38 | 06:08 | 06:38 | 07:07 | - | 07:27 | - | - | 08:06 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 05:40 | 06:10 | 06:41 | 07:11 | 07:21 | 07:31 | 07:41 | 07:56 | 08:10 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 05:41 | 06:11 | 06:42 | 07:12 | 07:22 | 07:32 | 07:42 | 07:57 | 08:11 |
| Park Ave opp Westfield Kotara, Kotara | 05:51 | 06:21 | 06:52 | 07:22 | 07:32 | 07:44 | 07:53 | 08:08 | 08:25 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 05:56 | 06:26 | 06:57 | 07:28 | 07:38 | 07:50 | 07:59 | 08:14 | 08:32 |
| Junction Fair, Glebe Rd, The Junction | 06:02 | 06:32 | 07:04 | 07:36 | 07:46 | 07:58 | 08:07 | 08:22 | 08:43 |
| Darby St at Bull St, Cooks Hill | 06:07 | 06:37 | 07:09 | 07:41 | 07:51 | 08:03 | 08:12 | 08:27 | 08:48 |
| Customs House, Watt St, Newcastle | 06:14 | 06:44 | 07:18 | 07:50 | 08:00 | 08:13 | 08:22 | 08:37 | 08:57 |

| Monday to Friday | | | | | | | | | |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lambton Pde at Hamilton St, Swansea Heads | - | - | 07:58 | - | 08:28 | - | 08:59 | - | - |
| Swansea High School, Park Ave, Caves Beach | - | - | 08:05 | - | 08:35 | - | 09:06 | - | - |
| Pacific Hwy after Lake Rd, Swansea | - | - | 08:10 | - | 08:40 | - | 09:10 | - | - |
| Pacific Hwy at Marks Point Rd, Marks Point | - | - | 08:16 | - | 08:46 | - | 09:16 | - | - |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | - | - | - | - | - | - | 09:47 |
| Pacific Hwy before Macquarie St, Belmont | - | - | 08:21 | - | 08:51 | - | 09:21 | - | 09:51 |
| Ntaba Rd opp Jewells Plaza, Jewells | - | - | 08:34 | - | 09:03 | - | 09:33 | - | 10:03 |
| Pacific Hwy at Oxford St, Gateshead | - | - | 08:44 | - | 09:13 | - | 09:41 | - | 10:11 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 08:23 | 08:36 | 08:48 | 09:04 | 09:17 | 09:30 | 09:45 | 10:00 | 10:15 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 08:23 | 08:37 | 08:49 | 09:05 | 09:18 | 09:31 | 09:46 | 10:01 | 10:16 |
| Park Ave opp Westfield Kotara, Kotara | 08:33 | 08:48 | 09:01 | 09:17 | 09:30 | 09:42 | 09:57 | 10:12 | 10:27 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 08:42 | 08:55 | 09:08 | 09:23 | 09:36 | 09:48 | 10:03 | 10:18 | 10:33 |
| Junction Fair, Glebe Rd, The Junction | 08:54 | 09:05 | 09:18 | 09:31 | 09:44 | 09:56 | 10:11 | 10:26 | 10:41 |
| Darby St at Bull St, Cooks Hill | 08:59 | 09:10 | 09:23 | 09:36 | 09:49 | 10:01 | 10:16 | 10:31 | 10:46 |
| Customs House, Watt St, Newcastle | 09:09 | 09:19 | 09:32 | 09:44 | 09:57 | 10:09 | 10:24 | 10:39 | 10:54 |

| Monday to Friday | | | | | | | | | |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lambton Pde at Hamilton St, Swansea Heads | - | 09:59 | - | - | - | 10:59 | - | - | - |
| Swansea High School, Park Ave, Caves Beach | - | 10:06 | - | - | - | 11:06 | - | - | - |
| Pacific Hwy after Lake Rd, Swansea | - | 10:10 | - | - | - | 11:10 | - | - | - |
| Pacific Hwy at Marks Point Rd, Marks Point | - | 10:16 | - | - | - | 11:16 | - | - | - |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | - | 10:47 | - | - | - | 11:47 | - |
| Pacific Hwy before Macquarie St, Belmont | - | 10:21 | - | 10:51 | - | 11:21 | - | 11:51 | - |
| Ntaba Rd opp Jewells Plaza, Jewells | - | 10:33 | - | 11:03 | - | 11:33 | - | 12:03 | - |
| Pacific Hwy at Oxford St, Gateshead | - | 10:41 | - | 11:11 | - | 11:41 | - | 12:11 | - |
| Charlestown Square, Frederick St, Stand C, Charlestown | 10:30 | 10:44 | 11:00 | 11:15 | 11:30 | 11:45 | 12:00 | 12:15 | 12:30 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 10:31 | 10:45 | 11:01 | 11:16 | 11:31 | 11:46 | 12:01 | 12:16 | 12:31 |
| Park Ave opp Westfield Kotara, Kotara | 10:43 | 10:57 | 11:13 | 11:27 | 11:43 | 11:57 | 12:13 | 12:27 | 12:43 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 10:48 | 11:03 | 11:18 | 11:33 | 11:48 | 12:03 | 12:18 | 12:33 | 12:48 |
| Junction Fair, Glebe Rd, The Junction | 10:56 | 11:11 | 11:26 | 11:41 | 11:56 | 12:11 | 12:26 | 12:41 | 12:56 |
| Darby St at Bull St, Cooks Hill | 11:01 | 11:16 | 11:31 | 11:46 | 12:01 | 12:16 | 12:31 | 12:46 | 13:01 |
| Customs House, Watt St, Newcastle | 11:09 | 11:24 | 11:39 | 11:54 | 12:09 | 12:24 | 12:39 | 12:54 | 13:09 |

| Monday to Friday | | | | | | | | | |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lambton Pde at Hamilton St, Swansea Heads | 11:59 | - | - | - | 12:59 | - | - | - | 13:59 |
| Swansea High School, Park Ave, Caves Beach | 12:06 | - | - | - | 13:06 | - | - | - | 14:06 |
| Pacific Hwy after Lake Rd, Swansea | 12:10 | - | - | - | 13:10 | - | - | - | 14:10 |
| Pacific Hwy at Marks Point Rd, Marks Point | 12:16 | - | - | - | 13:16 | - | - | - | 14:16 |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | 12:47 | - | - | - | 13:47 | - | - |
| Pacific Hwy before Macquarie St, Belmont | 12:21 | - | 12:51 | - | 13:21 | - | 13:51 | - | 14:21 |
| Ntaba Rd opp Jewells Plaza, Jewells | 12:33 | - | 13:03 | - | 13:33 | - | 14:03 | - | 14:33 |
| Pacific Hwy at Oxford St, Gateshead | 12:41 | - | 13:11 | - | 13:41 | - | 14:11 | - | 14:41 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 12:45 | 13:00 | 13:15 | 13:30 | 13:45 | 14:00 | 14:15 | 14:30 | 14:45 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 12:46 | 13:01 | 13:16 | 13:31 | 13:46 | 14:01 | 14:16 | 14:31 | 14:46 |
| Park Ave opp Westfield Kotara, Kotara | 12:57 | 13:13 | 13:27 | 13:43 | 13:57 | 14:13 | 14:27 | 14:43 | 14:57 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 13:03 | 13:18 | 13:33 | 13:48 | 14:03 | 14:18 | 14:33 | 14:48 | 15:03 |
| Junction Fair, Glebe Rd, The Junction | 13:11 | 13:26 | 13:41 | 13:56 | 14:11 | 14:26 | 14:41 | 14:56 | 15:11 |
| Darby St at Bull St, Cooks Hill | 13:16 | 13:31 | 13:46 | 14:01 | 14:16 | 14:31 | 14:46 | 15:01 | 15:16 |
| Customs House, Watt St, Newcastle | 13:24 | 13:39 | 13:54 | 14:09 | 14:24 | 14:39 | 14:54 | 15:09 | 15:24 |
| Monday to Friday | | | | | | | | | |
| Lambton Pde at Hamilton St, Swansea Heads | - | - | 14:40 | - | - | - | - | 15:55 | - |
| Swansea High School, Park Ave, Caves Beach | - | - | 14:47 | - | - | - | - | 16:02 | - |
| Pacific Hwy after Lake Rd, Swansea | - | - | 14:51 | - | - | - | - | 16:07 | - |
| Pacific Hwy at Marks Point Rd, Marks Point | - | - | 14:57 | - | - | - | - | 16:14 | - |
| Alick St opp Spinnakers Leisure Park, Belmont | 14:30 | - | - | - | - | 15:42 | - | - | 16:33 |
| Pacific Hwy before Macquarie St, Belmont | 14:34 | - | 15:02 | - | - | 15:46 | - | 16:20 | 16:37 |
| Ntaba Rd opp Jewells Plaza, Jewells | 14:48 | - | 15:15 | - | - | 16:00 | - | 16:32 | 16:48 |
| Pacific Hwy at Oxford St, Gateshead | 14:56 | - | 15:26 | - | - | 16:10 | - | 16:41 | 16:56 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 15:00 | 15:15 | 15:29 | 15:45 | 16:00 | 16:14 | 16:30 | 16:45 | 16:59 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 15:01 | 15:16 | 15:30 | 15:46 | 16:01 | 16:15 | 16:31 | 16:46 | 17:00 |
| Park Ave opp Westfield Kotara, Kotara | 15:12 | 15:28 | 15:42 | 15:57 | 16:12 | 16:27 | 16:41 | 16:57 | 17:11 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 15:18 | 15:33 | 15:48 | 16:03 | 16:18 | 16:33 | 16:48 | 17:03 | 17:18 |
| Junction Fair, Glebe Rd, The Junction | 15:26 | 15:42 | 15:57 | 16:12 | 16:27 | 16:42 | 16:56 | 17:11 | 17:26 |
| Darby St at Bull St, Cooks Hill | 15:31 | 15:47 | 16:02 | 16:17 | 16:32 | 16:47 | 17:01 | 17:16 | 17:31 |
| Customs House, Watt St, Newcastle | 15:39 | 15:55 | 16:10 | 16:25 | 16:40 | 16:55 | 17:09 | 17:24 | 17:39 |
| Monday to Friday | | | | | | | | | |
| Lambton Pde at Hamilton St, Swansea Heads | - | - | 16:59 | - | 17:30 | - | 18:00 | - | 18:33 |
| Swansea High School, Park Ave, Caves Beach | - | - | 17:05 | - | 17:36 | - | 18:06 | - | 18:39 |
| Pacific Hwy after Lake Rd, Swansea | - | - | 17:10 | - | 17:40 | - | 18:10 | - | 18:43 |
| Pacific Hwy at Marks Point Rd, Marks Point | - | - | 17:16 | - | 17:46 | - | 18:16 | - | 18:48 |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | - | 17:32 | - | - | - | - | - |
| Pacific Hwy before Macquarie St, Belmont | - | - | 17:21 | 17:36 | 17:51 | - | 18:21 | - | 18:52 |
| Ntaba Rd opp Jewells Plaza, Jewells | - | - | 17:33 | 17:48 | 18:02 | - | 18:32 | - | 19:02 |
| Pacific Hwy at Oxford St, Gateshead | - | - | 17:41 | 17:56 | 18:09 | - | 18:39 | - | 19:09 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 17:15 | 17:30 | 17:44 | 17:59 | 18:13 | 18:28 | 18:42 | 18:58 | 19:12 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 17:16 | 17:31 | 17:45 | 18:00 | 18:14 | 18:29 | 18:43 | 18:58 | 19:13 |
| Park Ave opp Westfield Kotara, Kotara | 17:26 | 17:41 | 17:56 | 18:13 | 18:24 | 18:39 | 18:54 | 19:08 | 19:22 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 17:33 | 17:46 | 18:03 | 18:19 | 18:29 | 18:44 | 18:59 | 19:12 | 19:26 |
| Junction Fair, Glebe Rd, The Junction | 17:41 | 17:53 | 18:11 | 18:28 | 18:35 | 18:50 | 19:05 | 19:18 | 19:32 |
| Darby St at Bull St, Cooks Hill | 17:46 | 17:58 | 18:16 | 18:33 | 18:40 | 18:55 | 19:10 | 19:23 | 19:37 |
| Customs House, Watt St, Newcastle | 17:54 | 18:05 | 18:24 | 18:40 | 18:47 | 19:02 | 19:17 | 19:30 | 19:44 |

| Monday to Friday | | | | | | | | | |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lambton Pde at Hamilton St, Swansea Heads | 19:01 | - | 20:01 | - | 20:56 | - | - | - | - |
| Swansea High School, Park Ave, Caves Beach | 19:07 | - | 20:07 | - | 21:02 | - | - | - | - |
| Pacific Hwy after Lake Rd, Swansea | 19:11 | - | 20:11 | - | 21:06 | - | - | - | - |
| Pacific Hwy at Marks Point Rd, Marks Point | 19:16 | - | 20:16 | - | 21:11 | - | - | - | - |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | - | - | - | - | 22:12 | 23:12 | - |
| Pacific Hwy before Macquarie St, Belmont | 19:20 | - | 20:20 | - | 21:15 | - | 22:15 | 23:15 | - |
| Ntaba Rd opp Jewells Plaza, Jewells | 19:30 | - | 20:29 | - | 21:24 | - | 22:24 | 23:24 | - |
| Pacific Hwy at Oxford St, Gateshead | 19:37 | - | 20:35 | - | 21:30 | - | 22:30 | 23:30 | - |
| Charlestown Square, Frederick St, Stand C, Charlestown | 19:40 | 20:11 | 20:38 | 21:09 | 21:33 | 22:04 | 22:33 | 23:33 | - |
| Charlestown Square, Pearson St, Stand A, Charlestown | 19:41 | 20:11 | 20:39 | 21:09 | 21:34 | 22:04 | 22:34 | 23:34 | - |
| Park Ave opp Westfield Kotara, Kotara | 19:50 | 20:19 | 20:47 | 21:17 | 21:42 | 22:12 | 22:42 | 23:42 | - |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 19:54 | 20:23 | 20:51 | 21:21 | 21:46 | 22:16 | 22:46 | 23:46 | - |
| Junction Fair, Glebe Rd, The Junction | 20:00 | 20:28 | 20:56 | 21:26 | 21:51 | 22:21 | 22:51 | 23:51 | - |
| Darby St at Bull St, Cooks Hill | 20:05 | 20:33 | 21:01 | 21:31 | 21:56 | 22:26 | 22:56 | 23:56 | - |
| Customs House, Watt St, Newcastle | 20:12 | 20:40 | 21:08 | 21:38 | 22:03 | 22:33 | 23:03 | 00:03 | - |
| Saturday | | | | | | | | | |
| Lambton Pde at Hamilton St, Swansea Heads | - | 06:33 | - | 07:29 | - | 08:26 | - | 09:24 | - |
| Swansea High School, Park Ave, Caves Beach | - | 06:39 | - | 07:35 | - | 08:33 | - | 09:31 | - |
| Pacific Hwy after Lake Rd, Swansea | - | 06:43 | - | 07:39 | - | 08:38 | - | 09:37 | - |
| Pacific Hwy at Marks Point Rd, Marks Point | - | 06:48 | - | 07:45 | - | 08:44 | - | 09:44 | - |
| Alick St opp Spinnakers Leisure Park, Belmont | 05:50 | - | 07:17 | - | 08:15 | - | 09:15 | - | 10:15 |
| Pacific Hwy before Macquarie St, Belmont | 05:53 | 06:53 | 07:20 | 07:50 | 08:19 | 08:49 | 09:19 | 09:49 | 10:19 |
| Ntaba Rd opp Jewells Plaza, Jewells | 06:02 | 07:02 | 07:31 | 08:01 | 08:30 | 09:00 | 09:30 | 10:00 | 10:30 |
| Pacific Hwy at Oxford St, Gateshead | 06:09 | 07:09 | 07:38 | 08:08 | 08:38 | 09:08 | 09:38 | 10:08 | 10:38 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 06:11 | 07:11 | 07:41 | 08:11 | 08:41 | 09:12 | 09:42 | 10:12 | 10:42 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 06:12 | 07:12 | 07:42 | 08:12 | 08:42 | 09:13 | 09:43 | 10:13 | 10:43 |
| Park Ave opp Westfield Kotara, Kotara | 06:21 | 07:21 | 07:51 | 08:22 | 08:52 | 09:24 | 09:54 | 10:24 | 10:54 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 06:26 | 07:26 | 07:56 | 08:27 | 08:57 | 09:29 | 09:59 | 10:29 | 10:59 |
| Junction Fair, Glebe Rd, The Junction | 06:32 | 07:32 | 08:02 | 08:34 | 09:05 | 09:37 | 10:07 | 10:37 | 11:07 |
| Darby St at Bull St, Cooks Hill | 06:36 | 07:36 | 08:06 | 08:38 | 09:09 | 09:41 | 10:11 | 10:41 | 11:11 |
| Customs House, Watt St, Newcastle | 06:43 | 07:43 | 08:13 | 08:47 | 09:18 | 09:50 | 10:20 | 10:50 | 11:20 |
| Saturday | | | | | | | | | |
| Lambton Pde at Hamilton St, Swansea Heads | 10:24 | - | 11:26 | - | 12:26 | - | 13:26 | - | 14:26 |
| Swansea High School, Park Ave, Caves Beach | 10:31 | - | 11:33 | - | 12:33 | - | 13:33 | - | 14:33 |
| Pacific Hwy after Lake Rd, Swansea | 10:37 | - | 11:38 | - | 12:38 | - | 13:38 | - | 14:38 |
| Pacific Hwy at Marks Point Rd, Marks Point | 10:44 | - | 11:44 | - | 12:44 | - | 13:44 | - | 14:44 |
| Alick St opp Spinnakers Leisure Park, Belmont | - | 11:15 | - | 12:15 | - | 13:15 | - | 14:15 | - |
| Pacific Hwy before Macquarie St, Belmont | 10:49 | 11:19 | 11:49 | 12:19 | 12:49 | 13:19 | 13:49 | 14:19 | 14:49 |
| Ntaba Rd opp Jewells Plaza, Jewells | 11:00 | 11:30 | 12:00 | 12:30 | 13:00 | 13:30 | 14:00 | 14:30 | 15:00 |
| Pacific Hwy at Oxford St, Gateshead | 11:08 | 11:38 | 12:08 | 12:38 | 13:08 | 13:38 | 14:08 | 14:38 | 15:08 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 11:12 | 11:42 | 12:12 | 12:42 | 13:12 | 13:42 | 14:12 | 14:42 | 15:12 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 11:13 | 11:43 | 12:13 | 12:43 | 13:13 | 13:43 | 14:13 | 14:43 | 15:13 |
| Park Ave opp Westfield Kotara, Kotara | 11:24 | 11:54 | 12:24 | 12:54 | 13:24 | 13:54 | 14:24 | 14:54 | 15:24 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 11:29 | 11:59 | 12:29 | 12:59 | 13:29 | 13:59 | 14:29 | 14:59 | 15:29 |
| Junction Fair, Glebe Rd, The Junction | 11:37 | 12:07 | 12:37 | 13:07 | 13:37 | 14:07 | 14:37 | 15:07 | 15:37 |
| Darby St at Bull St, Cooks Hill | 11:41 | 12:11 | 12:41 | 13:11 | 13:41 | 14:11 | 14:41 | 15:11 | 15:41 |
| Customs House, Watt St, Newcastle | 11:50 | 12:20 | 12:50 | 13:20 | 13:50 | 14:20 | 14:50 | 15:20 | 15:50 |

| Saturday | | | | | | | | | |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lambton Pde at Hamilton St, Swansea Heads | - | 15:26 | - | 16:26 | - | 17:27 | - | 18:31 | - |
| Swansea High School, Park Ave, Caves Beach | - | 15:33 | - | 16:33 | - | 17:34 | - | 18:37 | - |
| Pacific Hwy after Lake Rd, Swansea | - | 15:38 | - | 16:38 | - | 17:39 | - | 18:42 | - |
| Pacific Hwy at Marks Point Rd, Marks Point | - | 15:44 | - | 16:44 | - | 17:45 | - | 18:47 | - |
| Alick St opp Spinnakers Leisure Park, Belmont | 15:15 | - | 16:15 | - | 17:16 | - | 18:18 | - | 19:18 |
| Pacific Hwy before Macquarie St, Belmont | 15:19 | 15:49 | 16:19 | 16:49 | 17:20 | 17:50 | 18:22 | 18:52 | 19:22 |
| Ntaba Rd opp Jewells Plaza, Jewells | 15:30 | 16:00 | 16:30 | 17:00 | 17:30 | 18:00 | 18:31 | 19:01 | 19:31 |
| Pacific Hwy at Oxford St, Gateshead | 15:38 | 16:08 | 16:38 | 17:08 | 17:38 | 18:08 | 18:38 | 19:08 | 19:38 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 15:42 | 16:12 | 16:42 | 17:12 | 17:42 | 18:11 | 18:41 | 19:11 | 19:41 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 15:43 | 16:13 | 16:43 | 17:13 | 17:43 | 18:12 | 18:42 | 19:12 | 19:42 |
| Park Ave opp Westfield Kotara, Kotara | 15:54 | 16:24 | 16:54 | 17:24 | 17:54 | 18:23 | 18:53 | 19:23 | 19:53 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 15:59 | 16:29 | 16:59 | 17:29 | 17:59 | 18:28 | 18:58 | 19:28 | 19:58 |
| Junction Fair, Glebe Rd, The Junction | 16:07 | 16:37 | 17:07 | 17:37 | 18:07 | 18:36 | 19:05 | 19:35 | 20:05 |
| Darby St at Bull St, Cooks Hill | 16:11 | 16:41 | 17:11 | 17:41 | 18:11 | 18:40 | 19:09 | 19:39 | 20:09 |
| Customs House, Watt St, Newcastle | 16:20 | 16:50 | 17:20 | 17:50 | 18:19 | 18:48 | 19:16 | 19:46 | 20:16 |

| Saturday | | | | | |
|---|-------|-------|-------|-------|-------|
| Lambton Pde at Hamilton St, Swansea Heads | 19:31 | 20:31 | - | - | - |
| Swansea High School, Park Ave, Caves Beach | 19:37 | 20:37 | - | - | - |
| Pacific Hwy after Lake Rd, Swansea | 19:42 | 20:42 | - | - | - |
| Pacific Hwy at Marks Point Rd, Marks Point | 19:47 | 20:47 | - | - | - |
| Alick St opp Spinnakers Leisure Park, Belmont | - | - | 21:48 | 22:48 | 23:48 |
| Pacific Hwy before Macquarie St, Belmont | 19:52 | 20:52 | 21:52 | 22:52 | 23:52 |
| Ntaba Rd opp Jewells Plaza, Jewells | 20:01 | 21:01 | 22:01 | 23:01 | 00:01 |
| Pacific Hwy at Oxford St, Gateshead | 20:08 | 21:08 | 22:08 | 23:08 | 00:08 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 20:11 | 21:11 | 22:11 | 23:11 | 00:11 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 20:12 | 21:12 | 22:12 | 23:12 | 00:12 |
| Park Ave opp Westfield Kotara, Kotara | 20:23 | 21:23 | 22:22 | 23:22 | 00:22 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 20:28 | 21:28 | 22:27 | 23:27 | 00:27 |
| Junction Fair, Glebe Rd, The Junction | 20:35 | 21:35 | 22:33 | 23:33 | 00:33 |
| Darby St at Bull St, Cooks Hill | 20:39 | 21:39 | 22:37 | 23:37 | 00:37 |
| Customs House, Watt St, Newcastle | 20:46 | 21:46 | 22:44 | 23:44 | 00:44 |

| Sunday & Public Holidays | | | | | | | | | |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lambton Pde at Hamilton St, Swansea Heads | - | 07:29 | - | 08:26 | - | 09:24 | - | 10:24 | - |
| Swansea High School, Park Ave, Caves Beach | - | 07:35 | - | 08:33 | - | 09:31 | - | 10:31 | - |
| Pacific Hwy after Lake Rd, Swansea | - | 07:39 | - | 08:38 | - | 09:37 | - | 10:37 | - |
| Pacific Hwy at Marks Point Rd, Marks Point | - | 07:45 | - | 08:44 | - | 09:44 | - | 10:44 | - |
| Alick St opp Spinnakers Leisure Park, Belmont | 06:50 | - | - | - | - | - | - | - | - |
| Pacific Hwy before Macquarie St, Belmont | 06:53 | 07:50 | - | 08:49 | - | 09:49 | - | 10:49 | - |
| Ntaba Rd opp Jewells Plaza, Jewells | 07:02 | 08:01 | - | 09:00 | - | 10:00 | - | 11:00 | - |
| Pacific Hwy at Oxford St, Gateshead | 07:09 | 08:08 | - | 09:08 | - | 10:08 | - | 11:08 | - |
| Charlestown Square, Frederick St, Stand C, Charlestown | 07:11 | 08:11 | 08:42 | 09:12 | 09:42 | 10:12 | 10:42 | 11:12 | 11:42 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 07:12 | 08:12 | 08:43 | 09:13 | 09:43 | 10:13 | 10:43 | 11:13 | 11:43 |
| Park Ave opp Westfield Kotara, Kotara | 07:21 | 08:22 | 08:53 | 09:24 | 09:53 | 10:24 | 10:53 | 11:24 | 11:53 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 07:26 | 08:27 | 08:57 | 09:29 | 09:59 | 10:29 | 10:59 | 11:29 | 11:59 |
| Junction Fair, Glebe Rd, The Junction | 07:32 | 08:34 | 09:05 | 09:37 | 10:07 | 10:37 | 11:07 | 11:37 | 12:07 |
| Darby St at Bull St, Cooks Hill | 07:36 | 08:39 | 09:09 | 09:41 | 10:11 | 10:41 | 11:11 | 11:41 | 12:11 |
| Customs House, Watt St, Newcastle | 07:43 | 08:47 | 09:18 | 09:50 | 10:20 | 10:50 | 11:20 | 11:50 | 12:20 |

Sunday & Public Holidays

| Lambton Pde at Hamilton St, Swansea Heads | 11:26 | - | 12:26 | - | 13:26 | - | 14:26 | - | 15:26 |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Swansea High School, Park Ave, Caves Beach | 11:33 | - | 12:33 | - | 13:33 | - | 14:33 | - | 15:33 |
| Pacific Hwy after Lake Rd, Swansea | 11:38 | - | 12:38 | - | 13:38 | - | 14:38 | - | 15:38 |
| Pacific Hwy at Marks Point Rd, Marks Point | 11:44 | - | 12:44 | - | 13:44 | - | 14:44 | - | 15:44 |
| Pacific Hwy before Macquarie St, Belmont | 11:50 | - | 12:50 | - | 13:49 | - | 14:49 | - | 15:49 |
| Ntaba Rd opp Jewells Plaza, Jewells | 12:00 | - | 13:00 | - | 14:00 | - | 15:00 | - | 16:00 |
| Pacific Hwy at Oxford St, Gateshead | 12:08 | - | 13:08 | - | 14:08 | - | 15:08 | - | 16:08 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 12:12 | 12:42 | 13:12 | 13:42 | 14:12 | 14:42 | 15:12 | 15:42 | 16:12 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 12:13 | 12:43 | 13:13 | 13:43 | 14:13 | 14:43 | 15:13 | 15:43 | 16:13 |
| Park Ave opp Westfield Kotara, Kotara | 12:24 | 12:53 | 13:24 | 13:53 | 14:24 | 14:53 | 15:24 | 15:53 | 16:24 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 12:29 | 12:59 | 13:29 | 13:59 | 14:29 | 14:59 | 15:29 | 15:59 | 16:29 |
| Junction Fair, Glebe Rd, The Junction | 12:37 | 13:07 | 13:37 | 14:07 | 14:37 | 15:07 | 15:37 | 16:07 | 16:37 |
| Darby St at Bull St, Cooks Hill | 12:41 | 13:11 | 13:41 | 14:11 | 14:41 | 15:11 | 15:41 | 16:11 | 16:41 |
| Customs House, Watt St, Newcastle | 12:50 | 13:20 | 13:50 | 14:20 | 14:50 | 15:20 | 15:50 | 16:20 | 16:50 |

Sunday & Public Holidays

| Lambton Pde at Hamilton St, Swansea Heads | - | 16:26 | - | 17:27 | - | 18:31 | - | 19:31 | 20:31 |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Swansea High School, Park Ave, Caves Beach | - | 16:33 | - | 17:34 | - | 18:37 | - | 19:37 | 20:37 |
| Pacific Hwy after Lake Rd, Swansea | - | 16:38 | - | 17:39 | - | 18:42 | - | 19:42 | 20:42 |
| Pacific Hwy at Marks Point Rd, Marks Point | - | 16:44 | - | 17:45 | - | 18:47 | - | 19:47 | 20:47 |
| Pacific Hwy before Macquarie St, Belmont | - | 16:49 | - | 17:50 | - | 18:52 | - | 19:52 | 20:52 |
| Ntaba Rd opp Jewells Plaza, Jewells | - | 17:00 | - | 18:00 | - | 19:01 | - | 20:01 | 21:01 |
| Pacific Hwy at Oxford St, Gateshead | - | 17:08 | - | 18:08 | - | 19:08 | - | 20:08 | 21:08 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 16:42 | 17:12 | 17:42 | 18:11 | 18:42 | 19:11 | 19:42 | 20:11 | 21:11 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 16:43 | 17:13 | 17:43 | 18:12 | 18:43 | 19:12 | 19:42 | 20:12 | 21:12 |
| Park Ave opp Westfield Kotara, Kotara | 16:53 | 17:24 | 17:53 | 18:23 | 18:53 | 19:22 | 19:52 | 20:22 | 21:22 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 16:59 | 17:29 | 17:59 | 18:28 | 18:58 | 19:27 | 19:57 | 20:27 | 21:27 |
| Junction Fair, Glebe Rd, The Junction | 17:07 | 17:37 | 18:07 | 18:35 | 19:05 | 19:34 | 20:04 | 20:34 | 21:34 |
| Darby St at Bull St, Cooks Hill | 17:11 | 17:41 | 18:11 | 18:39 | 19:09 | 19:38 | 20:08 | 20:38 | 21:38 |
| Customs House, Watt St, Newcastle | 17:20 | 17:50 | 18:19 | 18:47 | 19:16 | 19:45 | 20:15 | 20:45 | 21:45 |

Sunday & Public Holidays

| Alick St opp Spinnakers Leisure Park, Belmont | 21:48 | 22:48 | 23:48 |
|---|-------|-------|-------|
| Pacific Hwy before Macquarie St, Belmont | 21:52 | 22:52 | 23:52 |
| Ntaba Rd opp Jewells Plaza, Jewells | 22:01 | 23:01 | 00:01 |
| Pacific Hwy at Oxford St, Gateshead | 22:08 | 23:08 | 00:08 |
| Charlestown Square, Frederick St, Stand C, Charlestown | 22:11 | 23:11 | 00:11 |
| Charlestown Square, Pearson St, Stand A, Charlestown | 22:12 | 23:12 | 00:12 |
| Park Ave opp Westfield Kotara, Kotara | 22:22 | 23:22 | 00:22 |
| Adamstown Community Early Learning, Glebe Rd, Adamstown | 22:27 | 23:27 | 00:27 |
| Junction Fair, Glebe Rd, The Junction | 22:33 | 23:33 | 00:33 |
| Darby St at Bull St, Cooks Hill | 22:37 | 23:37 | 00:37 |
| Customs House, Watt St, Newcastle | 22:44 | 23:44 | 00:44 |

Appendix F

Turning Path Assessment



Attachment 4: Mine Subsidence Risk study



Douglas Partners
Geotechnics | Environment | Groundwater

Report on
Desktop Study - Mine Subsidence Risk

Lake Macquarie Private Hospital Expansion
O'Brien Street, Gateshead

Prepared for
Akalán Projects Pty Ltd

Project 16471.21
October 2016

Integrated Practical Solutions



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The undersigned, on behalf of Douglas Partners Pty Ltd, confirm that this document and all attached drawings, logs and test results have been checked and reviewed for errors, omissions and inaccuracies.

| Signature | Date |
|-----------|-----------------|
| Author | 25 October 2016 |
| Reviewer | 25 October 2016 |



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Appendix A:

About this Report

Table A.1 – Pillar Stability Analysis – Pillars as Measured / Working Section 2.4 m

Table A.2 – Pillar Stability Analysis – Run 2 - Remove Crushed Pillars from Run 1

Table A.3 – Pillar Stability Analysis – Run 3 - Decrease Run 2 Pillars by 1 m

Table A.4 – Pillar Stability Analysis – Run 4 - Run 2 Working Section Increased to 3.0 m

Table A.5 – Pillar Stability Analysis – Run 5 - Decrease Run 2 Pillars by 1 m and Increase Working Section to 3.0 m

Table A.6 – Pillar Stability Analysis – Run 2A – Remove Low FoS Pillars from Beneath Angle of Draw

Drawing 1 – Site Location Plan

Drawing 2 – Layout of Mine Workings (RT303A) and Pillar Numbering

Drawing 3 – Pillar Factor of Safety – Run 2

Drawing 4 – Pillar Factor of Safety – Run 3 (Pillars Decreased by 1 m)

Drawing 5 – Pillar Factor of Safety – Run 4 (Working Section increased to 3.0 m)

Report on Desktop Study - Mine Subsidence Risk

Lake Macquarie Private Hospital Expansion

O'Brien Street, Gateshead

1. Introduction

This report presents the results of a desktop study to assess the mine subsidence risk for the proposed expansion of Lake Macquarie Private Hospital (LMPH) at O'Brien and Casey Streets, Gateshead (Lots 3 to 8, DP24268). The work was carried out for Akalan Projects Pty Ltd.

It is understood that the current proposed development comprises the construction of a single storey structure on Lot 3, DP24268 as part of a 20 bed ward extension. The development will require excavation of about 2 m depth along the northern boundary. The proposed finished basement floor level will be at about RL 42.0 (AHD). The lift well and stairs will be installed to floor level of about 37.0 AHD, to connect with existing hospital buildings to the south. Other future development on Lots 4 to 8 is not yet known.

A desktop study was undertaken to comment on the stability of the mine workings and also to provide comments on the likely surface subsidence parameters which would result from the 'worst credible case' future mine subsidence. No subsurface investigation was undertaken for the mine subsidence assessment.

Douglas Partners Pty Ltd (DP) has previously undertaken a desktop mine subsidence risk assessment of the Stage 2 LMPH Medical Suits at 8 Sydney Street, Gateshead (Ref 1). The results of the previous assessment were referred to in the preparation of this report.

The location of the site is shown on Drawing 1, attached. The area of the current proposed development (Lot 3) is located in the south-west corner of the site area shown on Drawing 1.

2. Scope of Work

The scope of work comprised:

- A review of the plans of the mine workings (called Record Traces or RTs) and the Department of Primary Industries – Minerals' (DPI-Minerals) online DIGS data base for relevant information;
- Review of other historical documents and data from DP files;
- Pillar stability analysis for pillars under the site and within and immediately surrounding the angle of draw;
- Comment on the pillar stability and the likelihood of mine subsidence affecting the site.

3. Data Review

3.1 Extent of Mining

Previous inquiries to the Mine Subsidence Board (MSB) indicates that the site has been undermined by abandoned mine workings in the Victoria Tunnel Seam (Ref 1).

The Victoria Tunnel workings were undertaken by BHP's Burwood Colliery at a depth of about 118 m to 124 m beneath the proposed floor level of 42.0 AHD in the area beneath the site.

Scanned images of the plans of these abandoned mines were obtained from the DPI – Minerals as part of the work for Ref 1. The images were georeferenced to the modern surface cadastre provided by the Department of Lands.

3.2 Record Trace – Victoria Tunnel Seam

The Victoria Tunnel Seam workings of the Burwood Colliery are recorded on Record Tracing (RT) 303A. The relationship between the workings and the site is shown on Drawing 2, attached. Reference to this drawing indicates that the workings comprised bord and pillar workings.

The nearest areas of partial and full pillar extraction are immediately west of the site. One row of full pillar extraction is located within the angle of draw for the site. Additional rows are located west of, and outside the angle of draw.

Dates on the RT near the site indicate that mining likely occurred in the late 1960s to early 1970s.

No sections showing the seam thickness or working section are shown on the RT.

Reference to the RT indicated a working floor elevation in the range of about 219' to 229'. The datum to which these elevations referred is 500' below "high water mark (ordinary spring tide), that is 5'6" above zero of Tide Gauge Newcastle". The Newcastle Harbour Tide Gauge datum (NHTG) is at an elevation of about -1.01 AHD. Therefore, the floor of the workings is estimated to be in the range of about RL -75.7 to RL -83.6 (AHD).

With reference to the proposed floor level of 42.0 AHD, it is therefore estimated that the floor of the workings is in the range of about 118 m to 126 m below the proposed finished floor level of the site.

3.3 Historical Data

Information previously obtained from the on Lake Macquarie City Council (LMCC) website (Ref 1) indicates that Burwood Colliery was owned by the Burwood Coal Co. and opened in 1885 at Glenrock. The first shaft at Whitebridge was sunk in 1888. In 1894 the Scottish Australian Mining Co. bought it for 27,000 pounds. The Glenrock entrance was closed and a new line was built for transport. There were five shafts at Whitebridge, working three seams: the Borehole, Victoria Tunnel and Dudley. The workings extended for a kilometre under the sea and as far as Gateshead, Charlestown and Merewether.

In 1932, Burwood Colliery was purchased by BHP. It closed in 1982.

3.4 Working Section and Seam Thickness

Limited data has been found on the working section thickness of the Victoria Tunnel Seam in the immediate vicinity of the site.

A previous review of data available on Department of Industry's online DIGS database (Ref 1) indicated the following:

Table 1: Summary of Available Colliery Bore Data (source: DIGS online database)

| Colliery | Bore Number (date) | Approximate Distance of Bore from Site | Thickness of Victoria Tunnel Seam (m) | Thickness of Working Section of Victoria Tunnel Seam (m) |
|-------------------------|-----------------------------|--|---------------------------------------|--|
| BHP Windale | DDH1 (1954) | 750 m SW | 2.41 | Not indicated |
| Waratah | DDH4 (undated) | 1.2 km NE | 2.83 | Not indicated |
| BHP Windale | DDH3 (1957) | 1.4 km SSW | 3.04 | Not indicated |
| Waratah | DDH9 (1960) | 1.5 km NW | 3.20 | 1.40 ? |
| BHP Burwood Dudley | DDH2 (1955) | 1.6 km SE | 4.13 | Not indicated |
| BHP Burwood | DDH8 (1971) | 1.8 km NW | 2.74 | Not indicated |
| BHP Burwood | No 7 Fan Shaft | 1.9 km NW (?) | 2.64 | Not indicated |
| BHP Burwood Lambton | Pump Bore DDH (1958) | 2.2 km ESE | 3.87 | Not indicated |
| Waratah | DDH8 (1960) | 2.4 km NW | 3.04 | 2.26 |
| BHP Burwood Dudley | DDH1 (1954) | 2.7 km ENE | 3.93 | Not indicated |
| South Burwood or Dudley | Downcast Shaft (1890) | 2.7 km ESE | 4.14 | Not indicated |
| Burwood Dudley | DDH1 | 2.7 km ENE | 3.93 | Not indicated |
| South Burwood | Upcast Shaft (1890) | 3.3 km ESE | 3.18 | Not indicated |
| Waratah | DDH7 (1960) | 3.5 km NW | 3.04 | 2.07 |
| Waratah | DDH6-Tickhole Tunnel (1960) | 4.9 km NW | 3.11 | 2.65 |

Photo 1, below, from LMCC online archives, shows the workings in the Victoria Tunnel Seam at Burwood Colliery. Note there can be two people seen to the left of the photo. There seems to be limited headroom above standing height.



Photo 1 - Victoria Tunnel Seam, Burwood Colliery (Ref LMCC online archives)

In addition, a CSIRO report titled “Petrographic Data on some New South Wales Coals”, by G H Taylor in 1963 indicated an overall Burwood Colliery Victoria Tunnel seam thickness of about 2.79 m, and an inferred working section of about 2.19 m. It’s not known to where this data specifically related.

The 1969 “Geology of New South Wales” publication by the Geological Society of Australia (edited G H Packham) indicates that the working section of the Victoria Tunnel Seam is rarely more than 7 feet (2.1 m).

Based on a review of the available data, a seam thickness and working section thickness of 2.4 m has been assumed for the workings beneath the site. It is considered likely that this thickness represents an over-estimate of the working section beneath the site, based on the two publications referenced above, Photo 1, and the available data on the thickness of the Victoria Tunnel working section in other collieries.

A sensitivity analysis has been based on a pillar height of 3.0 m. It is considered likely that this would represent an over-estimate of the working section beneath the site.

4. Pillar Stability Analysis

Pillar stability analysis was undertaken using the UNSW Pillar Stability Formula (Ref 2). Pillars used in the analysis, and the assigned numbering system, are shown on Drawing 2, attached. When DP previously undertook a pillar stability analysis for the medical suites to the south, 81 pillars were modelled. These previously modelled pillars have been incorporated into the current model, and are numbered A1 to A81. Eighty-five additional pillars were incorporated into the model, to expand coverage to and around the current site extents. The pillars added to the current model are numbered B1 to B85.

The stability analysis was therefore undertaken for 166 pillars within and up to at least 100 m beyond the angle of draw relative to the edge of the site to the north, west and south of the site. The model was not expanded to the east of the site due to the presence of a barrier within the workings.

All pillar dimensions were measured as per RT 303A. Abutment loads were applied to pillars adjacent to areas of pillar extraction. Analysis was undertaken using an iterative process.

During the initial analysis (Run 1), some localised pillars (generally within areas of full or partial pillar extraction) indicated a likelihood of failure / crush. During the second iteration of the analysis (Run 2), it was assumed that these localised pillars had crushed, and abutment loads were transferred to surrounding pillars, where present.

Run 2 suggested that the pillars with the lowest factors of safety within the project area were generally related to pillars B41, B42 and B43. These three pillars are located within the angle of draw, but not beneath the site. They are located in an area where there has been full pillar extraction along both sides of the pillar. Run 2A (Table A.6) analysed the impact that assumed crushing of these three pillars might have on the pillars beneath the site and within the angle of draw.

In addition to the analysis referred to above, sensitivity analyses were undertaken as follows:

- Run 3: decrease the pillars in Run 2 by 1 m;
- Run 4: increase the working section height in Run 2 to 3.0 m;
- Run 5: decrease the pillars in Run 2 by 1 m and also increase the working section height to 3 m.

The attached Drawings 3 to 5 provide a graphical representation of the factors of safety for the pillars in each of Runs 2, 3 and 4. Each of Runs 3 to 5 is considered conservative. The annotations on the RT, and the recent nature of the workings suggest that it is unlikely that additional coal was taken from the pillars beyond what is shown on the RT. Based on the available information, a working section height of 3 m is considered highly unlikely. While analysis was undertaken for Run 5, a graphical representation is not provided as it is considered that the combination of two conservative sensitivity analyses is not a credible scenario.

The results of the analyses are given in Tables A.1 to A.6, attached. The results of Runs 2, 2A, 3 and 4, are summarised in Table 2, below.

Table 2: Summary of Results of Pillar Analysis (Runs 2 and 2A) and Sensitivity Analyses (Runs 3 and 4)

| Analysis Run No | 2 | 2A | 3 | 4 |
|--|---|--|--------------------------------|-----------|
| Table No in Appendix: | A.2 | A.6 | A.3 | A.4 |
| Pillar Height (m) | 2.4 | 2.4 | 2.4 | 3.0 |
| Pillar Dimensions | as per RT, with crushed pillars removed | as per RT, with low FoS pillars removed beneath site | Pillars reduced by 1 m from RT | as per RT |
| Max W:H Ratio within angle of draw | 7.8 | 7.8 | 7.4 | 6.3 |
| Min W:H Ratio within angle of draw | 6.3 | 6.3 | 5.9 | 5.1 |
| Average W:H Ratio within angle of draw | 7.1 | 7.1 | 6.6 | 5.6 |
| Min FoS within angle of draw: | 1.97 | 2.38 | 1.72 | 1.49 |
| Max FoS within angle of draw: | 4.76 | 4.76 | 4.08 | 3.54 |
| Average FoS within | 3.60 | 3.66 | 3.06 | 2.76 |

5. Comments

Based on the available data it is considered that the working section is unlikely to have been greater than 2.4 m, and is likely to have been less than 2.4 m.

Given the age of the workings ranging from late 1960's to early 1970's, the pillar dimensions are unlikely to differ significantly from that shown on the RT.

The pillars located beneath the site and within the angle of draw are somewhat "protected" by larger pillars (B16 to the north), a barrier within the workings to the east, and large areas of pillars with factors of safety greater than 3.0 to the south.

An area of full pillar extraction is located west of the site, and partly within the angle of draw. A number of pillars west of the area of pillar extraction indicated marginal stability with factors of safety less than 1.5 (e.g. B51-54), however none of these pillars are located within the angle of draw for the site. It is considered that if these pillars fail, the loss of these pillars will not increase abutment loads in the project area as pillars within higher factors of safety, and an area of full pillar extraction are located between the marginal pillars and the angle of draw. Hence, based on the layout of the mine workings, and the analysis undertaken, it is not credible for a pillar run to propagate through the site.

Pillar stability analysis based on the estimated upper limit working section height of 2.4 m and pillar dimensions shown on the RT (Run 2) demonstrates a minimum pillar factor of safety of 1.97 within the project angle of draw. After the removal of pillars B41, B42 and B43 from the analysis (Run 2A), the minimum factor of safety within the project angle of draw increases to 2.38, with an average factor of safety of 3.66. A pillar run through the site is not considered to be credible under these conditions.

If the pillar dimensions were decreased by 1.0 m from what is shown on the RT, then the minimum pillar factor of safety within the angle of draw (Run 3) decreases to 1.72, with an average factor of safety of 3.06. Given the conservative nature of the sensitivity analysis, a pillar run is also not considered to be credible under these conditions.

If the working section thickness is increased to 3.0 m height, and the pillar dimensions are as shown on the RT, then the analysis (Run 4) suggests that the minimum factor of safety within the angle of draw would be 1.49, with an average factor of safety of 2.76. As previously discussed, a working section height of greater than 2.4 is considered to be highly unlikely, hence a pillar run under these conditions is also considered not credible.

6. Conclusions

Based on the results of the above, the pillars within the project angle of draw have an acceptable factor of safety even when considering the sensitivity analyses, which model conditions which are unlikely to be present.

The risk of a pillar run propagating through the site is considered not credible.

Hence, based on the layout of the mine workings as shown on the record trace, together with historical data regarding the working section height in the Victoria Tunnel Seam, it is considered that the risk of pillar failure in the Victoria Tunnel Seam workings at this site is not credible.

7. References

1. Douglas Partners Pty Ltd, "Report on Desk Study – Mine Subsidence Risk, Lake Macquarie Private Hospital Medical Suits – Stage 2, Sydney Street, Gateshead", Project No. 16471.12 dated 26 July 2010.
2. Galvin, J M, Hebblewhite, B K, Salamon, M D G and Lin, B B, "Establishing the Strength of Rectangular and Irregular Pillars", Final Report for ACARP Project C5024, 1998.

8. Limitations

Douglas Partners Pty Ltd (DP) has prepared this report for this project at Lake Macquarie Private Hospital, O'Brien Street, Gateshead in accordance with DP's proposal NCL150797 dated 25 November 2015 and acceptance received from Mr Hector Pedrol of Akalan Project Pty Ltd dated 20 September 2016. The work was carried out under DP's Conditions of Engagement. This report is provided for the exclusive use of Akalan Project Pty Ltd for this project only and for the purposes as described in the report. It should not be used by or relied upon for other projects or purposes on the same or other site or by a third party. Any party so relying upon this report beyond its exclusive use and purpose as stated above, and without the express written consent of DP, does so entirely at its own risk and without recourse to DP for any loss or damage. In preparing this report DP has necessarily relied upon information provided by the client and/or their agents.

The results provided in the report are indicative of the sub-surface conditions on the site only at the specific sampling and/or testing locations, and then only to the depths investigated and at the time the work was carried out. Subsurface conditions can change abruptly due to variable geological processes and also as a result of human influences. Such changes may occur after DP's field testing has been completed.

DP's advice is based upon the conditions encountered during this investigation. The accuracy of the advice provided by DP in this report may be affected by undetected variations in ground conditions across the site between and beyond the sampling and/or testing locations. The advice may also be limited by budget constraints imposed by others or by site accessibility.

This report must be read in conjunction with all of the attached and should be kept in its entirety without separation of individual pages or sections. DP cannot be held responsible for interpretations or conclusions made by others unless they are supported by an expressed statement, interpretation, outcome or conclusion stated in this report.

This report, or sections from this report, should not be used as part of a specification for a project, without review and agreement by DP. This is because this report has been written as advice and opinion rather than instructions for construction.

The scope for work for this investigation/report did not include the assessment of surface or sub-surface materials or groundwater for contaminants, within or adjacent to the site. Should evidence of filling of unknown origin be noted in the report, and in particular the presence of building demolition materials, it should be recognised that there may be some risk that such filling may contain contaminants and hazardous building materials.

Douglas Partners Pty Ltd

Appendix A

About This Report

Table A.2 – Pillar Stability Analysis – Run 2 - Remove Crushed Pillars from Run 1

Table A.3 – Pillar Stability Analysis – Run 3 - Decrease Run 2 Pillars by 1 m

Table A.4 – Pillar Stability Analysis – Run 4 - Run 2 Working Section Increased to 3.0 m

Table A.5 – Pillar Stability Analysis – Run 5 - Decrease Run 2 Pillars by 1 m and Increase Working Section to 3.0 m

Table A.6 – Pillar Stability Analysis – Run 2A – Remove Low FoS Pillars from Beneath Angle of Draw

Drawing 1 – Site Location Plan

Drawing 2 – Layout of Mine Workings (RT303A) and Pillar Numbering

Drawing 3 – Pillar Factor of Safety – Run 2

Drawing 4 – Pillar Factor of Safety – Run 3 (Pillars Decreased by 1 m)

Drawing 5 – Pillar Factor of Safety – Run 4 (Working Section increased to 3.0 m)

About this Report

Douglas Partners



Introduction

These notes have been provided to amplify DP's report in regard to classification methods, field procedures and the comments section. Not all are necessarily relevant to all reports.

DP's reports are based on information gained from limited subsurface excavations and sampling, supplemented by knowledge of local geology and experience. For this reason, they must be regarded as interpretive rather than factual documents, limited to some extent by the scope of information on which they rely.

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This report is the property of Douglas Partners Pty Ltd. The report may only be used for the purpose for which it was commissioned and in accordance with the Conditions of Engagement for the commission supplied at the time of proposal. Unauthorised use of this report in any form whatsoever is prohibited.

Borehole and Test Pit Logs

The borehole and test pit logs presented in this report are an engineering and/or geological interpretation of the subsurface conditions, and their reliability will depend to some extent on frequency of sampling and the method of drilling or excavation. Ideally, continuous undisturbed sampling or core drilling will provide the most reliable assessment, but this is not always practicable or possible to justify on economic grounds. In any case the boreholes and test pits represent only a very small sample of the total subsurface profile.

Interpretation of the information and its application to design and construction should therefore take into account the spacing of boreholes or pits, the frequency of sampling, and the possibility of other than 'straight line' variations between the test locations.

Groundwater

Where groundwater levels are measured in boreholes there are several potential problems, namely:

- In low permeability soils groundwater may enter the hole very slowly or perhaps not at all during the time the hole is left open;

- A localised, perched water table may lead to an erroneous indication of the true water table;
- Water table levels will vary from time to time with seasons or recent weather changes. They may not be the same at the time of construction as are indicated in the report; and
- The use of water or mud as a drilling fluid will mask any groundwater inflow. Water has to be blown out of the hole and drilling mud must first be washed out of the hole if water measurements are to be made.

More reliable measurements can be made by installing standpipes which are read at intervals over several days, or perhaps weeks for low permeability soils. Piezometers, sealed in a particular stratum, may be advisable in low permeability soils or where there may be interference from a perched water table.

Reports

The report has been prepared by qualified personnel, is based on the information obtained from field and laboratory testing, and has been undertaken to current engineering standards of interpretation and analysis. Where the report has been prepared for a specific design proposal, the information and interpretation may not be relevant if the design proposal is changed. If this happens, DP will be pleased to review the report and the sufficiency of the investigation work.

Every care is taken with the report as it relates to interpretation of subsurface conditions, discussion of geotechnical and environmental aspects, and recommendations or suggestions for design and construction. However, DP cannot always anticipate or assume responsibility for:

- Unexpected variations in ground conditions. The potential for this will depend partly on borehole or pit spacing and sampling frequency;
- Changes in policy or interpretations of policy by statutory authorities; or
- The actions of contractors responding to commercial pressures.

If these occur, DP will be pleased to assist with investigations or advice to resolve the matter.

About this Report

Site Anomalies

In the event that conditions encountered on site during construction appear to vary from those which were expected from the information contained in the report, DP requests that it be immediately notified. Most problems are much more readily resolved when conditions are exposed rather than at some later stage, well after the event.

Information for Contractual Purposes

Where information obtained from this report is provided for tendering purposes, it is recommended that all information, including the written report and discussion, be made available. In circumstances where the discussion or comments section is not relevant to the contractual situation, it may be appropriate to prepare a specially edited document. DP would be pleased to assist in this regard and/or to make additional report copies available for contract purposes at a nominal charge.

Site Inspection

The company will always be pleased to provide engineering inspection services for geotechnical and environmental aspects of work to which this report is related. This could range from a site visit to confirm that conditions exposed are as expected, to full time engineering presence on site.

Table A.1: Pillar Stability Analysis

Run 1: Pillars As Measured

Key to Colour Coding of Factors of Safety / Width: Height Ratios

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 1
Calculations by JAW

4.50

Greater than 3.0

2.40

Between 2.2 and 3.0

2.10

Between 1.8 and 2.2

1.70

Between 1.5 and 1.8

1.20

Less than 1.5

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

| Analysis Id. | Comment | Depth D (m) | Panel Width/Span (Longwall only) (m) | Seam Thickness (m) | Working Section H (m) | Pillar Height Section H (m) | Unit Weighth γ (kN/m³) | Pillar Details | | | Adway Details | | Extract Ratio (%) | Pillar Area m² | Total Area m² | w1/Height Ratio w1/H | w2/H Height Ratio w2/H | Width/Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) ("Yield") φ _s = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|------------------|-------------------|--|-----------------------|-----------------------------|--------------------------------------|------------------------------|--------------------|---------------------|-----------------------|---------------|-----------|----------------------|-------------------|------------------|----------------------------|---------------------------------|-----------------------|----------------|---------|-----------------------|---------------------------------------|----------------------------------|--------------------------------------|---------------------|------------------------------|-----------------------------------|-----------------|---------------------------------|--|------------------------------------|-------|-------------------|--------------------------|---------|------------------------|--|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (") | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wΘ Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A1 | | 127.7 | | 2.4 | 2.4 | 2.4 | 25 | 18.6 | 31.0 | 90.0 | 4.9 | 5.2 | 32.2 | 576.6 | 850.7 | 7.8 | 12.9 | 7.75 | 1.250 | 1.250 | 23.250 | 4.71 | 2716 | 0.79 | 20 | | | | | | Yes | 23.31 | 13443 | 4.95 | 2.3E-24 | 1 in 1000000 | |
| A2 | | 126.7 | | 2.4 | 2.4 | 2.4 | 25 | 17.4 | 31.5 | 90.0 | 5.2 | 5.1 | 33.7 | 548.1 | 827.2 | 7.3 | 13.1 | 7.25 | 1.288 | 1.288 | 22.417 | 4.78 | 2619 | 0.77 | 20 | | | | | | Yes | 22.00 | 12057 | 4.60 | 3.4E-22 | 1 in 1000000 | |
| A3 | | 126.7 | | 2.4 | 2.4 | 2.4 | 25 | 19.1 | 31.4 | 90.0 | 5.3 | 5.4 | 33.2 | 599.7 | 897.9 | 8.0 | 13.1 | 7.96 | 1.244 | 1.244 | 23.752 | 4.74 | 2843 | 0.81 | 20 | | | | | | Yes | 23.99 | 14388 | 5.06 | 4.7E-25 | 1 in 1000000 | |
| A4 | Tailgate Loading | 124.6 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 16.8 | 31.4 | 90.0 | 5.4 | 5.1 | 34.9 | 527.5 | 810.3 | 7.0 | 13.1 | 7.00 | 1.303 | 1.303 | 21.889 | 4.78 | 2523 | 0.77 | 20 | A | T | | 1868 | | 8.32 | Yes | 21.34 | 11259 | 2.66 | 1.9E-09 | 1 in 1000000 |
| A5 | | 124.1 | | 2.4 | 2.4 | 2.4 | 25 | 16.5 | 31.1 | 90.0 | 5.4 | 5.2 | 35.5 | 513.2 | 795.0 | 6.9 | 13.0 | 6.88 | 1.307 | 1.307 | 21.561 | 4.81 | 2466 | 0.77 | 20 | | | | | | Yes | 21.00 | 10777 | 4.37 | 9.8E-21 | 1 in 1000000 | |
| A6 | | 123.6 | | 2.4 | 2.4 | 2.4 | 25 | 17.7 | 26.9 | 90.0 | 4.8 | 5.3 | 34.3 | 476.1 | 724.5 | 7.4 | 11.2 | 7.38 | 1.206 | 1.206 | 21.351 | 4.70 | 2238 | 0.78 | 20 | | | | | | Yes | 21.66 | 10314 | 4.61 | 3.2E-22 | 1 in 1000000 | |
| A7 | | 123.1 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 26.5 | 90.0 | 5.2 | 5.4 | 36.2 | 455.8 | 714.6 | 7.2 | 11.0 | 7.17 | 1.213 | 1.213 | 20.860 | 4.82 | 2199 | 0.78 | 20 | | | | | | Yes | 21.08 | 9606 | 4.37 | 1.0E-20 | 1 in 1000000 | |
| A8 | | 122.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.7 | 26.5 | 90.0 | 5.4 | 5.8 | 38.0 | 442.6 | 713.8 | 7.0 | 11.0 | 6.96 | 1.227 | 1.227 | 20.488 | 4.95 | 2189 | 0.77 | 20 | | | | | | Yes | 20.58 | 9106 | 4.16 | 2.0E-19 | 1 in 1000000 | |
| A9 | | 121.4 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 27.6 | 90.0 | 5.0 | 5.3 | 35.2 | 469.2 | 723.8 | 7.1 | 11.5 | 7.08 | 1.238 | 1.238 | 21.040 | 4.68 | 2196 | 0.77 | 20 | | | | | | Yes | 21.04 | 9872 | 4.50 | 1.6E-21 | 1 in 1000000 | |
| A10 | | 123.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 17.4 | 90.0 | 5.3 | 4.9 | 40.3 | 301.0 | 504.0 | 7.2 | 7.3 | 7.21 | 1.003 | 1.003 | 17.350 | 5.19 | 1561 | 0.78 | 20 | | | | | | Yes | 19.24 | 5793 | 3.71 | 1.3E-16 | 1 in 1000000 | |
| A11 | | 124.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 17.3 | 90.0 | 5.3 | 5.0 | 40.9 | 294.1 | 497.3 | 7.1 | 7.2 | 7.08 | 1.009 | 1.009 | 17.149 | 5.25 | 1544 | 0.77 | 20 | | | | | | Yes | 18.96 | 5575 | 3.61 | 5.4E-16 | 1 in 1000000 | |
| A12 | | 123.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.7 | 17.1 | 90.0 | 5.1 | 5.2 | 41.3 | 285.6 | 486.1 | 7.0 | 7.1 | 6.96 | 1.012 | 1.012 | 16.898 | 5.24 | 1498 | 0.76 | 20 | | | | | | Yes | 18.65 | 5326 | 3.56 | 1.2E-15 | 1 in 1000000 | |
| A13 | | 123.0 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 17.0 | 90.0 | 5.3 | 5.1 | 41.4 | 289.0 | 492.8 | 7.1 | 7.1 | 7.08 | 1.000 | 1.000 | 17.000 | 5.24 | 1515 | 0.78 | 20 | | | | | | Yes | 18.87 | 5454 | 3.60 | 6.4E-16 | 1 in 1000000 | |
| A14 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 17.1 | 90.0 | 5.5 | 5.7 | 43.3 | 290.7 | 513.0 | 7.1 | 7.1 | 7.08 | 1.003 | 1.003 | 17.050 | 5.38 | 1563 | 0.78 | 20 | | | | | | Yes | 18.90 | 5494 | 3.51 | 2.2E-15 | 1 in 1000000 | |
| A15 | | 128.8 | | 2.4 | 2.4 | 2.4 | 25 | 24.5 | 38.0 | 90.0 | 4.2 | 5.1 | 24.7 | 931.0 | 1237.0 | 10.2 | 15.8 | 10.21 | 1.216 | 1.216 | 29.792 | 4.28 | 3984 | 0.87 | 20 | | | | | | Yes | 33.43 | 31125 | 7.81 | 3.0E-42 | 1 in 1000000 | |
| A16 | | 128.9 | | 2.4 | 2.4 | 2.4 | 25 | 18.6 | 31.5 | 90.0 | 5.4 | 5.3 | 33.7 | 585.9 | 883.2 | 7.8 | 13.1 | 7.75 | 1.257 | 1.257 | 23.389 | 4.86 | 2846 | 0.80 | 20 | | | | | | Yes | 23.39 | 13702 | 4.81 | 1.6E-23 | 1 in 1000000 | |
| A17 | | 128.8 | | 2.4 | 2.4 | 2.4 | 25 | 20.0 | 31.7 | 90.0 | 5.3 | 5.9 | 33.4 | 634.0 | 951.3 | 8.3 | 13.2 | 8.33 | 1.226 | 1.226 | 24.526 | 4.83 | 3064 | 0.82 | 20 | | | | | | Yes | 25.21 | 15982 | 5.22 | 5.0E-26 | 1 in 1000000 | |
| A18 | | 127.3 | | 2.4 | 2.4 | 2.4 | 25 | 19.1 | 31.7 | 90.0 | 5.2 | 5.4 | 32.8 | 605.5 | 901.5 | 8.0 | 13.2 | 7.96 | 1.248 | 1.248 | 23.837 | 4.74 | 2869 | 0.80 | 20 | | | | | | Yes | 24.03 | 14552 | 5.07 | 4.0E-25 | 1 in 1000000 | |
| A19 | | 125.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 31.5 | 90.0 | 5.2 | 5.5 | 34.8 | 535.5 | 821.4 | 7.1 | 13.1 | 7.08 | 1.299 | 1.299 | 22.082 | 4.83 | 2585 | 0.77 | 20 | | | | | | Yes | 21.57 | 11549 | 4.47 | 2.4E-21 | 1 in 1000000 | |
| A20 | | 125.1 | | 2.4 | 2.4 | 2.4 | 25 | 16.3 | 31.5 | 90.0 | 5.3 | 5.4 | 35.6 | 513.5 | 797.0 | 6.8 | 13.1 | 6.79 | 1.318 | 1.318 | 21.483 | 4.85 | 2493 | 0.76 | 20 | | | | | | Yes | 20.85 | 10704 | 4.29 | 2.9E-20 | 1 in 1000000 | |
| A21 | | 124.4 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 16.0 | 90.0 | 5.3 | 5.0 | 41.8 | 275.2 | 472.5 | 7.2 | 6.7 | 6.67 | 0.964 | 0.964 | 16.578 | 5.34 | 1469 | 0.78 | 20 | | | | | | Yes | 18.74 | 5159 | 3.51 | 2.3E-15 | 1 in 1000000 | |
| A22 | | 123.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 16.4 | 90.0 | 5.2 | 5.0 | 41.2 | 282.1 | 479.4 | 7.2 | 6.8 | 6.83 | 0.976 | 0.976 | 16.790 | 5.27 | 1485 | 0.78 | 20 | | | | | | Yes | 18.87 | 5322 | 3.58 | 8.0E-16 | 1 in 1000000 | |
| A23 | | 123.6 | | 2.4 | 2.4 | 2.4 | 25 | 17.4 | 16.4 | 90.0 | 4.8 | 5.3 | 40.8 | 285.4 | 481.7 | 7.3 | 6.8 | 6.83 | 0.970 | 0.970 | 16.885 | 5.22 | 1489 | 0.77 | 20 | | | | | | Yes | 19.04 | 5433 | 3.65 | 3.1E-16 | 1 in 1000000 | |
| A24 | | 123.0 | | 2.4 | 2.4 | 2.4 | 25 | 17.4 | 16.4 | 90.0 | 5.3 | 5.2 | 41.8 | 285.4 | 490.3 | 7.3 | 6.8 | 6.83 | 0.970 | 0.970 | 16.885 | 5.28 | 1508 | 0.78 | 20 | | | | | | Yes | 19.04 | 5433 | 3.60 | 6.0E-16 | 1 in 1000000 | |
| A25 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.4 | 16.4 | 90.0 | 5.3 | 5.3 | 42.1 | 285.4 | 492.6 | 7.3 | 6.8 | 6.83 | 0.970 | 0.970 | 16.885 | 5.26 | 1501 | 0.78 | 20 | | | | | | Yes | 19.04 | 5433 | 3.62 | 4.8E-16 | 1 in 1000000 | |
| A26 | Tailgate Loading | 129.9 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 20.5 | 23.8 | 90.0 | 5.4 | 6.2 | 37.2 | 487.9 | 777.0 | 8.5 | 9.9 | 8.54 | 1.074 | 1.074</ | | | | | | | | | | | | | | | | | |

Table A.1: Pillar Stability Analysis

Run 1: Pillars As Measured

Key to Colour Coding of Factors of Safety / Width: Height Ratios

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 1
Calculations by JAW

| | |
|------|--|
| 4.50 | Greater than 3.0 |
| 2.40 | Between 2.2 and 3.0 |
| 2.10 | Between 1.8 and 2.2 |
| 1.70 | Between 1.5 and 1.8 |
| 1.20 | Less than 1.5 |
| | Indicating Pillar Located within Project Angle of Draw |
| | Indicating Pillar Located beneath site |

| Analysis Id. | Comment | Depth D (m) | Panel Width/Span (Longwall only) (m) | Seam Thickness (m) | Working Section H (m) | Pillar Height Section H (m) | Unit Weight γ (kN/m³) | Pillar Details | | | Adjoint Data | | Extract Ratio (%) | Pillar Area m³ | Total Area m³ | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Strength | Power Law | | Probability of Failure NSW Power Formulae | |
|--------------|------------------|-------------------|--|-----------------------|-----------------------------|-----------------------------------|-----------------------------|--------------------|---------------------|-----------------------|--------------|-----------|----------------------|-------------------|------------------|--------------------------|---------------------------|---------------------|----------------|-------|-----------------------|---------------------------------------|----------------------------------|-----------------------------------|------------------|------------------------|--------------------------------|-----------------|------------------------------|---|---------------------------------|--------|----------|-----------|----------|--|------------------------|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (°) | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wΘ Effective Width | | | | | | | | | | | | (MPa) | (MN) | FoS | | Probability of Failure |
| A74 | | 122.3 | | 2.4 | 2.4 | 2.4 | 25 | 16.4 | 17.4 | 90.0 | 5.5 | 5.2 | 42.3 | 285.4 | 494.9 | 6.8 | 7.3 | 6.83 | 1.030 | 1.030 | 16.885 | 5.30 | 1513 | 0.77 | 20 | | | | | | Yes | 18.49 | 5276 | 3.49 | 3.2E-15 | 1 in 1000000 | |
| A75 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 16.6 | 16.9 | 90.0 | 5.2 | 5.4 | 42.3 | 280.5 | 486.1 | 6.9 | 7.0 | 6.92 | 1.009 | 1.009 | 16.749 | 5.28 | 1480 | 0.77 | 20 | | | | | | Yes | 18.51 | 5194 | 3.51 | 2.4E-15 | 1 in 1000000 | |
| A76 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 16.6 | 17.1 | 90.0 | 4.8 | 5.7 | 41.8 | 283.9 | 487.9 | 6.9 | 7.1 | 6.92 | 1.015 | 1.015 | 16.846 | 5.23 | 1486 | 0.76 | 20 | | | | | | Yes | 18.57 | 5271 | 3.55 | 1.3E-15 | 1 in 1000000 | |
| A77 | | 121.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.6 | 17.0 | 90.0 | 5.0 | 5.0 | 40.6 | 282.2 | 475.2 | 6.9 | 7.1 | 6.92 | 1.012 | 1.012 | 16.798 | 5.10 | 1440 | 0.76 | 20 | | | | | | Yes | 18.54 | 5233 | 3.63 | 3.9E-16 | 1 in 1000000 | |
| A78 | Maingate Loading | 121.8 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 16.5 | 29.9 | 90.0 | 5.3 | 4.4 | 34.0 | 493.4 | 747.7 | 6.9 | 12.5 | 6.88 | 1.289 | 1.289 | 21.265 | 4.62 | 2277 | 0.77 | 20 | A | M | | 985 | | 6.61 | Yes | 20.85 | 10288 | 3.15 | 3.9E-13 | 1 in 1000000 |
| A79 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 16.2 | 17.6 | 90.0 | 6.6 | 5.3 | 45.4 | 285.1 | 522.1 | 6.8 | 7.3 | 6.75 | 1.041 | 1.041 | 16.871 | 5.58 | 1591 | 0.79 | 20 | | | | | | Yes | 18.38 | 5241 | 3.29 | 5.2E-14 | 1 in 1000000 | |
| A80 | Tailgate Loading | 125.6 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 18.5 | 31.5 | 90.0 | 23.2 | 5.0 | 61.7 | 582.8 | 1522.1 | 7.7 | 13.1 | 7.71 | 1.260 | 1.260 | 23.310 | 8.20 | 4779 | 0.98 | 20 | A | T | | 3305 | | 13.87 | Yes | 23.27 | 13558 | 1.68 | 6.6E-04 | 1 in 1777 |
| A81 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 15.4 | 17.5 | 90.0 | 5.2 | 5.1 | 42.1 | 269.5 | 465.6 | 6.4 | 7.3 | 6.42 | 1.064 | 1.064 | 16.383 | 5.26 | 1418 | 0.74 | 20 | | | | | | Yes | 17.75 | 4785 | 3.38 | 1.6E-14 | 1 in 1000000 | |
| B1 | | 121.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 15.9 | 90.0 | 5.4 | 6.7 | 46.5 | 273.5 | 510.8 | 7.2 | 6.6 | 6.63 | 0.961 | 0.961 | 16.524 | 5.66 | 1548 | 0.78 | 20 | | | | | | Yes | 18.71 | 5118 | 3.31 | 4.3E-14 | 1 in 1000000 | |
| B2 | | 120.6 | | 2.4 | 2.4 | 2.4 | 25 | 16.8 | 15.9 | 90.0 | 5.4 | 6.7 | 46.8 | 267.1 | 501.7 | 7.0 | 6.6 | 6.63 | 0.972 | 0.972 | 16.338 | 5.66 | 1513 | 0.78 | 20 | | | | | | Yes | 18.39 | 4911 | 3.25 | 1.0E-13 | 1 in 1000000 | |
| B3 | | 120.1 | | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 15.4 | 90.0 | 5.4 | 6.7 | 47.9 | 246.4 | 472.9 | 6.7 | 6.4 | 6.42 | 0.981 | 0.981 | 15.694 | 5.76 | 1420 | 0.76 | 20 | | | | | | Yes | 17.62 | 4342 | 3.06 | 1.5E-12 | 1 in 1000000 | |
| B4 | | 120.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 15.7 | 90.0 | 5.4 | 5.0 | 42.2 | 271.6 | 469.9 | 7.2 | 6.5 | 6.54 | 0.952 | 0.952 | 16.461 | 5.20 | 1412 | 0.79 | 20 | | | | | | Yes | 18.73 | 5088 | 3.60 | 6.0E-16 | 1 in 1000000 | |
| B5 | | 119.6 | | 2.4 | 2.4 | 2.4 | 25 | 16.9 | 15.8 | 90.0 | 5.4 | 5.0 | 42.4 | 267.0 | 463.8 | 7.0 | 6.6 | 6.58 | 0.966 | 0.966 | 16.331 | 5.19 | 1387 | 0.78 | 20 | | | | | | Yes | 18.44 | 4923 | 3.55 | 1.3E-15 | 1 in 1000000 | |
| B6 | | 119.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 16.1 | 90.0 | 5.4 | 5.0 | 41.8 | 278.5 | 479.0 | 7.2 | 6.7 | 6.71 | 0.964 | 0.964 | 16.678 | 5.12 | 1427 | 0.79 | 20 | | | | | | Yes | 18.86 | 5253 | 3.68 | 2.0E-16 | 1 in 1000000 | |
| B7 | | 118.6 | | 2.4 | 2.4 | 2.4 | 25 | 18.3 | 24.6 | 90.0 | 5.4 | 5.2 | 36.3 | 450.2 | 706.3 | 7.6 | 10.3 | 7.63 | 1.147 | 1.147 | 20.987 | 4.65 | 2094 | 0.81 | 20 | | | | | | Yes | 21.90 | 9860 | 4.71 | 7.5E-23 | 1 in 1000000 | |
| B8 | | 119.0 | | 2.4 | 2.4 | 2.4 | 25 | 18.1 | 24.9 | 90.0 | 5.4 | 5.2 | 36.3 | 450.7 | 707.4 | 7.5 | 10.4 | 7.54 | 1.158 | 1.158 | 20.962 | 4.67 | 2104 | 0.80 | 20 | | | | | | Yes | 21.74 | 9799 | 4.66 | 1.6E-22 | 1 in 1000000 | |
| B9 | | 120.0 | | 2.4 | 2.4 | 2.4 | 25 | 18.0 | 24.9 | 90.0 | 5.4 | 5.2 | 36.4 | 448.2 | 704.3 | 7.5 | 10.4 | 7.50 | 1.161 | 1.161 | 20.895 | 4.71 | 2113 | 0.80 | 20 | | | | | | Yes | 21.64 | 9697 | 4.59 | 4.2E-22 | 1 in 1000000 | |
| B10 | | 121.3 | | 2.4 | 2.4 | 2.4 | 25 | 18.8 | 24.7 | 90.0 | 5.4 | 5.2 | 35.8 | 464.4 | 723.6 | 7.8 | 10.3 | 7.83 | 1.136 | 1.136 | 21.350 | 4.73 | 2194 | 0.81 | 20 | | | | | | Yes | 22.48 | 10439 | 4.76 | 3.7E-23 | 1 in 1000000 | |
| B11 | Maingate Loading | 121.8 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 15.2 | 40.0 | 90.0 | 6.1 | 4.8 | 36.3 | 608.0 | 954.2 | 6.3 | 16.7 | 6.33 | 1.449 | 1.449 | 22.029 | 4.78 | 2906 | 0.76 | 20 | A | M | | 1310 | | 6.93 | Yes | 20.56 | 12498 | 2.96 | 5.9E-12 | 1 in 1000000 |
| B12 | | 121.0 | | 2.4 | 2.4 | 2.4 | 25 | 18.6 | 19.0 | 90.0 | 5.4 | 5.2 | 39.2 | 353.4 | 580.8 | 7.8 | 7.9 | 7.75 | 1.011 | 1.011 | 18.798 | 4.97 | 1757 | 0.81 | 20 | | | | | | Yes | 20.92 | 7393 | 4.21 | 1.0E-19 | 1 in 1000000 | |
| B13 | | 119.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.8 | 18.7 | 90.0 | 5.4 | 5.2 | 40.8 | 314.2 | 530.6 | 7.0 | 7.8 | 7.00 | 1.054 | 1.054 | 17.699 | 5.05 | 1588 | 0.78 | 20 | | | | | | Yes | 19.15 | 6017 | 3.79 | 4.1E-17 | 1 in 1000000 | |
| B14 | | 118.4 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 18.7 | 90.0 | 5.4 | 5.2 | 40.5 | 321.6 | 540.1 | 7.2 | 7.8 | 7.17 | 1.042 | 1.042 | 17.919 | 4.97 | 1599 | 0.79 | 20 | | | | | | Yes | 19.50 | 6273 | 3.92 | 6.0E-18 | 1 in 1000000 | |
| B15 | | 117.7 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 19.5 | 90.0 | 5.4 | 5.2 | 39.8 | 337.4 | 560.7 | 7.2 | 8.1 | 7.21 | 1.060 | 1.060 | 18.334 | 4.89 | 1650 | 0.79 | 20 | | | | | | Yes | 19.79 | 6677 | 4.05 | 1.0E-18 | 1 in 1000000 | |
| B16 | | 119.0 | | 2.4 | 2.4 | 2.4 | 25 | 63.4 | 42.3 | 90.0 | 5.4 | 5.2 | 17.9 | 2681.8 | 3268.0 | 26.4 | 17.6 | 17.63 | 0.800 | 0.800 | 50.744 | 3.63 | 9722 | 1.01 | 20 | | | | | | Yes | 173.66 | 465736 | 47.90 | 8.0E-293 | 1 in 1000000 | |
| B17 | | 119.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.1 | 31.1 | 90.0 | 5.5 | 5.7 | 37.0 | 500.7 | 794.9 | 6.7 | 13.0 | 6.71 | 1.318 | 1.318 | 21.217 | 4.75 | 2379 | 0.77 | 20 | | | | | | Yes | 20.61 | 10318 | 4.34 | 1.6E-20 | 1 in 1000000 | |
| B18 | Tailgate Loading | 119.9 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 16.7 | 31.1 | 90.0 | 5.6 | 5.7 | 36.7 | 519.4 | 820.6 | 7.0 | 13.0 | 6.96 | 1.301 | 1.301 | 21.731 | 4.74 | 2460 | 0. | | | | | | | | | | | | | |

Table A.1: Pillar Stability Analysis

Run 1: Pillars As Measured

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 1
Calculations by JAW

Key to Colour Coding of Factors of Safety / Width: Height Ratios

4.50

Greater than 3.0

2.40

Between 2.2 and 3.0

2.10

Between 1.8 and 2.2

1.70

Between 1.5 and 1.8

1.20

Less than 1.5

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

| Analysis Id: | Comment | Depth | Panel Width/Span (Longwall only) | Seam Thickness | Working Section | Pillar Height Section | Unit Weighth γ (kN/m³) | Pillar Details | | | adway Det | | Extract. Ratio | Pillar Area | Total Area | w1/ Height Ratio | w2/H Height Ratio | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment Transfer R | Abutment Angle ° | Abut (A) Yield (Y) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|----------------------------------|-------|-------------------------------------|----------------|-----------------|-----------------------|------------------------------|----------------|--------|-----------------------|-----------|-----------|----------------|-------------|------------|------------------------|-------------------------|---------------------------|----------------|-------|-----------------------|---------------------------------------|----------------------------------|-----------------------------------|------------------|-----------------------|-----------------------------------|-----------------|---------------------------------|--|------------------------------------|-------|-------------------|-----------------------|------|------------------------|--|
| | | | | | | | | Width | Length | Internal Angle (") | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wΘ Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| B66 | Double Goaf Loading | 119.5 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 24.7 | 16.2 | 90.0 | 5.5 | 5.0 | 37.5 | 400.1 | 640.2 | 10.3 | 6.8 | 6.75 | 0.792 | 0.792 | 19.567 | 4.78 | 1913 | 0.90 | 20 | A | G | | 2113 | | 10.06 | Yes | 27.21 | 10888 | 2.70 | 2.5E-10 | 1 in 1000000 |
| B67 | Tailgate Loading | 119.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 24.7 | 16.2 | 90.0 | 5.5 | 5.2 | 38.1 | 400.1 | 646.3 | 10.3 | 6.8 | 6.75 | 0.792 | 0.792 | 19.567 | 4.81 | 1923 | 0.90 | 20 | A | T | | 1803 | | 9.31 | Yes | 27.21 | 10888 | 2.92 | 1.1E-11 | 1 in 1000000 |
| B68 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.8 | 37.9 | 432.0 | 695.4 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.83 | 2086 | 0.76 | 20 | A | G | | 3287 | | 12.44 | Yes | 19.99 | 8636 | 1.61 | 1.4E-03 | 1 in 705 |
| B69 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.8 | 37.9 | 432.0 | 695.4 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.83 | 2086 | 0.76 | 20 | A | G | | 3287 | | 12.44 | Yes | 19.99 | 8636 | 1.61 | 1.4E-03 | 1 in 705 |
| B70 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.6 | 37.5 | 432.0 | 691.1 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.80 | 2073 | 0.76 | 20 | A | G | | 3267 | | 12.36 | Yes | 19.99 | 8636 | 1.62 | 1.3E-03 | 1 in 801 |
| B71 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.7 | 37.7 | 432.0 | 693.2 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.81 | 2080 | 0.76 | 20 | A | G | | 3277 | | 12.40 | Yes | 19.99 | 8636 | 1.61 | 1.3E-03 | 1 in 751 |
| B72 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.7 | 37.7 | 432.0 | 693.2 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.81 | 2080 | 0.76 | 20 | A | G | | 3277 | | 12.40 | Yes | 19.99 | 8636 | 1.61 | 1.3E-03 | 1 in 751 |
| B73 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.9 | 38.1 | 432.0 | 697.5 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.84 | 2092 | 0.76 | 20 | A | G | | 3297 | | 12.48 | Yes | 19.99 | 8636 | 1.60 | 1.5E-03 | 1 in 662 |
| B74 | Double Goaf Loading | 118.2 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 25.3 | 15.5 | 90.0 | 5.5 | 5.3 | 38.8 | 392.2 | 640.6 | 10.5 | 6.5 | 6.46 | 0.760 | 0.760 | 19.223 | 4.83 | 1893 | 0.91 | 20 | A | G | | 2043 | | 10.04 | Yes | 27.67 | 10849 | 2.76 | 1.2E-10 | 1 in 1000000 |
| B75 | Double Goaf Loading | 118.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 25.1 | 15.5 | 90.0 | 5.5 | 5.8 | 40.3 | 389.1 | 651.8 | 10.5 | 6.5 | 6.46 | 0.764 | 0.764 | 19.165 | 4.94 | 1923 | 0.91 | 20 | A | G | | 2087 | | 10.31 | Yes | 27.39 | 10655 | 2.66 | 4.9E-10 | 1 in 1000000 |
| B76 | Maingate Loading | 117.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 26.4 | 15.6 | 90.0 | 5.5 | 5.3 | 38.2 | 411.8 | 666.7 | 11.0 | 6.5 | 6.50 | 0.743 | 0.743 | 19.611 | 4.74 | 1950 | 0.92 | 20 | A | M | | 1090 | | 7.38 | Yes | 29.30 | 12067 | 3.97 | 3.1E-18 | 1 in 1000000 |
| B77 | Rotated panel / Maingate Loading | 118.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.4 | 27.7 | 90.0 | 5.7 | 5.3 | 38.7 | 426.6 | 696.3 | 6.4 | 11.5 | 6.42 | 1.285 | 1.285 | 19.795 | 4.82 | 2054 | 0.76 | 20 | A | M | | 1440 | | 8.19 | Yes | 19.55 | 8340 | 2.39 | 2.4E-08 | 1 in 1000000 |
| B78 | Rotated panel / Maingate Loading | 119.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.3 | 27.3 | 90.0 | 5.6 | 5.3 | 38.7 | 417.7 | 681.3 | 6.4 | 11.4 | 6.38 | 1.282 | 1.282 | 19.610 | 4.85 | 2027 | 0.75 | 20 | A | M | | 1423 | | 8.26 | Yes | 19.41 | 8109 | 2.35 | 4.1E-08 | 1 in 1000000 |
| B79 | Rotated panel / Maingate Loading | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 27.3 | 90.0 | 5.4 | 5.3 | 37.9 | 423.2 | 681.3 | 6.5 | 11.4 | 6.46 | 1.276 | 1.276 | 19.773 | 4.83 | 2044 | 0.75 | 20 | A | M | | 1428 | | 8.20 | Yes | 19.59 | 8288 | 2.39 | 2.4E-08 | 1 in 1000000 |
| B80 | Rotated panel / Maingate Loading | 121.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 27.3 | 90.0 | 5.7 | 5.3 | 38.8 | 423.2 | 691.1 | 6.5 | 11.4 | 6.46 | 1.276 | 1.276 | 19.773 | 4.94 | 2091 | 0.76 | 20 | A | M | | 1463 | | 8.40 | Yes | 19.59 | 8288 | 2.33 | 5.3E-08 | 1 in 1000000 |
| B81 | Rotated panel / Maingate Loading | 122.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 27.3 | 90.0 | 5.6 | 5.3 | 38.5 | 423.2 | 687.9 | 6.5 | 11.4 | 6.46 | 1.276 | 1.276 | 19.773 | 4.96 | 2098 | 0.75 | 20 | A | M | | 1467 | | 8.42 | Yes | 19.59 | 8288 | 2.32 | 5.9E-08 | 1 in 1000000 |
| B82 | Rotated panel / Maingate Loading | 123.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 27.3 | 90.0 | 5.6 | 5.3 | 38.5 | 423.2 | 687.9 | 6.5 | 11.4 | 6.46 | 1.276 | 1.276 | 19.773 | 5.00 | 2115 | 0.75 | 20 | A | M | | 1479 | | 8.49 | Yes | 19.59 | 8288 | 2.31 | 7.7E-08 | 1 in 1000000 |
| B83 | | 113.0 | | 2.4 | 2.4 | 2.4 | 25 | 13.6 | 9.9 | 90.0 | 5.4 | 6.2 | 56.0 | 134.6 | 305.9 | 5.7 | 4.1 | 4.13 | 0.843 | 0.859 | 11.679 | 6.42 | 864 | 0.72 | 21 | A | M | | 89 | | 7.08 | Yes | 14.47 | 1948 | 2.04 | 3.4E-06 | 1 in 450037 |
| B84 | | 113.5 | | 2.4 | 2.4 | 2.4 | 25 | 14.0 | 9.6 | 90.0 | 5.6 | 6.2 | 56.6 | 134.4 | 309.7 | 5.8 | 4.0 | 4.00 | 0.814 | 0.823 | 11.521 | 6.54 | 879 | 0.74 | 22 | A | M | | 92 | | 7.23 | Yes | 14.45 | 1942 | 2.00 | 6.4E-06 | 1 in 215774 |
| B85 | | 113.8 | | 2.4 | 2.4 | 2.4 | 25 | 13.8 | 10.0 | 90.0 | 5.4 | 5.3 | 53.0 | 138.0 | 293.8 | 5.8 | 4.2 | 4.17 | 0.840 | 0.853 | 11.766 | 6.06 | 836 | 0.73 | 23 | A | M | | 85 | | 6.67 | Yes | 14.56 | 2009 | 2.18 | 4.6E-07 | 1 in 1000000 |

Table A.2: Pillar Stability Analysis

Run 2: Remove Crushed Pillars from Run 1

Key to Colour Coding of Factors of Safety / Width: Height Ratios

| | |
|------|---------------------|
| 4.50 | Greater than 3.0 |
| 2.40 | Between 2.2 and 3.0 |
| 2.10 | Between 1.8 and 2.2 |
| 1.70 | Between 1.5 and 1.8 |
| 1.20 | Less than 1.5 |

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 2
Calculations by JAW

| Analysis Id. | Comment | Depth | Panel Width/Span (Longwall only) | Seam Thickness | Working Section | Pillar Height Section | Unit Weight γ (kN/m³) | Pillar Details | | | Adway Deta | | Extract. Ratio | Pillar Area | Total Area | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment Transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Strength | Power Law | | Probability of Failure NSW Power Formulae | |
|--------------|------------------|-------|-------------------------------------|----------------|-----------------|-----------------------|-----------------------------|--------------------|---------------------|--------------------------|------------|-----------|----------------|-------------|------------|--------------------------------|---------------------------------|---------------------------|----------------|-------|--------------------|---------------------------------------|----------------------------------|--------------------------------------|------------------|------------------------------|-----------------------------------|-----------------|---------------------------------|---|------------------------------------|-------|----------|-----------|---------|--|--------------|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (°) | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | Effective Width | | | | | | | | | | | | (MPa) | (MN) | (MPa) | | (MN) |
| A1 | | 127.7 | | 2.4 | 2.4 | 2.4 | 25 | 18.6 | 31.0 | 90.0 | 4.9 | 5.2 | 32.2 | 576.6 | 850.7 | 7.8 | 12.9 | 7.75 | 1.250 | 1.250 | 23.250 | 4.71 | 2716 | 0.79 | 20 | | | | | | Yes | 23.31 | 13443 | 4.95 | 2.3E-24 | 1 in 1000000 | |
| A2 | | 126.7 | | 2.4 | 2.4 | 2.4 | 25 | 17.4 | 31.5 | 90.0 | 5.2 | 5.1 | 33.7 | 548.1 | 827.2 | 7.3 | 13.1 | 7.25 | 1.288 | 1.288 | 22.417 | 4.78 | 2619 | 0.77 | 20 | | | | | | Yes | 22.00 | 12057 | 4.60 | 3.4E-22 | 1 in 1000000 | |
| A3 | | 126.7 | | 2.4 | 2.4 | 2.4 | 25 | 19.1 | 31.4 | 90.0 | 5.3 | 5.4 | 33.2 | 599.7 | 897.9 | 8.0 | 13.1 | 7.96 | 1.244 | 1.244 | 23.752 | 4.74 | 2843 | 0.81 | 20 | | | | | | Yes | 23.99 | 14388 | 5.06 | 4.7E-25 | 1 in 1000000 | |
| A4 | Tailgate Loading | 124.6 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 16.8 | 31.4 | 90.0 | 5.4 | 5.1 | 34.9 | 527.5 | 810.3 | 7.0 | 13.1 | 7.00 | 1.303 | 1.303 | 21.889 | 4.78 | 2523 | 0.77 | 20 | A | T | | 1868 | | 8.32 | Yes | 21.34 | 11259 | 2.66 | 1.9E-09 | 1 in 1000000 |
| A5 | | 124.1 | | 2.4 | 2.4 | 2.4 | 25 | 16.5 | 31.1 | 90.0 | 5.4 | 5.2 | 35.5 | 513.2 | 795.0 | 6.9 | 13.0 | 6.88 | 1.307 | 1.307 | 21.561 | 4.81 | 2466 | 0.77 | 20 | | | | | | Yes | 21.00 | 10777 | 4.37 | 9.8E-21 | 1 in 1000000 | |
| A6 | | 123.6 | | 2.4 | 2.4 | 2.4 | 25 | 17.7 | 26.9 | 90.0 | 4.8 | 5.3 | 34.3 | 476.1 | 724.5 | 7.4 | 11.2 | 7.38 | 1.206 | 1.206 | 21.351 | 4.70 | 2238 | 0.78 | 20 | | | | | | Yes | 21.66 | 10314 | 4.61 | 3.2E-22 | 1 in 1000000 | |
| A7 | | 123.1 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 26.5 | 90.0 | 5.2 | 5.4 | 36.2 | 455.8 | 714.6 | 7.2 | 11.0 | 7.17 | 1.213 | 1.213 | 20.860 | 4.82 | 2199 | 0.78 | 20 | | | | | | Yes | 21.08 | 9606 | 4.37 | 1.0E-20 | 1 in 1000000 | |
| A8 | | 122.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.7 | 26.5 | 90.0 | 5.4 | 5.8 | 38.0 | 442.6 | 713.8 | 7.0 | 11.0 | 6.96 | 1.227 | 1.227 | 20.488 | 4.95 | 2189 | 0.77 | 20 | | | | | | Yes | 20.58 | 9106 | 4.16 | 2.0E-19 | 1 in 1000000 | |
| A9 | | 121.4 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 27.6 | 90.0 | 5.0 | 5.3 | 35.2 | 469.2 | 723.8 | 7.1 | 11.5 | 7.08 | 1.238 | 1.238 | 21.040 | 4.68 | 2196 | 0.77 | 20 | | | | | | Yes | 21.04 | 9872 | 4.50 | 1.6E-21 | 1 in 1000000 | |
| A10 | | 123.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 17.4 | 90.0 | 5.3 | 4.9 | 40.3 | 301.0 | 504.0 | 7.2 | 7.3 | 7.21 | 1.003 | 1.003 | 17.350 | 5.19 | 1561 | 0.78 | 20 | | | | | | Yes | 19.24 | 5793 | 3.71 | 1.3E-16 | 1 in 1000000 | |
| A11 | | 124.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 17.3 | 90.0 | 5.3 | 5.0 | 40.9 | 294.1 | 497.3 | 7.1 | 7.2 | 7.08 | 1.009 | 1.009 | 17.149 | 5.25 | 1544 | 0.77 | 20 | | | | | | Yes | 18.96 | 5575 | 3.61 | 5.4E-16 | 1 in 1000000 | |
| A12 | | 123.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.7 | 17.1 | 90.0 | 5.1 | 5.2 | 41.3 | 285.6 | 486.1 | 7.0 | 7.1 | 6.96 | 1.012 | 1.012 | 16.898 | 5.24 | 1498 | 0.76 | 20 | | | | | | Yes | 18.65 | 5326 | 3.56 | 1.2E-15 | 1 in 1000000 | |
| A13 | | 123.0 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 17.0 | 90.0 | 5.3 | 5.1 | 41.4 | 289.0 | 492.8 | 7.1 | 7.1 | 7.08 | 1.000 | 1.000 | 17.000 | 5.24 | 1515 | 0.78 | 20 | | | | | | Yes | 18.87 | 5454 | 3.60 | 6.4E-16 | 1 in 1000000 | |
| A14 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 17.1 | 90.0 | 5.5 | 5.7 | 43.3 | 290.7 | 513.0 | 7.1 | 7.1 | 7.08 | 1.003 | 1.003 | 17.050 | 5.38 | 1563 | 0.78 | 20 | | | | | | Yes | 18.90 | 5494 | 3.51 | 2.2E-15 | 1 in 1000000 | |
| A15 | | 128.8 | | 2.4 | 2.4 | 2.4 | 25 | 24.5 | 38.0 | 90.0 | 4.2 | 5.1 | 24.7 | 931.0 | 1237.0 | 10.2 | 15.8 | 10.21 | 1.216 | 1.216 | 29.792 | 4.28 | 3984 | 0.87 | 20 | | | | | | Yes | 33.43 | 31125 | 7.81 | 3.0E-42 | 1 in 1000000 | |
| A16 | | 128.9 | | 2.4 | 2.4 | 2.4 | 25 | 18.6 | 31.5 | 90.0 | 5.4 | 5.3 | 33.7 | 585.9 | 883.2 | 7.8 | 13.1 | 7.75 | 1.257 | 1.257 | 23.389 | 4.86 | 2846 | 0.80 | 20 | | | | | | Yes | 23.39 | 13702 | 4.81 | 1.6E-23 | 1 in 1000000 | |
| A17 | | 128.8 | | 2.4 | 2.4 | 2.4 | 25 | 20.0 | 31.7 | 90.0 | 5.3 | 5.9 | 33.4 | 634.0 | 951.3 | 8.3 | 13.2 | 8.33 | 1.226 | 1.226 | 24.526 | 4.83 | 3064 | 0.82 | 20 | | | | | | Yes | 25.21 | 15982 | 5.22 | 5.0E-26 | 1 in 1000000 | |
| A18 | | 127.3 | | 2.4 | 2.4 | 2.4 | 25 | 19.1 | 31.7 | 90.0 | 5.2 | 5.4 | 32.8 | 605.5 | 901.5 | 8.0 | 13.2 | 7.96 | 1.248 | 1.248 | 23.837 | 4.74 | 2869 | 0.80 | 20 | | | | | | Yes | 24.03 | 14552 | 5.07 | 4.0E-25 | 1 in 1000000 | |
| A19 | | 125.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 31.5 | 90.0 | 5.2 | 5.5 | 34.8 | 535.5 | 821.4 | 7.1 | 13.1 | 7.08 | 1.299 | 1.299 | 22.082 | 4.83 | 2585 | 0.77 | 20 | | | | | | Yes | 21.57 | 11549 | 4.47 | 2.4E-21 | 1 in 1000000 | |
| A20 | | 125.1 | | 2.4 | 2.4 | 2.4 | 25 | 16.3 | 31.5 | 90.0 | 5.3 | 5.4 | 35.6 | 513.5 | 797.0 | 6.8 | 13.1 | 6.79 | 1.318 | 1.318 | 21.483 | 4.85 | 2493 | 0.76 | 20 | | | | | | Yes | 20.85 | 10704 | 4.29 | 2.9E-20 | 1 in 1000000 | |
| A21 | | 124.4 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 16.0 | 90.0 | 5.3 | 5.0 | 41.8 | 275.2 | 472.5 | 7.2 | 6.7 | 6.67 | 0.964 | 0.964 | 16.578 | 5.34 | 1469 | 0.78 | 20 | | | | | | Yes | 18.74 | 5159 | 3.51 | 2.3E-15 | 1 in 1000000 | |
| A22 | | 123.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 16.4 | 90.0 | 5.2 | 5.0 | 41.2 | 282.1 | 479.4 | 7.2 | 6.8 | 6.83 | 0.976 | 0.976 | 16.790 | 5.27 | 1485 | 0.78 | 20 | | | | | | Yes | 18.87 | 5322 | 3.58 | 8.0E-16 | 1 in 1000000 | |
| A23 | | 123.6 | | 2.4 | 2.4 | 2.4 | 25 | 17.4 | 16.4 | 90.0 | 4.8 | 5.3 | 40.8 | 285.4 | 481.7 | 7.3 | 6.8 | 6.83 | 0.970 | 0.970 | 16.885 | 5.22 | 1489 | 0.77 | 20 | | | | | | Yes | 19.04 | 5433 | 3.65 | 3.1E-16 | 1 in 1000000 | |
| A24 | | 123.0 | | 2.4 | 2.4 | 2.4 | 25 | 17.4 | 16.4 | 90.0 | 5.3 | 5.2 | 41.8 | 285.4 | 490.3 | 7.3 | 6.8 | 6.83 | 0.970 | 0.970 | 16.885 | 5.28 | 1508 | 0.78 | 20 | | | | | | Yes | 19.04 | 5433 | 3.60 | 6.0E-16 | 1 in 1000000 | |
| A25 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.4 | 16.4 | 90.0 | 5.3 | 5.3 | 42.1 | 285.4 | 492.6 | 7.3 | 6.8 | 6.83 | 0.970 | 0.970 | 16.885 | 5.26 | 1501 | 0.78 | 20 | | | | | | Yes | 19.04 | 5433 | 3.62 | 4.8E-16 | 1 in 1000000 | |
| A26 | Tailgate Loading | 129.9 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 20.5 | 23.8 | 90.0 | 5.4 | 6.2 | 37.2 | 487.9 | 777.0 | 8.5 | 9.9 | 8.54 | 1.074 | 1.074 | 22.027 | 5.17 | 2523 | 0.83 | 20 | A | | | | | | | | | | | |

Table A.2: Pillar Stability Analysis

Run 2: Remove Crushed Pillars from Run 1

Key to Colour Coding of Factors of Safety / Width: Height Ratios

| | |
|------|--|
| 4.50 | Greater than 3.0 |
| 2.40 | Between 2.2 and 3.0 |
| 2.10 | Between 1.8 and 2.2 |
| 1.70 | Between 1.5 and 1.8 |
| 1.20 | Less than 1.5 |
| | Indicating Pillar Located within Project Angle of Draw |
| | Indicating Pillar Located beneath site |

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 2
Calculations by JAW

| Analysis Id. | Comment | Depth D (m) | Panel Width/Span (Longwall only) (m) | Seam Thickness (m) | Working Section H (m) | Pillar Height Section H (m) | Unit Weight γ (kN/m³) | Pillar Details | | | Jadway Det. | | Extract. Ratio | Pillar Area m³ | Total Area m³ | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|--------------------------------|-----------------------|--|--------------------------|--------------------------------|--------------------------------------|--------------------------------|--------------------|---------------------|--------------------------|-------------|-----------|-------------------|----------------------|---------------------|--------------------------------|---------------------------------|---------------------------|----------------|-------|--------------------------|--|-------------------------------------|---|------------------------|------------------------------|--------------------------------------|--------------------|------------------------------------|---|---------------------------------------|--------|-------------------|--------------------------|----------|---------------------------|--|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (") | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wφ Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A74 | | 122.3 | | 2.4 | 2.4 | 2.4 | 25 | 16.4 | 17.4 | 90.0 | 5.5 | 5.2 | 42.3 | 285.4 | 494.9 | 6.8 | 7.3 | 6.83 | 1.030 | 1.030 | 16.885 | 5.30 | 1513 | 0.77 | 20 | | | | | | Yes | 18.49 | 5276 | 3.49 | 3.2E-15 | 1 in 1000000 | |
| A75 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 16.6 | 16.9 | 90.0 | 5.2 | 5.4 | 42.3 | 280.5 | 486.1 | 6.9 | 7.0 | 6.92 | 1.009 | 1.009 | 16.749 | 5.28 | 1480 | 0.77 | 20 | | | | | | Yes | 18.51 | 5194 | 3.51 | 2.4E-15 | 1 in 1000000 | |
| A76 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 16.6 | 17.1 | 90.0 | 4.8 | 5.7 | 41.8 | 283.9 | 487.9 | 6.9 | 7.1 | 6.92 | 1.015 | 1.015 | 16.846 | 5.23 | 1486 | 0.76 | 20 | | | | | | Yes | 18.57 | 5271 | 3.55 | 1.3E-15 | 1 in 1000000 | |
| A77 | | 121.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.6 | 17.0 | 90.0 | 5.0 | 5.0 | 40.6 | 282.2 | 475.2 | 6.9 | 7.1 | 6.92 | 1.012 | 1.012 | 16.798 | 5.10 | 1440 | 0.76 | 20 | | | | | | Yes | 18.54 | 5233 | 3.63 | 3.9E-16 | 1 in 1000000 | |
| A78 | Maingate Loading | 121.8 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 16.5 | 29.9 | 90.0 | 5.3 | 4.4 | 34.0 | 493.4 | 747.7 | 6.9 | 12.5 | 6.88 | 1.289 | 1.289 | 21.265 | 4.62 | 2277 | 0.77 | 20 | A | M | | 985 | | 6.61 | Yes | 20.85 | 10288 | 3.15 | 3.9E-13 | 1 in 1000000 |
| A79 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 16.2 | 17.6 | 90.0 | 6.6 | 5.3 | 45.4 | 285.1 | 522.1 | 6.8 | 7.3 | 6.75 | 1.041 | 1.041 | 16.871 | 5.58 | 1591 | 0.79 | 20 | | | | | | Yes | 18.38 | 5241 | 3.29 | 5.2E-14 | 1 in 1000000 | |
| A80 | Tailgate Loading / Double Goaf | 125.6 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 18.5 | 31.5 | 90.0 | 23.2 | 5.0 | 61.7 | 582.8 | 1522.1 | 7.7 | 13.1 | 7.71 | 1.260 | 1.260 | 23.310 | 8.20 | 4779 | 0.98 | 20 | A | G | | 3888 | | 14.87 | Yes | 23.27 | 13558 | 1.56 | 2.3E-03 | 1 in 409 |
| A81 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 15.4 | 17.5 | 90.0 | 5.2 | 5.1 | 42.1 | 269.5 | 465.6 | 6.4 | 7.3 | 6.42 | 1.064 | 1.064 | 16.383 | 5.26 | 1418 | 0.74 | 20 | | | | | | Yes | 17.75 | 4785 | 3.38 | 1.6E-14 | 1 in 1000000 | |
| B1 | | 121.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 15.9 | 90.0 | 5.4 | 6.7 | 46.5 | 273.5 | 510.8 | 7.2 | 6.6 | 6.63 | 0.961 | 0.961 | 16.524 | 5.66 | 1548 | 0.78 | 20 | | | | | | Yes | 18.71 | 5118 | 3.31 | 4.3E-14 | 1 in 1000000 | |
| B2 | | 120.6 | | 2.4 | 2.4 | 2.4 | 25 | 16.8 | 15.9 | 90.0 | 5.4 | 6.7 | 46.8 | 267.1 | 501.7 | 7.0 | 6.6 | 6.63 | 0.972 | 0.972 | 16.338 | 5.66 | 1513 | 0.78 | 20 | | | | | | Yes | 18.39 | 4911 | 3.25 | 1.0E-13 | 1 in 1000000 | |
| B3 | | 120.1 | | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 15.4 | 90.0 | 5.4 | 6.7 | 47.9 | 246.4 | 472.9 | 6.7 | 6.4 | 6.42 | 0.981 | 0.981 | 15.694 | 5.76 | 1420 | 0.76 | 20 | | | | | | Yes | 17.62 | 4342 | 3.06 | 1.5E-12 | 1 in 1000000 | |
| B4 | | 120.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 15.7 | 90.0 | 5.4 | 5.0 | 42.2 | 271.6 | 469.9 | 7.2 | 6.5 | 6.54 | 0.952 | 0.952 | 16.461 | 5.20 | 1412 | 0.79 | 20 | | | | | | Yes | 18.73 | 5088 | 3.60 | 6.0E-16 | 1 in 1000000 | |
| B5 | | 119.6 | | 2.4 | 2.4 | 2.4 | 25 | 16.9 | 15.8 | 90.0 | 5.4 | 5.0 | 42.4 | 267.0 | 463.8 | 7.0 | 6.6 | 6.58 | 0.966 | 0.966 | 16.331 | 5.19 | 1387 | 0.78 | 20 | | | | | | Yes | 18.44 | 4923 | 3.55 | 1.3E-15 | 1 in 1000000 | |
| B6 | | 119.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 16.1 | 90.0 | 5.4 | 5.0 | 41.8 | 278.5 | 479.0 | 7.2 | 6.7 | 6.71 | 0.964 | 0.964 | 16.678 | 5.12 | 1427 | 0.79 | 20 | | | | | | Yes | 18.86 | 5253 | 3.68 | 2.0E-16 | 1 in 1000000 | |
| B7 | | 118.6 | | 2.4 | 2.4 | 2.4 | 25 | 18.3 | 24.6 | 90.0 | 5.4 | 5.2 | 36.3 | 450.2 | 706.3 | 7.6 | 10.3 | 7.63 | 1.147 | 1.147 | 20.987 | 4.65 | 2094 | 0.81 | 20 | | | | | | Yes | 21.90 | 9860 | 4.71 | 7.5E-23 | 1 in 1000000 | |
| B8 | | 119.0 | | 2.4 | 2.4 | 2.4 | 25 | 18.1 | 24.9 | 90.0 | 5.4 | 5.2 | 36.3 | 450.7 | 707.4 | 7.5 | 10.4 | 7.54 | 1.158 | 1.158 | 20.962 | 4.67 | 2104 | 0.80 | 20 | | | | | | Yes | 21.74 | 9799 | 4.66 | 1.6E-22 | 1 in 1000000 | |
| B9 | | 120.0 | | 2.4 | 2.4 | 2.4 | 25 | 18.0 | 24.9 | 90.0 | 5.4 | 5.2 | 36.4 | 448.2 | 704.3 | 7.5 | 10.4 | 7.50 | 1.161 | 1.161 | 20.895 | 4.71 | 2113 | 0.80 | 20 | | | | | | Yes | 21.64 | 9697 | 4.59 | 4.2E-22 | 1 in 1000000 | |
| B10 | | 121.3 | | 2.4 | 2.4 | 2.4 | 25 | 18.8 | 24.7 | 90.0 | 5.4 | 5.2 | 35.8 | 464.4 | 723.6 | 7.8 | 10.3 | 7.83 | 1.136 | 1.136 | 21.350 | 4.73 | 2194 | 0.81 | 20 | | | | | | Yes | 22.48 | 10439 | 4.76 | 3.7E-23 | 1 in 1000000 | |
| B11 | Maingate Loading | 121.8 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 15.2 | 40.0 | 90.0 | 6.1 | 4.8 | 36.3 | 608.0 | 954.2 | 6.3 | 16.7 | 6.33 | 1.449 | 1.449 | 22.029 | 4.78 | 2906 | 0.76 | 20 | A | M | | 1310 | | 6.93 | Yes | 20.56 | 12498 | 2.96 | 5.9E-12 | 1 in 1000000 |
| B12 | | 121.0 | | 2.4 | 2.4 | 2.4 | 25 | 18.6 | 19.0 | 90.0 | 5.4 | 5.2 | 39.2 | 353.4 | 580.8 | 7.8 | 7.9 | 7.75 | 1.011 | 1.011 | 18.798 | 4.97 | 1757 | 0.81 | 20 | | | | | | Yes | 20.92 | 7393 | 4.21 | 1.0E-19 | 1 in 1000000 | |
| B13 | | 119.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.8 | 18.7 | 90.0 | 5.4 | 5.2 | 40.8 | 314.2 | 530.6 | 7.0 | 7.8 | 7.00 | 1.054 | 1.054 | 17.699 | 5.05 | 1588 | 0.78 | 20 | | | | | | Yes | 19.15 | 6017 | 3.79 | 4.1E-17 | 1 in 1000000 | |
| B14 | | 118.4 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 18.7 | 90.0 | 5.4 | 5.2 | 40.5 | 321.6 | 540.1 | 7.2 | 7.8 | 7.17 | 1.042 | 1.042 | 17.919 | 4.97 | 1599 | 0.79 | 20 | | | | | | Yes | 19.50 | 6273 | 3.92 | 6.0E-18 | 1 in 1000000 | |
| B15 | | 117.7 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 19.5 | 90.0 | 5.4 | 5.2 | 39.8 | 337.4 | 560.7 | 7.2 | 8.1 | 7.21 | 1.060 | 1.060 | 18.334 | 4.89 | 1650 | 0.79 | 20 | | | | | | Yes | 19.79 | 6677 | 4.05 | 1.0E-18 | 1 in 1000000 | |
| B16 | | 119.0 | | 2.4 | 2.4 | 2.4 | 25 | 63.4 | 42.3 | 90.0 | 5.4 | 5.2 | 17.9 | 2681.8 | 3268.0 | 26.4 | 17.6 | 17.63 | 0.800 | 0.800 | 50.744 | 3.63 | 9722 | 1.01 | 20 | | | | | | Yes | 173.66 | 465736 | 47.90 | 8.0E-293 | 1 in 1000000 | |
| B17 | | 119.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.1 | 31.1 | 90.0 | 5.5 | 5.7 | 37.0 | 500.7 | 794.9 | 6.7 | 13.0 | 6.71 | 1.318 | 1.318 | 21.217 | 4.75 | 2379 | 0.77 | 20 | | | | | | Yes | 20.61 | 10318 | 4.34 | 1.6E-20 | 1 in 1000000 | |
| B18 | Tailgate Loading | 119.9 | 22.0 | 2.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Table A.2: Pillar Stability Analysis

Run 2: Remove Crushed Pillars from Run 1

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 2
Calculations by JAW

Key to Colour Coding of Factors of Safety / Width: Height Ratios

4.50

Greater than 3.0

2.40

Between 2.2 and 3.0

2.10

Between 1.8 and 2.2

1.70

Between 1.5 and 1.8

1.20

Less than 1.5

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

| Analysis Id: | Comment | Depth | Panel Width/Span (Longwall only) | Seam Thickness | Working Section | Pillar Height Section | Unit Weighth γ (kN/m³) | Pillar Details | | | Adway Deta | | Extract. Ratio | Pillar Area | Total Area | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae | |
|--------------|----------------------------------|-------|-------------------------------------|----------------|-----------------|-----------------------|------------------------------|----------------|---------------|--------------------|------------|--------|----------------|-------------|------------|--------------------------|---------------------------|---------------------|----------------|----------------|--------|---------------------------------|----------------------------|--------------------------------|------------------|------------------------|-----------------------------|--------------|---------------------------|--|------------------------------|-------|--------------------|----------------|--------------------|---------|---|------------------------|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (°) | b1 (m) | b2 (m) | | | | | | | Ratio (%) | Θ ₀ | Θ | | | | | | | | | | | | Effective Width wΘ | Strength (MPa) | "Ultimate" Load MN | FoS | | Probability of Failure |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| B66 | Double Goaf Loading | 119.5 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 24.7 | 16.2 | 90.0 | 5.5 | 5.0 | 37.5 | 400.1 | 640.2 | 10.3 | 6.8 | 6.75 | 0.792 | 0.792 | 19.567 | 4.78 | 1913 | 0.90 | 20 | A | G | | 2113 | | 10.06 | Yes | 27.21 | 10888 | 2.70 | 2.5E-10 | 1 in 1000000 | |
| B67 | Tailgate Loading | 119.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 24.7 | 16.2 | 90.0 | 5.5 | 5.2 | 38.1 | 400.1 | 646.3 | 10.3 | 6.8 | 6.75 | 0.792 | 0.792 | 19.567 | 4.81 | 1923 | 0.90 | 20 | A | T | | 1803 | | 9.31 | Yes | 27.21 | 10888 | 2.92 | 1.1E-11 | 1 in 1000000 | |
| B68 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.8 | 37.9 | 432.0 | 695.4 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.83 | 2086 | 0.76 | 20 | A | G | | 3287 | | 12.44 | Yes | 19.99 | 8636 | 1.61 | 1.4E-03 | 1 in 705 | |
| B69 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.8 | 37.9 | 432.0 | 695.4 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.83 | 2086 | 0.76 | 20 | A | G | | 3287 | | 12.44 | Yes | 19.99 | 8636 | 1.61 | 1.4E-03 | 1 in 705 | |
| B70 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.6 | 37.5 | 432.0 | 691.1 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.80 | 2073 | 0.76 | 20 | A | G | | 3267 | | 12.36 | Yes | 19.99 | 8636 | 1.62 | 1.3E-03 | 1 in 801 | |
| B71 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.7 | 37.7 | 432.0 | 693.2 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.81 | 2080 | 0.76 | 20 | A | G | | 3277 | | 12.40 | Yes | 19.99 | 8636 | 1.61 | 1.3E-03 | 1 in 751 | |
| B72 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.7 | 37.7 | 432.0 | 693.2 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.81 | 2080 | 0.76 | 20 | A | G | | 3277 | | 12.40 | Yes | 19.99 | 8636 | 1.61 | 1.3E-03 | 1 in 751 | |
| B73 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.9 | 38.1 | 432.0 | 697.5 | 6.7 | 11.3 | 6.67 | 1.256 | 1.256 | 20.093 | 4.84 | 2092 | 0.76 | 20 | A | G | | 3297 | | 12.48 | Yes | 19.99 | 8636 | 1.60 | 1.5E-03 | 1 in 662 | |
| B74 | Double Goaf Loading | 118.2 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 25.3 | 15.5 | 90.0 | 5.5 | 5.3 | 38.8 | 392.2 | 640.6 | 10.5 | 6.5 | 6.46 | 0.760 | 0.760 | 19.223 | 4.83 | 1893 | 0.91 | 20 | A | G | | 2043 | | 10.04 | Yes | 27.67 | 10849 | 2.76 | 1.2E-10 | 1 in 1000000 | |
| B75 | Double Goaf Loading | 118.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 25.1 | 15.5 | 90.0 | 5.5 | 5.8 | 40.3 | 389.1 | 651.8 | 10.5 | 6.5 | 6.46 | 0.764 | 0.764 | 19.165 | 4.94 | 1923 | 0.91 | 20 | A | G | | 2087 | | 10.31 | Yes | 27.39 | 10655 | 2.66 | 4.9E-10 | 1 in 1000000 | |
| B76 | Maingate Loading | 117.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 26.4 | 15.6 | 90.0 | 5.5 | 5.3 | 38.2 | 411.8 | 666.7 | 11.0 | 6.5 | 6.50 | 0.743 | 0.743 | 19.611 | 4.74 | 1950 | 0.92 | 20 | A | M | | 1090 | | 7.38 | Yes | 29.30 | 12067 | 3.97 | 3.1E-18 | 1 in 1000000 | |
| B77 | Rotated panel / Maingate Loading | 118.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.4 | 27.7 | 90.0 | 5.7 | 5.3 | 38.7 | 426.6 | 696.3 | 6.4 | 11.5 | 6.42 | 1.285 | 1.285 | 19.795 | 4.82 | 2054 | 0.76 | 20 | A | M | | 1440 | | 8.19 | Yes | 19.55 | 8340 | 2.39 | 2.4E-08 | 1 in 1000000 | |
| B78 | Rotated panel / Maingate Loading | 119.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.3 | 27.3 | 90.0 | 5.6 | 5.3 | 38.7 | 417.7 | 681.3 | 6.4 | 11.4 | 6.38 | 1.282 | 1.282 | 19.610 | 4.85 | 2027 | 0.75 | 20 | A | M | | 1423 | | 8.26 | Yes | 19.41 | 8109 | 2.35 | 4.1E-08 | 1 in 1000000 | |
| B79 | Rotated panel / Maingate Loading | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 27.3 | 90.0 | 5.4 | 5.3 | 37.9 | 423.2 | 681.3 | 6.5 | 11.4 | 6.46 | 1.276 | 1.276 | 19.773 | 4.83 | 2044 | 0.75 | 20 | A | M | | 1428 | | 8.20 | Yes | 19.59 | 8288 | 2.39 | 2.4E-08 | 1 in 1000000 | |
| B80 | Rotated panel / Maingate Loading | 121.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 27.3 | 90.0 | 5.7 | 5.3 | 38.8 | 423.2 | 691.1 | 6.5 | 11.4 | 6.46 | 1.276 | 1.276 | 19.773 | 4.94 | 2091 | 0.76 | 20 | A | M | | 1463 | | 8.40 | Yes | 19.59 | 8288 | 2.33 | 5.3E-08 | 1 in 1000000 | |
| B81 | Rotated panel / Maingate Loading | 122.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 27.3 | 90.0 | 5.6 | 5.3 | 38.5 | 423.2 | 687.9 | 6.5 | 11.4 | 6.46 | 1.276 | 1.276 | 19.773 | 4.96 | 2098 | 0.75 | 20 | A | M | | 1467 | | 8.42 | Yes | 19.59 | 8288 | 2.32 | 5.9E-08 | 1 in 1000000 | |
| B82 | Rotated panel / Maingate Loading | 123.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 27.3 | 90.0 | 5.6 | 5.3 | 38.5 | 423.2 | 687.9 | 6.5 | 11.4 | 6.46 | 1.276 | 1.276 | 19.773 | 5.00 | 2115 | 0.75 | 20 | A | M | | 1479 | | 8.49 | Yes | 19.59 | 8288 | 2.31 | 7.7E-08 | 1 in 1000000 | |
| B83 | | 113.0 | | 2.4 | 2.4 | 2.4 | 25 | 13.6 | 9.9 | 90.0 | 5.4 | 6.2 | 56.0 | 134.6 | 305.9 | 5.7 | 4.1 | 4.13 | 0.843 | 0.859 | 11.679 | 6.42 | 864 | 0.72 | 21 | A | M | | 89 | | 7.08 | Yes | 14.47 | 1948 | 2.04 | 3.4E-06 | 1 in 450037 | |
| B84 | | 113.5 | | 2.4 | 2.4 | 2.4 | 25 | 14.0 | 9.6 | 90.0 | 5.6 | 6.2 | 56.6 | 134.4 | 309.7 | 5.8 | 4.0 | 4.00 | 0.814 | 0.823 | 11.521 | 6.54 | 879 | 0.74 | 22 | A | M | | 92 | | 7.23 | Yes | 14.45 | 1942 | 2.00 | 6.4E-06 | 1 in 215774 | |
| B85 | | 113.8 | | 2.4 | 2.4 | 2.4 | 25 | 13.8 | 10.0 | 90.0 | 5.4 | 5.3 | 53.0 | 138.0 | 293.8 | 5.8 | 4.2 | 4.17 | 0.840 | 0.853 | 11.766 | 6.06 | 836 | 0.73 | 23 | A | M | | 85 | | 6.67 | Yes | 14.56 | 2009 | 2.18 | 4.6E-07 | 1 in 1000000 | |

Table A.3: Pillar Stability Analysis

Run 3: Decrease Run 2 Pillars by 1 m

Key to Colour Coding of Factors of Safety / Width: Height Ratios

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 3
Calculations by JAW

4.50

Greater than 3.0

2.40

Between 2.2 and 3.0

2.10

Between 1.8 and 2.2

1.70

Between 1.5 and 1.8

1.20

Less than 1.5

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

| Analysis Id. | Comment | Depth D (m) | Panel Width/Span (Longwall only) (m) | Seam Thickness (m) | Working Section H (m) | Pillar Height Section H (m) | Unit Weighth γ (kN/m³) | Pillar Details | | | Jadway Det | | Extract. Ratio | Pillar Area m³ | Total Area m³ | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|------------------|-----------------------|--|-----------------------|-----------------------------|-----------------------------------|------------------------------|--------------------|---------------------|-----------------------|------------|-----------|----------------|-------------------|------------------|--------------------------|---------------------------|------------------------|----------------|-------|-----------------------|---------------------------------------|----------------------------------|--------------------------------------|------------------|------------------------------|-----------------------------------|-----------------|---------------------------------|--|------------------------------------|-------|-------------------|--------------------------|---------|------------------------|--|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (") | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wΘ Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A1 | | 127.7 | | 2.4 | 2.4 | 2.4 | 25 | 17.6 | 30.0 | 90.0 | 5.9 | 6.2 | 37.9 | 528.0 | 850.7 | 7.3 | 12.5 | 7.33 | 1.261 | 1.261 | 22.185 | 5.14 | 2716 | 0.79 | 20 | | | | | | Yes | 22.02 | 11626 | 4.28 | 3.5E-20 | 1 in 1000000 | |
| A2 | | 126.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.4 | 30.5 | 90.0 | 6.2 | 6.1 | 39.5 | 500.2 | 827.2 | 6.8 | 12.7 | 6.83 | 1.301 | 1.301 | 21.330 | 5.24 | 2619 | 0.77 | 20 | | | | | | Yes | 20.83 | 10418 | 3.98 | 2.7E-18 | 1 in 1000000 | |
| A3 | | 126.7 | | 2.4 | 2.4 | 2.4 | 25 | 18.1 | 30.4 | 90.0 | 6.3 | 6.4 | 38.7 | 550.2 | 897.9 | 7.5 | 12.7 | 7.54 | 1.254 | 1.254 | 22.690 | 5.17 | 2843 | 0.81 | 20 | | | | | | Yes | 22.64 | 12457 | 4.38 | 8.3E-21 | 1 in 1000000 | |
| A4 | Tailgate Loading | 124.6 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 15.8 | 30.4 | 90.0 | 6.4 | 6.1 | 40.7 | 480.3 | 810.3 | 6.6 | 12.7 | 6.58 | 1.316 | 1.316 | 20.793 | 5.25 | 2523 | 0.77 | 20 | A | T | | 1868 | | 9.14 | Yes | 20.24 | 9722 | 2.21 | 2.9E-07 | 1 in 1000000 |
| A5 | | 124.1 | | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 30.1 | 90.0 | 6.4 | 6.2 | 41.3 | 466.6 | 795.0 | 6.5 | 12.5 | 6.46 | 1.320 | 1.320 | 20.463 | 5.29 | 2466 | 0.77 | 20 | | | | | | Yes | 19.93 | 9299 | 3.77 | 5.5E-17 | 1 in 1000000 | |
| A6 | | 123.6 | | 2.4 | 2.4 | 2.4 | 25 | 16.7 | 25.9 | 90.0 | 5.8 | 6.3 | 40.3 | 432.5 | 724.5 | 7.0 | 10.8 | 6.96 | 1.216 | 1.216 | 20.307 | 5.17 | 2238 | 0.78 | 20 | | | | | | Yes | 20.48 | 8860 | 3.96 | 3.6E-18 | 1 in 1000000 | |
| A7 | | 123.1 | | 2.4 | 2.4 | 2.4 | 25 | 16.2 | 25.5 | 90.0 | 6.2 | 6.4 | 42.2 | 413.1 | 714.6 | 6.8 | 10.6 | 6.75 | 1.223 | 1.223 | 19.813 | 5.32 | 2199 | 0.78 | 20 | | | | | | Yes | 19.95 | 8242 | 3.75 | 7.5E-17 | 1 in 1000000 | |
| A8 | | 122.7 | | 2.4 | 2.4 | 2.4 | 25 | 15.7 | 25.5 | 90.0 | 6.4 | 6.8 | 43.9 | 400.4 | 713.8 | 6.5 | 10.6 | 6.54 | 1.238 | 1.238 | 19.434 | 5.47 | 2189 | 0.77 | 20 | | | | | | Yes | 19.51 | 7810 | 3.57 | 1.0E-15 | 1 in 1000000 | |
| A9 | | 121.4 | | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 26.6 | 90.0 | 6.0 | 6.3 | 41.2 | 425.6 | 723.8 | 6.7 | 11.1 | 6.67 | 1.249 | 1.249 | 19.981 | 5.16 | 2196 | 0.77 | 20 | | | | | | Yes | 19.93 | 8484 | 3.86 | 1.4E-17 | 1 in 1000000 | |
| A10 | | 123.9 | | 2.4 | 2.4 | 2.4 | 25 | 16.3 | 16.4 | 90.0 | 6.3 | 5.9 | 47.0 | 267.3 | 504.0 | 6.8 | 6.8 | 6.79 | 1.003 | 1.003 | 16.350 | 5.84 | 1561 | 0.78 | 20 | | | | | | Yes | 18.14 | 4849 | 3.11 | 7.8E-13 | 1 in 1000000 | |
| A11 | | 124.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 16.3 | 90.0 | 6.3 | 6.0 | 47.6 | 260.8 | 497.3 | 6.7 | 6.8 | 6.67 | 1.009 | 1.009 | 16.149 | 5.92 | 1544 | 0.77 | 20 | | | | | | Yes | 17.88 | 4664 | 3.02 | 2.7E-12 | 1 in 1000000 | |
| A12 | | 123.2 | | 2.4 | 2.4 | 2.4 | 25 | 15.7 | 16.1 | 90.0 | 6.1 | 6.2 | 48.0 | 252.8 | 486.1 | 6.5 | 6.7 | 6.54 | 1.013 | 1.013 | 15.897 | 5.93 | 1498 | 0.76 | 20 | | | | | | Yes | 17.61 | 4451 | 2.97 | 5.4E-12 | 1 in 1000000 | |
| A13 | | 123.0 | | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 16.0 | 90.0 | 6.3 | 6.1 | 48.1 | 256.0 | 492.8 | 6.7 | 6.7 | 6.67 | 1.000 | 1.000 | 16.000 | 5.92 | 1515 | 0.78 | 20 | | | | | | Yes | 17.80 | 4556 | 3.01 | 3.2E-12 | 1 in 1000000 | |
| A14 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 16.1 | 90.0 | 6.5 | 6.7 | 49.8 | 257.6 | 513.0 | 6.7 | 6.7 | 6.67 | 1.003 | 1.003 | 16.050 | 6.07 | 1563 | 0.78 | 20 | | | | | | Yes | 17.83 | 4592 | 2.94 | 8.8E-12 | 1 in 1000000 | |
| A15 | | 128.8 | | 2.4 | 2.4 | 2.4 | 25 | 23.5 | 37.0 | 90.0 | 5.2 | 6.1 | 29.7 | 869.5 | 1237.0 | 9.8 | 15.4 | 9.79 | 1.223 | 1.223 | 28.744 | 4.58 | 3984 | 0.87 | 20 | | | | | | Yes | 31.47 | 27361 | 6.87 | 2.4E-36 | 1 in 1000000 | |
| A16 | | 128.9 | | 2.4 | 2.4 | 2.4 | 25 | 17.6 | 30.5 | 90.0 | 6.4 | 6.3 | 39.2 | 536.8 | 883.2 | 7.3 | 12.7 | 7.33 | 1.268 | 1.268 | 22.320 | 5.30 | 2846 | 0.80 | 20 | | | | | | Yes | 22.09 | 11857 | 4.17 | 1.8E-19 | 1 in 1000000 | |
| A17 | | 128.8 | | 2.4 | 2.4 | 2.4 | 25 | 19.0 | 30.7 | 90.0 | 6.3 | 6.9 | 38.7 | 583.3 | 951.3 | 7.9 | 12.8 | 7.92 | 1.235 | 1.235 | 23.473 | 5.25 | 3064 | 0.82 | 20 | | | | | | Yes | 23.76 | 13860 | 4.52 | 1.1E-21 | 1 in 1000000 | |
| A18 | | 127.3 | | 2.4 | 2.4 | 2.4 | 25 | 18.1 | 30.7 | 90.0 | 6.2 | 6.4 | 38.4 | 555.7 | 901.5 | 7.5 | 12.8 | 7.54 | 1.258 | 1.258 | 22.773 | 5.16 | 2869 | 0.80 | 20 | | | | | | Yes | 22.68 | 12603 | 4.39 | 7.0E-21 | 1 in 1000000 | |
| A19 | | 125.9 | | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 30.5 | 90.0 | 6.2 | 6.5 | 40.6 | 488.0 | 821.4 | 6.7 | 12.7 | 6.67 | 1.312 | 1.312 | 20.989 | 5.30 | 2585 | 0.77 | 20 | | | | | | Yes | 20.44 | 9975 | 3.86 | 1.5E-17 | 1 in 1000000 | |
| A20 | | 125.1 | | 2.4 | 2.4 | 2.4 | 25 | 15.3 | 30.5 | 90.0 | 6.3 | 6.4 | 41.5 | 466.7 | 797.0 | 6.4 | 12.7 | 6.38 | 1.332 | 1.332 | 20.378 | 5.34 | 2493 | 0.76 | 20 | | | | | | Yes | 19.80 | 9239 | 3.71 | 1.4E-16 | 1 in 1000000 | |
| A21 | | 124.4 | | 2.4 | 2.4 | 2.4 | 25 | 16.2 | 15.0 | 90.0 | 6.3 | 6.0 | 48.6 | 243.0 | 472.5 | 6.8 | 6.3 | 6.25 | 0.962 | 0.962 | 15.577 | 6.05 | 1469 | 0.78 | 20 | | | | | | Yes | 17.65 | 4288 | 2.92 | 1.2E-11 | 1 in 1000000 | |
| A22 | | 123.9 | | 2.4 | 2.4 | 2.4 | 25 | 16.2 | 15.4 | 90.0 | 6.2 | 6.0 | 48.0 | 249.5 | 479.4 | 6.8 | 6.4 | 6.42 | 0.975 | 0.975 | 15.790 | 5.95 | 1485 | 0.78 | 20 | | | | | | Yes | 17.77 | 4433 | 2.99 | 4.4E-12 | 1 in 1000000 | |
| A23 | | 123.6 | | 2.4 | 2.4 | 2.4 | 25 | 16.4 | 15.4 | 90.0 | 5.8 | 6.3 | 47.6 | 252.6 | 481.7 | 6.8 | 6.4 | 6.42 | 0.969 | 0.969 | 15.884 | 5.89 | 1489 | 0.77 | 20 | | | | | | Yes | 17.92 | 4526 | 3.04 | 2.0E-12 | 1 in 1000000 | |
| A24 | | 123.0 | | 2.4 | 2.4 | 2.4 | 25 | 16.4 | 15.4 | 90.0 | 6.3 | 6.2 | 48.5 | 252.6 | 490.3 | 6.8 | 6.4 | 6.42 | 0.969 | 0.969 | 15.884 | 5.97 | 1508 | 0.78 | 20 | | | | | | Yes | 17.92 | 4526 | 3.00 | 3.5E-12 | 1 in 1000000 | |
| A25 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 16.4 | 15.4 | 90.0 | 6.3 | 6.3 | 48.7 | 252.6 | 492.6 | 6.8 | 6.4 | 6.42 | 0.969 | 0.969 | 15.884 | 5.94 | 1501 | 0.78 | 20 | | | | | | Yes | 17.92 | 4526 | 3.02 | 2.9E-12 | 1 in 1000000 | |
| A26 | Tailgate Loading | 129.9 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 19.5 | 22.8 | 90.0 | 6.4 | 7.2 | 42.8 | 444.6 | 777.0 | 8.1 | 9.5 | 8.13 | 1.078 | 1.078 | 21.021 | 5.68</ | | | | | | | | | | | | | | | |

Table A.3: Pillar Stability Analysis

Run 3: Decrease Run 2 Pillars by 1 m

Key to Colour Coding of Factors of Safety / Width: Height Ratios

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 3
Calculations by JAW

| | |
|------|---------------------|
| 4.50 | Greater than 3.0 |
| 2.40 | Between 2.2 and 3.0 |
| 2.10 | Between 1.8 and 2.2 |
| 1.70 | Between 1.5 and 1.8 |
| 1.20 | Less than 1.5 |

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

| Analysis Id. | Comment | Depth D (m) | Panel Width/Span (Longwall only) (m) | Seam Thickness (m) | Working Section H (m) | Pillar Height Section H (m) | Unit Weight γ (kN/m³) | Pillar Details | | | Adjoint Det. | | Extract. Ratio | Pillar Area m³ | Total Area m³ | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment Transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|--------------------------------|-------------------|--|-----------------------|-----------------------------|-----------------------------------|-----------------------------|--------------------|---------------------|--------------------------|--------------|-----------|-------------------|-------------------|------------------|--------------------------------|---------------------------------|---------------------------|----------------|-------|--------------------------|---------------------------------------|----------------------------------|--------------------------------------|---------------------|------------------------------|-----------------------------------|-----------------|---------------------------------|--|------------------------------------|--------|-------------------|--------------------------|----------|---------------------------|--|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (') | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wΘ Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A74 | | 122.3 | | 2.4 | 2.4 | 2.4 | 25 | 15.4 | 16.4 | 90.0 | 6.5 | 6.2 | 49.0 | 252.6 | 494.9 | 6.4 | 6.8 | 6.42 | 1.031 | 1.031 | 15.884 | 5.99 | 1513 | 0.77 | 20 | | | | | | Yes | 17.48 | 4414 | 2.92 | 1.2E-11 | 1 in 1000000 | |
| A75 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 15.6 | 15.9 | 90.0 | 6.2 | 6.4 | 49.0 | 248.0 | 486.1 | 6.5 | 6.6 | 6.50 | 1.010 | 1.010 | 15.749 | 5.97 | 1480 | 0.77 | 20 | | | | | | Yes | 17.48 | 4336 | 2.93 | 9.9E-12 | 1 in 1000000 | |
| A76 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 15.6 | 16.1 | 90.0 | 5.8 | 6.7 | 48.5 | 251.2 | 487.9 | 6.5 | 6.7 | 6.50 | 1.016 | 1.016 | 15.846 | 5.92 | 1486 | 0.76 | 20 | | | | | | Yes | 17.54 | 4404 | 2.96 | 5.9E-12 | 1 in 1000000 | |
| A77 | | 121.2 | | 2.4 | 2.4 | 2.4 | 25 | 15.6 | 16.0 | 90.0 | 6.0 | 6.0 | 47.5 | 249.6 | 475.2 | 6.5 | 6.7 | 6.50 | 1.013 | 1.013 | 15.797 | 5.77 | 1440 | 0.76 | 20 | | | | | | Yes | 17.51 | 4370 | 3.04 | 2.1E-12 | 1 in 1000000 | |
| A78 | Maingate Loading | 121.8 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 15.5 | 28.9 | 90.0 | 6.3 | 5.4 | 40.1 | 448.0 | 747.7 | 6.5 | 12.0 | 6.46 | 1.302 | 1.302 | 20.178 | 5.08 | 2277 | 0.77 | 20 | A | M | | 1025 | | 7.37 | Yes | 19.79 | 8865 | 2.68 | 3.3E-10 | 1 in 1000000 |
| A79 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 15.2 | 16.6 | 90.0 | 7.6 | 6.3 | 51.7 | 252.3 | 522.1 | 6.3 | 6.9 | 6.33 | 1.044 | 1.044 | 15.869 | 6.31 | 1591 | 0.79 | 20 | | | | | | Yes | 17.39 | 4388 | 2.76 | 1.2E-10 | 1 in 1000000 | |
| A80 | Tailgate Loading / Double Goaf | 125.6 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 17.5 | 30.5 | 90.0 | 24.2 | 6.0 | 64.9 | 533.8 | 1522.1 | 7.3 | 12.7 | 7.29 | 1.271 | 1.271 | 22.240 | 8.95 | 4779 | 0.98 | 20 | A | G | | 3888 | | 16.24 | Yes | 21.98 | 11730 | 1.35 | 2.5E-02 | 1 in 36 |
| A81 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 14.4 | 16.5 | 90.0 | 6.2 | 6.1 | 49.0 | 237.6 | 465.6 | 6.0 | 6.9 | 6.00 | 1.068 | 1.068 | 15.379 | 5.97 | 1418 | 0.74 | 20 | | | | | | Yes | 16.85 | 4003 | 2.82 | 4.5E-11 | 1 in 1000000 | |
| B1 | | 121.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.2 | 14.9 | 90.0 | 6.4 | 7.7 | 52.7 | 241.4 | 510.8 | 6.8 | 6.2 | 6.21 | 0.958 | 0.958 | 15.523 | 6.41 | 1548 | 0.78 | 20 | | | | | | Yes | 17.62 | 4252 | 2.75 | 1.3E-10 | 1 in 1000000 | |
| B2 | | 120.6 | | 2.4 | 2.4 | 2.4 | 25 | 15.8 | 14.9 | 90.0 | 6.4 | 7.7 | 53.1 | 235.4 | 501.7 | 6.6 | 6.2 | 6.21 | 0.971 | 0.971 | 15.337 | 6.43 | 1513 | 0.78 | 20 | | | | | | Yes | 17.33 | 4080 | 2.70 | 2.8E-10 | 1 in 1000000 | |
| B3 | | 120.1 | | 2.4 | 2.4 | 2.4 | 25 | 15.0 | 14.4 | 90.0 | 6.4 | 7.7 | 54.3 | 216.0 | 472.9 | 6.3 | 6.0 | 6.00 | 0.980 | 0.980 | 14.694 | 6.57 | 1420 | 0.76 | 20 | | | | | | Yes | 16.65 | 3596 | 2.53 | 3.0E-09 | 1 in 1000000 | |
| B4 | | 120.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.3 | 14.7 | 90.0 | 6.4 | 6.0 | 49.0 | 239.6 | 469.9 | 6.8 | 6.1 | 6.13 | 0.948 | 0.948 | 15.459 | 5.89 | 1412 | 0.79 | 20 | | | | | | Yes | 17.63 | 4224 | 2.99 | 4.0E-12 | 1 in 1000000 | |
| B5 | | 119.6 | | 2.4 | 2.4 | 2.4 | 25 | 15.9 | 14.8 | 90.0 | 6.4 | 6.0 | 49.3 | 235.3 | 463.8 | 6.6 | 6.2 | 6.17 | 0.964 | 0.964 | 15.330 | 5.89 | 1387 | 0.78 | 20 | | | | | | Yes | 17.37 | 4087 | 2.95 | 7.6E-12 | 1 in 1000000 | |
| B6 | | 119.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.3 | 15.1 | 90.0 | 6.4 | 6.0 | 48.6 | 246.1 | 479.0 | 6.8 | 6.3 | 6.29 | 0.962 | 0.962 | 15.677 | 5.80 | 1427 | 0.79 | 20 | | | | | | Yes | 17.75 | 4370 | 3.06 | 1.5E-12 | 1 in 1000000 | |
| B7 | | 118.6 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 23.6 | 90.0 | 6.4 | 6.2 | 42.2 | 408.3 | 706.3 | 7.2 | 9.8 | 7.21 | 1.154 | 1.154 | 19.965 | 5.13 | 2094 | 0.81 | 20 | | | | | | Yes | 20.67 | 8440 | 4.03 | 1.3E-18 | 1 in 1000000 | |
| B8 | | 119.0 | | 2.4 | 2.4 | 2.4 | 25 | 17.1 | 23.9 | 90.0 | 6.4 | 6.2 | 42.2 | 408.7 | 707.4 | 7.1 | 10.0 | 7.13 | 1.166 | 1.166 | 19.936 | 5.15 | 2104 | 0.80 | 20 | | | | | | Yes | 20.53 | 8391 | 3.99 | 2.4E-18 | 1 in 1000000 | |
| B9 | | 120.0 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 23.9 | 90.0 | 6.4 | 6.2 | 42.3 | 406.3 | 704.3 | 7.1 | 10.0 | 7.08 | 1.169 | 1.169 | 19.868 | 5.20 | 2113 | 0.80 | 20 | | | | | | Yes | 20.43 | 8303 | 3.93 | 5.5E-18 | 1 in 1000000 | |
| B10 | | 121.3 | | 2.4 | 2.4 | 2.4 | 25 | 17.8 | 23.7 | 90.0 | 6.4 | 6.2 | 41.7 | 421.9 | 723.6 | 7.4 | 9.9 | 7.42 | 1.142 | 1.142 | 20.331 | 5.20 | 2194 | 0.81 | 20 | | | | | | Yes | 21.20 | 8942 | 4.08 | 6.8E-19 | 1 in 1000000 | |
| B11 | Maingate Loading | 121.8 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 14.2 | 39.0 | 90.0 | 7.1 | 5.8 | 42.0 | 553.8 | 954.2 | 5.9 | 16.3 | 5.92 | 1.466 | 1.451 | 20.599 | 5.25 | 2906 | 0.76 | 20 | A | M | | 1362 | | 7.71 | Yes | 19.49 | 10793 | 2.53 | 3.1E-09 | 1 in 1000000 |
| B12 | | 121.0 | | 2.4 | 2.4 | 2.4 | 25 | 17.6 | 18.0 | 90.0 | 6.4 | 6.2 | 45.5 | 316.8 | 580.8 | 7.3 | 7.5 | 7.33 | 1.011 | 1.011 | 17.798 | 5.55 | 1757 | 0.81 | 20 | | | | | | Yes | 19.68 | 6234 | 3.55 | 1.3E-15 | 1 in 1000000 | |
| B13 | | 119.7 | | 2.4 | 2.4 | 2.4 | 25 | 15.8 | 17.7 | 90.0 | 6.4 | 6.2 | 47.3 | 279.7 | 530.6 | 6.6 | 7.4 | 6.58 | 1.057 | 1.057 | 16.696 | 5.68 | 1588 | 0.78 | 20 | | | | | | Yes | 18.10 | 5061 | 3.19 | 2.4E-13 | 1 in 1000000 | |
| B14 | | 118.4 | | 2.4 | 2.4 | 2.4 | 25 | 16.2 | 17.7 | 90.0 | 6.4 | 6.2 | 46.9 | 286.7 | 540.1 | 6.8 | 7.4 | 6.75 | 1.044 | 1.044 | 16.917 | 5.58 | 1599 | 0.79 | 20 | | | | | | Yes | 18.41 | 5278 | 3.30 | 4.7E-14 | 1 in 1000000 | |
| B15 | | 117.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.3 | 18.5 | 90.0 | 6.4 | 6.2 | 46.2 | 301.6 | 560.7 | 6.8 | 7.7 | 6.79 | 1.063 | 1.063 | 17.330 | 5.47 | 1650 | 0.79 | 20 | | | | | | Yes | 18.68 | 5634 | 3.42 | 9.1E-15 | 1 in 1000000 | |
| B16 | | 119.0 | | 2.4 | 2.4 | 2.4 | 25 | 62.4 | 41.3 | 90.0 | 6.4 | 6.2 | 21.1 | 2577.1 | 3268.0 | 26.0 | 17.2 | 17.21 | 0.797 | 0.797 | 49.703 | 3.77 | 9722 | 1.01 | 20 | | | | | | Yes | 167.32 | 431202 | 44.35 | 1.3E-270 | 1 in 1000000 | |
| B17 | | 119.7 | | 2.4 | 2.4 | 2.4 | 25 | 15.1 | 30.1 | 90.0 | 6.5 | 6.7 | 42.8 | 454.5 | 794.9 | 6.3 | 12.5 | 6.29 | 1.332 | 1.332 | 20.111 | 5.23 | 2379 | 0.77 | 20 | | | | | | Yes | 19.58 | 8900 | 3.74 | 8.3E-17 | 1 in 1000000 | |
| B18 | Tailgate Loading | 119.9 | 22.0 | 2.4 | 2.4 | 2.4 | 25 | 15.7 | 30.1 | 90.0 | 6.6 | 6.7 | 42.4 | 472 | | | | | | | | | | | | | | | | | | | | | | | |

Table A.3: Pillar Stability Analysis

Run 3: Decrease Run 2 Pillars by 1 m

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 3
Calculations by JAW

Key to Colour Coding of Factors of Safety / Width: Height Ratios

| | |
|------|---------------------|
| 4.50 | Greater than 3.0 |
| 2.40 | Between 2.2 and 3.0 |
| 2.10 | Between 1.8 and 2.2 |
| 1.70 | Between 1.5 and 1.8 |
| 1.20 | Less than 1.5 |

Indicating Pillar Located within Project Angle of Draw
Indicating Pillar Located beneath site

| Analysis Id: | Comment | Depth | Panel Width/Span (Longwall only) | Seam Thickness | Working Section | Pillar Height Section | Unit Weight γ (kN/m³) | Pillar Details | | | Adjoint Details | | Extract. Ratio | Pillar Area | Total Area | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) φ _y = 0.7 | Pillar Stress ("Abut") ("Abut") | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|----------------------------------|-------|-------------------------------------|----------------|-----------------|-----------------------|-----------------------------|--------------------|---------------------|--------------------------|-----------------|-----------|----------------|-------------|------------|--------------------------------|---------------------------------|---------------------------|----------------|-------|--------------------|---------------------------------------|----------------------------------|---|------------------------|------------------------------|--------------------------------------|--------------------|------------------------------------|---|---------------------------------------|-------|-------------------|--------------------------|------|---------------------------|--|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (") | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| B66 | Double Goaf Loading | 119.5 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 23.7 | 15.2 | 90.0 | 6.5 | 6.0 | 43.7 | 360.2 | 640.2 | 9.9 | 6.3 | 6.33 | 0.781 | 0.781 | 18.521 | 5.31 | 1913 | 0.90 | 20 | A | G | | 2113 | | 11.17 | Yes | 25.36 | 9136 | 2.27 | 1.3E-07 | 1 in 1000000 |
| B67 | Tailgate Loading | 119.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 23.7 | 15.2 | 90.0 | 6.5 | 6.2 | 44.3 | 360.2 | 646.3 | 9.9 | 6.3 | 6.33 | 0.781 | 0.781 | 18.521 | 5.34 | 1923 | 0.90 | 20 | A | T | | 1803 | | 10.34 | Yes | 25.36 | 9136 | 2.45 | 9.4E-09 | 1 in 1000000 |
| B68 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.8 | 43.9 | 390.0 | 695.4 | 6.3 | 10.8 | 6.25 | 1.268 | 1.268 | 19.024 | 5.35 | 2086 | 0.76 | 20 | A | G | | 3287 | | 13.78 | Yes | 18.99 | 7408 | 1.38 | 1.9E-02 | 1 in 47 |
| B69 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.8 | 43.9 | 390.0 | 695.4 | 6.3 | 10.8 | 6.25 | 1.268 | 1.268 | 19.024 | 5.35 | 2086 | 0.76 | 20 | A | G | | 3287 | | 13.78 | Yes | 18.99 | 7408 | 1.38 | 1.9E-02 | 1 in 47 |
| B70 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.6 | 43.6 | 390.0 | 691.1 | 6.3 | 10.8 | 6.25 | 1.268 | 1.268 | 19.024 | 5.32 | 2073 | 0.76 | 20 | A | G | | 3267 | | 13.69 | Yes | 18.99 | 7408 | 1.39 | 1.7E-02 | 1 in 52 |
| B71 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.7 | 43.7 | 390.0 | 693.2 | 6.3 | 10.8 | 6.25 | 1.268 | 1.268 | 19.024 | 5.33 | 2080 | 0.76 | 20 | A | G | | 3277 | | 13.74 | Yes | 18.99 | 7408 | 1.38 | 1.8E-02 | 1 in 49 |
| B72 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.7 | 43.7 | 390.0 | 693.2 | 6.3 | 10.8 | 6.25 | 1.268 | 1.268 | 19.024 | 5.33 | 2080 | 0.76 | 20 | A | G | | 3277 | | 13.74 | Yes | 18.99 | 7408 | 1.38 | 1.8E-02 | 1 in 49 |
| B73 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.9 | 44.1 | 390.0 | 697.5 | 6.3 | 10.8 | 6.25 | 1.268 | 1.268 | 19.024 | 5.37 | 2092 | 0.76 | 20 | A | G | | 3297 | | 13.82 | Yes | 18.99 | 7408 | 1.37 | 2.0E-02 | 1 in 45 |
| B74 | Double Goaf Loading | 118.2 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 24.3 | 14.5 | 90.0 | 6.5 | 6.3 | 45.0 | 352.4 | 640.6 | 10.1 | 6.0 | 6.04 | 0.747 | 0.747 | 18.162 | 5.37 | 1893 | 0.91 | 20 | A | G | | 2043 | | 11.17 | Yes | 25.75 | 9075 | 2.31 | 7.8E-08 | 1 in 1000000 |
| B75 | Double Goaf Loading | 118.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 24.1 | 14.5 | 90.0 | 6.5 | 6.8 | 46.4 | 349.5 | 651.8 | 10.0 | 6.0 | 6.04 | 0.751 | 0.751 | 18.106 | 5.50 | 1923 | 0.91 | 20 | A | G | | 2087 | | 11.47 | Yes | 25.50 | 8910 | 2.22 | 2.6E-07 | 1 in 1000000 |
| B76 | Maingate Loading | 117.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 25.4 | 14.6 | 90.0 | 6.5 | 6.3 | 44.4 | 370.8 | 666.7 | 10.6 | 6.1 | 6.08 | 0.730 | 0.730 | 18.542 | 5.26 | 1950 | 0.92 | 20 | A | M | | 1118 | | 8.27 | Yes | 27.28 | 10116 | 3.30 | 4.9E-14 | 1 in 1000000 |
| B77 | Rotated panel / Maingate Loading | 118.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 14.4 | 26.7 | 90.0 | 6.7 | 6.3 | 44.8 | 384.5 | 696.3 | 6.0 | 11.1 | 6.00 | 1.299 | 1.299 | 18.709 | 5.34 | 2054 | 0.76 | 20 | A | M | | 1477 | | 9.18 | Yes | 18.62 | 7158 | 2.03 | 4.3E-06 | 1 in 341810 |
| B78 | Rotated panel / Maingate Loading | 119.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 14.3 | 26.3 | 90.0 | 6.6 | 6.3 | 44.8 | 376.1 | 681.3 | 6.0 | 11.0 | 5.96 | 1.296 | 1.291 | 18.460 | 5.39 | 2027 | 0.75 | 20 | A | M | | 1459 | | 9.27 | Yes | 18.46 | 6943 | 1.99 | 7.2E-06 | 1 in 189645 |
| B79 | Rotated panel / Maingate Loading | 120.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 14.5 | 26.3 | 90.0 | 6.4 | 6.3 | 44.0 | 381.4 | 681.3 | 6.0 | 11.0 | 6.04 | 1.289 | 1.289 | 18.694 | 5.36 | 2044 | 0.75 | 20 | A | M | | 1464 | | 9.20 | Yes | 18.64 | 7110 | 2.03 | 4.3E-06 | 1 in 336458 |
| B80 | Rotated panel / Maingate Loading | 121.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 14.5 | 26.3 | 90.0 | 6.7 | 6.3 | 44.8 | 381.4 | 691.1 | 6.0 | 11.0 | 6.04 | 1.289 | 1.289 | 18.694 | 5.48 | 2091 | 0.76 | 20 | A | M | | 1500 | | 9.42 | Yes | 18.64 | 7110 | 1.98 | 8.4E-06 | 1 in 158049 |
| B81 | Rotated panel / Maingate Loading | 122.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 14.5 | 26.3 | 90.0 | 6.6 | 6.3 | 44.6 | 381.4 | 687.9 | 6.0 | 11.0 | 6.04 | 1.289 | 1.289 | 18.694 | 5.50 | 2098 | 0.75 | 20 | A | M | | 1504 | | 9.45 | Yes | 18.64 | 7110 | 1.97 | 9.3E-06 | 1 in 142496 |
| B82 | Rotated panel / Maingate Loading | 123.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 14.5 | 26.3 | 90.0 | 6.6 | 6.3 | 44.6 | 381.4 | 687.9 | 6.0 | 11.0 | 6.04 | 1.289 | 1.289 | 18.694 | 5.55 | 2115 | 0.75 | 20 | A | M | | 1517 | | 9.52 | Yes | 18.64 | 7110 | 1.96 | 1.2E-05 | 1 in 110435 |
| B83 | | 113.0 | | 2.4 | 2.4 | 2.4 | 25 | 12.6 | 8.9 | 90.0 | 6.4 | 7.2 | 63.3 | 112.1 | 305.9 | 5.3 | 3.7 | 3.71 | 0.828 | 0.868 | 10.936 | 7.71 | 864 | 0.72 | 21 | A | M | | 105 | | 8.64 | Yes | 13.87 | 1556 | 1.60 | 1.4E-03 | 1 in 683 |
| B84 | | 113.5 | | 2.4 | 2.4 | 2.4 | 25 | 13.0 | 8.6 | 90.0 | 6.6 | 7.2 | 63.9 | 111.8 | 309.7 | 5.4 | 3.6 | 3.59 | 0.796 | 0.832 | 10.821 | 7.86 | 879 | 0.74 | 22 | A | M | | 109 | | 8.83 | Yes | 13.83 | 1546 | 1.57 | 2.2E-03 | 1 in 417 |
| B85 | | 113.8 | | 2.4 | 2.4 | 2.4 | 25 | 12.8 | 9.0 | 90.0 | 6.4 | 6.3 | 60.8 | 115.2 | 293.8 | 5.3 | 3.8 | 3.75 | 0.826 | 0.862 | 11.028 | 7.25 | 836 | 0.73 | 23 | A | M | | 101 | | 8.13 | Yes | 13.95 | 1607 | 1.71 | 3.8E-04 | 1 in 2982 |

| | |
|------------------------------|--|
| Project: | Lake Macquarie Private Hospital Northern Expansion |
| Location: | O'Brien Street, Gateshead |
| Analysis Assumptions: | NSW Pillar formula |
| Project Number | 16471.21 |

Client: Akalan Projects
Date: 18/10/16
Sheet: 4
Calculations by JAW



| | | |
|------|---------------------|--|
| 4.50 | Greater than 3.0 |  Indicating Pillar Located within Project Angle of Draw  Indicating Pillar Located beneath site |
| 2.40 | Between 2.2 and 3.0 | |
| 2.10 | Between 1.8 and 2.2 | |
| 1.70 | Between 1.5 and 1.8 | |
| 1.20 | Less than 1.5 | |

Table A.4 Run 4 Page 1

Table A.4: Pillar Stability Analysis

Run 4: Increase Run 2 Working Section Height to 3.0 m

Key to Colour Coding of Factors of Safety / Width: Height Ratios

| | |
|------|---------------------|
| 4.50 | Greater than 3.0 |
| 2.40 | Between 2.2 and 3.0 |
| 2.10 | Between 1.8 and 2.2 |
| 1.70 | Between 1.5 and 1.8 |
| 1.20 | Less than 1.5 |

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 4
Calculations by JAW

| Analysis Id. | Comment | Depth D (m) | Panel Width/Span (Longwall only) (m) | Seam Thickness (m) | Working Section H (m) | Pillar Height Section H (m) | Unit Weight γ (kN/m³) | Pillar Details | | | Adjoint Det. | | Extract. Ratio | Pillar Area m³ | Total Area m³ | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment Transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|--------------------------------|-------------------|--|-----------------------|-----------------------------|-----------------------------------|-----------------------------|--------------------|---------------------|-----------------------|--------------|-----------|----------------|-------------------|------------------|--------------------------------|---------------------------------|---------------------------|----------------|-------|-----------------------|---------------------------------------|----------------------------------|--------------------------------------|------------------|------------------------------|-----------------------------------|-----------------|---------------------------------|--|------------------------------------|-------|-------------------|--------------------------|----------|------------------------|--|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (°) | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wΘ Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| A74 | | 122.3 | | 3.0 | 3.0 | 3.0 | 25 | 16.4 | 17.4 | 90.0 | 5.5 | 5.2 | 42.3 | 285.4 | 494.9 | 5.5 | 5.8 | 5.47 | 1.030 | 1.024 | 16.798 | 5.30 | 1513 | 0.77 | 20 | | | | | | Yes | 14.37 | 4099 | 2.71 | 2.3E-10 | 1 in 1000000 | |
| A75 | | 121.8 | | 3.0 | 3.0 | 3.0 | 25 | 16.6 | 16.9 | 90.0 | 5.2 | 5.4 | 42.3 | 280.5 | 486.1 | 5.5 | 5.6 | 5.53 | 1.009 | 1.008 | 16.725 | 5.28 | 1480 | 0.77 | 20 | | | | | | Yes | 14.36 | 4027 | 2.72 | 2.0E-10 | 1 in 1000000 | |
| A76 | | 121.8 | | 3.0 | 3.0 | 3.0 | 25 | 16.6 | 17.1 | 90.0 | 4.8 | 5.7 | 41.8 | 283.9 | 487.9 | 5.5 | 5.7 | 5.53 | 1.015 | 1.013 | 16.808 | 5.23 | 1486 | 0.76 | 20 | | | | | | Yes | 14.39 | 4085 | 2.75 | 1.3E-10 | 1 in 1000000 | |
| A77 | | 121.2 | | 3.0 | 3.0 | 3.0 | 25 | 16.6 | 17.0 | 90.0 | 5.0 | 5.0 | 40.6 | 282.2 | 475.2 | 5.5 | 5.7 | 5.53 | 1.012 | 1.010 | 16.767 | 5.10 | 1440 | 0.76 | 20 | | | | | | Yes | 14.37 | 4056 | 2.82 | 4.9E-11 | 1 in 1000000 | |
| A78 | Maingate Loading | 121.8 | 22.0 | 3.0 | 3.0 | 3.0 | 25 | 16.5 | 29.9 | 90.0 | 5.3 | 4.4 | 34.0 | 493.4 | 747.7 | 5.5 | 10.0 | 5.50 | 1.289 | 1.235 | 20.385 | 4.62 | 2277 | 0.77 | 20 | A | M | | 985 | | 6.61 | Yes | 15.87 | 7828 | 2.40 | 2.0E-08 | 1 in 1000000 |
| A79 | | 121.9 | | 3.0 | 3.0 | 3.0 | 25 | 16.2 | 17.6 | 90.0 | 6.6 | 5.3 | 45.4 | 285.1 | 522.1 | 5.4 | 5.9 | 5.40 | 1.041 | 1.033 | 16.735 | 5.58 | 1591 | 0.79 | 20 | | | | | | Yes | 14.32 | 4083 | 2.57 | 1.8E-09 | 1 in 1000000 | |
| A80 | Tailgate Loading / Double Goaf | 125.6 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 18.5 | 31.5 | 90.0 | 23.2 | 5.0 | 61.7 | 582.8 | 1522.1 | 6.2 | 10.5 | 6.17 | 1.260 | 1.260 | 23.310 | 8.20 | 4779 | 0.98 | 20 | A | G | | 3888 | | 14.87 | Yes | 17.40 | 10138 | 1.17 | 1.8E-01 | 1 in 6 |
| A81 | | 121.8 | | 3.0 | 3.0 | 3.0 | 25 | 15.4 | 17.5 | 90.0 | 5.2 | 5.1 | 42.1 | 269.5 | 465.6 | 5.1 | 5.8 | 5.13 | 1.064 | 1.045 | 16.093 | 5.26 | 1418 | 0.74 | 20 | | | | | | Yes | 13.99 | 3771 | 2.66 | 4.8E-10 | 1 in 1000000 | |
| B1 | | 121.2 | | 3.0 | 3.0 | 3.0 | 25 | 17.2 | 15.9 | 90.0 | 5.4 | 6.7 | 46.5 | 273.5 | 510.8 | 5.7 | 5.3 | 5.30 | 0.961 | 0.964 | 16.583 | 5.66 | 1548 | 0.78 | 20 | | | | | | Yes | 14.37 | 3931 | 2.54 | 2.7E-09 | 1 in 1000000 | |
| B2 | | 120.6 | | 3.0 | 3.0 | 3.0 | 25 | 16.8 | 15.9 | 90.0 | 5.4 | 6.7 | 46.8 | 267.1 | 501.7 | 5.6 | 5.3 | 5.30 | 0.972 | 0.976 | 16.399 | 5.66 | 1513 | 0.78 | 20 | | | | | | Yes | 14.24 | 3803 | 2.51 | 3.9E-09 | 1 in 1000000 | |
| B3 | | 120.1 | | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 15.4 | 90.0 | 5.4 | 6.7 | 47.9 | 246.4 | 472.9 | 5.3 | 5.1 | 5.13 | 0.981 | 0.985 | 15.762 | 5.76 | 1420 | 0.76 | 20 | | | | | | Yes | 13.87 | 3418 | 2.41 | 1.8E-08 | 1 in 1000000 | |
| B4 | | 120.2 | | 3.0 | 3.0 | 3.0 | 25 | 17.3 | 15.7 | 90.0 | 5.4 | 5.0 | 42.2 | 271.6 | 469.9 | 5.8 | 5.2 | 5.23 | 0.952 | 0.955 | 16.525 | 5.20 | 1412 | 0.79 | 20 | | | | | | Yes | 14.36 | 3901 | 2.76 | 1.1E-10 | 1 in 1000000 | |
| B5 | | 119.6 | | 3.0 | 3.0 | 3.0 | 25 | 16.9 | 15.8 | 90.0 | 5.4 | 5.0 | 42.4 | 267.0 | 463.8 | 5.6 | 5.3 | 5.27 | 0.966 | 0.970 | 16.400 | 5.19 | 1387 | 0.78 | 20 | | | | | | Yes | 14.25 | 3805 | 2.74 | 1.4E-10 | 1 in 1000000 | |
| B6 | | 119.2 | | 3.0 | 3.0 | 3.0 | 25 | 17.3 | 16.1 | 90.0 | 5.4 | 5.0 | 41.8 | 278.5 | 479.0 | 5.8 | 5.4 | 5.37 | 0.964 | 0.967 | 16.726 | 5.12 | 1427 | 0.79 | 20 | | | | | | Yes | 14.45 | 4025 | 2.82 | 4.7E-11 | 1 in 1000000 | |
| B7 | | 118.6 | | 3.0 | 3.0 | 3.0 | 25 | 18.3 | 24.6 | 90.0 | 5.4 | 5.2 | 36.3 | 450.2 | 706.3 | 6.1 | 8.2 | 6.10 | 1.147 | 1.147 | 20.987 | 4.65 | 2094 | 0.81 | 20 | | | | | | Yes | 16.44 | 7400 | 3.53 | 1.6E-15 | 1 in 1000000 | |
| B8 | | 119.0 | | 3.0 | 3.0 | 3.0 | 25 | 18.1 | 24.9 | 90.0 | 5.4 | 5.2 | 36.3 | 450.7 | 707.4 | 6.0 | 8.3 | 6.03 | 1.158 | 1.158 | 20.962 | 4.67 | 2104 | 0.80 | 20 | | | | | | Yes | 16.38 | 7383 | 3.51 | 2.4E-15 | 1 in 1000000 | |
| B9 | | 120.0 | | 3.0 | 3.0 | 3.0 | 25 | 18.0 | 24.9 | 90.0 | 5.4 | 5.2 | 36.4 | 448.2 | 704.3 | 6.0 | 8.3 | 6.00 | 1.161 | 1.161 | 20.895 | 4.71 | 2113 | 0.80 | 20 | | | | | | Yes | 16.33 | 7320 | 3.46 | 4.5E-15 | 1 in 1000000 | |
| B10 | | 121.3 | | 3.0 | 3.0 | 3.0 | 25 | 18.8 | 24.7 | 90.0 | 5.4 | 5.2 | 35.8 | 464.4 | 723.6 | 6.3 | 8.2 | 6.27 | 1.136 | 1.136 | 21.350 | 4.73 | 2194 | 0.81 | 20 | | | | | | Yes | 16.72 | 7762 | 3.54 | 1.6E-15 | 1 in 1000000 | |
| B11 | Maingate Loading | 121.8 | 22.0 | 3.0 | 3.0 | 3.0 | 25 | 15.2 | 40.0 | 90.0 | 6.1 | 4.8 | 36.3 | 608.0 | 954.2 | 5.1 | 13.3 | 5.07 | 1.449 | 1.291 | 19.627 | 4.78 | 2906 | 0.76 | 20 | A | M | | 1310 | | 6.93 | Yes | 15.48 | 9411 | 2.23 | 2.2E-07 | 1 in 1000000 |
| B12 | | 121.0 | | 3.0 | 3.0 | 3.0 | 25 | 18.6 | 19.0 | 90.0 | 5.4 | 5.2 | 39.2 | 353.4 | 580.8 | 6.2 | 6.3 | 6.20 | 1.011 | 1.011 | 18.798 | 4.97 | 1757 | 0.81 | 20 | | | | | | Yes | 15.61 | 5518 | 3.14 | 4.7E-13 | 1 in 1000000 | |
| B13 | | 119.7 | | 3.0 | 3.0 | 3.0 | 25 | 16.8 | 18.7 | 90.0 | 5.4 | 5.2 | 40.8 | 314.2 | 530.6 | 5.6 | 6.2 | 5.60 | 1.054 | 1.046 | 17.577 | 5.05 | 1588 | 0.78 | 20 | | | | | | Yes | 14.75 | 4633 | 2.92 | 1.2E-11 | 1 in 1000000 | |
| B14 | | 118.4 | | 3.0 | 3.0 | 3.0 | 25 | 17.2 | 18.7 | 90.0 | 5.4 | 5.2 | 40.5 | 321.6 | 540.1 | 5.7 | 6.2 | 5.73 | 1.042 | 1.038 | 17.854 | 4.97 | 1599 | 0.79 | 20 | | | | | | Yes | 14.92 | 4800 | 3.00 | 3.4E-12 | 1 in 1000000 | |
| B15 | | 117.7 | | 3.0 | 3.0 | 3.0 | 25 | 17.3 | 19.5 | 90.0 | 5.4 | 5.2 | 39.8 | 337.4 | 560.7 | 5.8 | 6.5 | 5.77 | 1.060 | 1.055 | 18.252 | 4.89 | 1650 | 0.79 | 20 | | | | | | Yes | 15.11 | 5097 | 3.09 | 9.8E-13 | 1 in 1000000 | |
| B16 | | 119.0 | | 3.0 | 3.0 | 3.0 | 25 | 63.4 | 42.3 | 90.0 | 5.4 | 5.2 | 17.9 | 2681.8 | 3268.0 | 21.1 | 14.1 | 14.10 | 0.800 | 0.800 | 50.744 | 3.63 | 9722 | 1.01 | 20 | | | | | | Yes | 99.66 | 267280 | 27.49 | 3.0E-165 | 1 in 1000000 | |
| B17 | | 119.7 | | 3.0 | 3.0 | 3.0 | 25 | 16.1 | 31.1 | 90.0 | 5.5 | 5.7 | 37.0 | 500.7 | 794.9 | 5.4 | 10.4 | 5.37 | 1.318 | 1.243 | 20.016 | 4.75 | 2379 | 0.77 | 20 | | | | | | Yes | 15.68 | 7851 | 3.30 | 4.7E-14 | 1 in 1000000 | |
| B18 | Tailgate Loading | 119.9 | 22.0 | 3.0 | 3.0 | 3.0 | 25 | 16.7 | 31.1 | 90.0 | 5.6 | 5.7 | 36.7 | 519.4 | 820.6 | 5.6 | 10.4 | 5.57 | 1.301 | 1.253 | 20.9. | | | | | | | | | | | | | | | | |

Table A.4: Pillar Stability Analysis

Run 4: Increase Run 2 Working Section Height to 3.0 m

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 4
Calculations by JAW

Key to Colour Coding of Factors of Safety / Width: Height Ratios

4.50

Greater than 3.0

2.40

Between 2.2 and 3.0

2.10

Between 1.8 and 2.2

1.70

Between 1.5 and 1.8

1.20

Less than 1.5

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

| Analysis Id: | Comment | Depth | Panel Width/Span (Longwall only) | Seam Thickness | Working Section | Pillar Height Section | Unit Weighth γ (kN/m³) | Pillar Details | | | adway Det | | Extract. Ratio | Pillar Area | Total Area | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment Transfer R | Abutment Angle ° | Abut (A) Yield (Y) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|----------------------------------|-------|-------------------------------------|----------------|-----------------|-----------------------|------------------------------|----------------|--------|-----------------------|-----------|-----------|----------------|-------------|------------|-----------------------------|------------------------------|---------------------------|----------------|-------|-----------------|---------------------------------------|----------------------------------|-----------------------------------|------------------|-----------------------|--------------------------------|-----------------|------------------------------|--|------------------------------------|-------|-------------------|-----------------------|------|------------------------|--|
| | | | | | | | | Width | Length | Internal Angle (") | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| B66 | Double Goaf Loading | 119.5 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 24.7 | 16.2 | 90.0 | 5.5 | 5.0 | 37.5 | 400.1 | 640.2 | 8.2 | 5.4 | 5.40 | 0.792 | 0.792 | 19.567 | 4.78 | 1913 | 0.90 | 20 | A | G | | 2113 | | 10.06 | Yes | 18.46 | 7386 | 1.83 | 6.8E-05 | 1 in 16681 |
| B67 | Tailgate Loading | 119.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 24.7 | 16.2 | 90.0 | 5.5 | 5.2 | 38.1 | 400.1 | 646.3 | 8.2 | 5.4 | 5.40 | 0.792 | 0.792 | 19.567 | 4.81 | 1923 | 0.90 | 20 | A | T | | 1803 | | 9.31 | Yes | 18.46 | 7386 | 1.98 | 8.1E-06 | 1 in 164699 |
| B68 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.8 | 37.9 | 432.0 | 695.4 | 5.3 | 9.0 | 5.33 | 1.256 | 1.194 | 19.101 | 4.83 | 2086 | 0.76 | 20 | A | G | | 3287 | | 12.44 | Yes | 15.30 | 6610 | 1.23 | 1.0E-01 | 1 in 11 |
| B69 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.8 | 37.9 | 432.0 | 695.4 | 5.3 | 9.0 | 5.33 | 1.256 | 1.194 | 19.101 | 4.83 | 2086 | 0.76 | 20 | A | G | | 3287 | | 12.44 | Yes | 15.30 | 6610 | 1.23 | 1.0E-01 | 1 in 11 |
| B70 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.6 | 37.5 | 432.0 | 691.1 | 5.3 | 9.0 | 5.33 | 1.256 | 1.194 | 19.101 | 4.80 | 2073 | 0.76 | 20 | A | G | | 3267 | | 12.36 | Yes | 15.30 | 6610 | 1.24 | 9.4E-02 | 1 in 12 |
| B71 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.7 | 37.7 | 432.0 | 693.2 | 5.3 | 9.0 | 5.33 | 1.256 | 1.194 | 19.101 | 4.81 | 2080 | 0.76 | 20 | A | G | | 3277 | | 12.40 | Yes | 15.30 | 6610 | 1.23 | 9.8E-02 | 1 in 11 |
| B72 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.7 | 37.7 | 432.0 | 693.2 | 5.3 | 9.0 | 5.33 | 1.256 | 1.194 | 19.101 | 4.81 | 2080 | 0.76 | 20 | A | G | | 3277 | | 12.40 | Yes | 15.30 | 6610 | 1.23 | 9.8E-02 | 1 in 11 |
| B73 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 27.0 | 90.0 | 5.2 | 5.9 | 38.1 | 432.0 | 697.5 | 5.3 | 9.0 | 5.33 | 1.256 | 1.194 | 19.101 | 4.84 | 2092 | 0.76 | 20 | A | G | | 3297 | | 12.48 | Yes | 15.30 | 6610 | 1.23 | 1.1E-01 | 1 in 10 |
| B74 | Double Goaf Loading | 118.2 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 25.3 | 15.5 | 90.0 | 5.5 | 5.3 | 38.8 | 392.2 | 640.6 | 8.4 | 5.2 | 5.17 | 0.760 | 0.760 | 19.223 | 4.83 | 1893 | 0.91 | 20 | A | G | | 2043 | | 10.04 | Yes | 18.63 | 7305 | 1.86 | 5.0E-05 | 1 in 22922 |
| B75 | Double Goaf Loading | 118.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 25.1 | 15.5 | 90.0 | 5.5 | 5.8 | 40.3 | 389.1 | 651.8 | 8.4 | 5.2 | 5.17 | 0.764 | 0.764 | 19.165 | 4.94 | 1923 | 0.91 | 20 | A | G | | 2087 | | 10.31 | Yes | 18.49 | 7192 | 1.79 | 1.2E-04 | 1 in 9113 |
| B76 | Maingate Loading | 117.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 26.4 | 15.6 | 90.0 | 5.5 | 5.3 | 38.2 | 411.8 | 666.7 | 8.8 | 5.2 | 5.20 | 0.743 | 0.743 | 19.611 | 4.74 | 1950 | 0.92 | 20 | A | M | | 1090 | | 7.38 | Yes | 19.47 | 8020 | 2.64 | 6.5E-10 | 1 in 1000000 |
| B77 | Rotated panel / Maingate Loading | 118.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.4 | 27.7 | 90.0 | 5.7 | 5.3 | 38.7 | 426.6 | 696.3 | 5.1 | 9.2 | 5.13 | 1.285 | 1.195 | 18.410 | 4.82 | 2054 | 0.76 | 20 | A | M | | 1440 | | 8.19 | Yes | 14.99 | 6392 | 1.83 | 7.3E-05 | 1 in 15475 |
| B78 | Rotated panel / Maingate Loading | 119.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.3 | 27.3 | 90.0 | 5.6 | 5.3 | 38.7 | 417.7 | 681.3 | 5.1 | 9.1 | 5.10 | 1.282 | 1.190 | 18.203 | 4.85 | 2027 | 0.75 | 20 | A | M | | 1423 | | 8.26 | Yes | 14.90 | 6222 | 1.80 | 1.1E-04 | 1 in 10545 |
| B79 | Rotated panel / Maingate Loading | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.5 | 27.3 | 90.0 | 5.4 | 5.3 | 37.9 | 423.2 | 681.3 | 5.2 | 9.1 | 5.17 | 1.276 | 1.192 | 18.480 | 4.83 | 2044 | 0.75 | 20 | A | M | | 1428 | | 8.20 | Yes | 15.02 | 6355 | 1.83 | 7.3E-05 | 1 in 15669 |
| B80 | Rotated panel / Maingate Loading | 121.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.5 | 27.3 | 90.0 | 5.7 | 5.3 | 38.8 | 423.2 | 691.1 | 5.2 | 9.1 | 5.17 | 1.276 | 1.192 | 18.480 | 4.94 | 2091 | 0.76 | 20 | A | M | | 1463 | | 8.40 | Yes | 15.02 | 6355 | 1.79 | 1.3E-04 | 1 in 8450 |
| B81 | Rotated panel / Maingate Loading | 122.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.5 | 27.3 | 90.0 | 5.6 | 5.3 | 38.5 | 423.2 | 687.9 | 5.2 | 9.1 | 5.17 | 1.276 | 1.192 | 18.480 | 4.96 | 2098 | 0.75 | 20 | A | M | | 1467 | | 8.42 | Yes | 15.02 | 6355 | 1.78 | 1.4E-04 | 1 in 7767 |
| B82 | Rotated panel / Maingate Loading | 123.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.5 | 27.3 | 90.0 | 5.6 | 5.3 | 38.5 | 423.2 | 687.9 | 5.2 | 9.1 | 5.17 | 1.276 | 1.192 | 18.480 | 5.00 | 2115 | 0.75 | 20 | A | M | | 1479 | | 8.49 | Yes | 15.02 | 6355 | 1.77 | 1.8E-04 | 1 in 6309 |
| B83 | | 113.0 | | 3.0 | 3.0 | 3.0 | 25 | 13.6 | 9.9 | 90.0 | 5.4 | 6.2 | 56.0 | 134.6 | 305.9 | 4.5 | 3.3 | 3.30 | 0.843 | 0.916 | 12.460 | 6.42 | 864 | 0.72 | 21 | A | M | | 89 | | 7.08 | No | 12.37 | 1666 | 1.75 | 2.4E-04 | 1 in 4733 |
| B84 | | 113.5 | | 3.0 | 3.0 | 3.0 | 25 | 14.0 | 9.6 | 90.0 | 5.6 | 6.2 | 56.6 | 134.4 | 309.7 | 4.7 | 3.2 | 3.20 | 0.814 | 0.892 | 12.484 | 6.54 | 879 | 0.74 | 22 | A | M | | 92 | | 7.23 | No | 12.38 | 1664 | 1.71 | 3.9E-04 | 1 in 2941 |
| B85 | | 113.8 | | 3.0 | 3.0 | 3.0 | 25 | 13.8 | 10.0 | 90.0 | 5.4 | 5.3 | 53.0 | 138.0 | 293.8 | 4.6 | 3.3 | 3.33 | 0.840 | 0.911 | 12.577 | 6.06 | 836 | 0.73 | 23 | A | M | | 85 | | 6.67 | No | 12.43 | 1715 | 1.86 | 4.6E-05 | 1 in 25244 |

Table A.5: Pillar Stability Analysis

Run 5: Decrease Run 2 Pillars by 1 m and increase working section to 3.0 m

Key to Colour Coding of Factors of Safety / Width: Height Ratios

| | |
|------|---------------------|
| 4.50 | Greater than 3.0 |
| 2.40 | Between 2.2 and 3.0 |
| 2.10 | Between 1.8 and 2.2 |
| 1.70 | Between 1.5 and 1.8 |
| 1.20 | Less than 1.5 |

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

Project:

Lake Macquarie Private Hospital Northern Expansion

Location:

O'Brien Street, Gateshead

Analysis Assumptions:

NSW Pillar formula

Project Number

16471.21

Client:

Akalan Projects

Date:

18/10/16

Sheet:

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Calculations by JAW

| Analysis Id. | Comment | Depth | Panel Width/Span (Longwall only) | Seam Thickness | Working Section | Pillar Height Section | Unit Weight γ (kN/m³) | Pillar Details | | | Adway Det | | Extract. Ratio | Pillar Area | Total Area | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|------------------|-------|-------------------------------------|----------------|-----------------|-----------------------|-----------------------------|----------------|---------------|--------------------|-----------|--------|----------------|-------------|------------|--------------------------|---------------------------|---------------------|----------------|-------|--------------------|---------------------------------|----------------------------|--------------------------------|------------------|------------------------|-----------------------------|--------------|---------------------------|---|------------------------------|-------|----------------|--------------------|---------|------------------------|--|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (°) | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wΘ Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A1 | | 127.7 | | 3.0 | 3.0 | 3.0 | 25 | 17.6 | 30.0 | 90.0 | 5.9 | 6.2 | 37.9 | 528.0 | 850.7 | 5.9 | 10.0 | 5.87 | 1.261 | 1.248 | 21.958 | 5.14 | 2716 | 0.79 | 20 | | | | | | Yes | 16.66 | 8798 | 3.24 | 1.1E-13 | 1 in 1000000 | |
| A2 | | 126.7 | | 3.0 | 3.0 | 3.0 | 25 | 16.4 | 30.5 | 90.0 | 6.2 | 6.1 | 39.5 | 500.2 | 827.2 | 5.5 | 10.2 | 5.47 | 1.301 | 1.241 | 20.357 | 5.24 | 2619 | 0.77 | 20 | | | | | | Yes | 15.84 | 7926 | 3.03 | 2.4E-12 | 1 in 1000000 | |
| A3 | | 126.7 | | 3.0 | 3.0 | 3.0 | 25 | 18.1 | 30.4 | 90.0 | 6.3 | 6.4 | 38.7 | 550.2 | 897.9 | 6.0 | 10.1 | 6.03 | 1.254 | 1.254 | 22.690 | 5.17 | 2843 | 0.81 | 20 | | | | | | Yes | 17.06 | 9385 | 3.30 | 4.7E-14 | 1 in 1000000 | |
| A4 | Tailgate Loading | 124.6 | 22.0 | 3.0 | 3.0 | 3.0 | 25 | 15.8 | 30.4 | 90.0 | 6.4 | 6.1 | 40.7 | 480.3 | 810.3 | 5.3 | 10.1 | 5.27 | 1.316 | 1.231 | 19.443 | 5.25 | 2523 | 0.77 | 20 | A | T | | 1868 | | 9.14 | Yes | 15.43 | 7410 | 1.69 | 5.7E-04 | 1 in 2045 |
| A5 | | 124.1 | | 3.0 | 3.0 | 3.0 | 25 | 15.5 | 30.1 | 90.0 | 6.4 | 6.2 | 41.3 | 466.6 | 795.0 | 5.2 | 10.0 | 5.17 | 1.320 | 1.222 | 18.943 | 5.29 | 2466 | 0.77 | 20 | | | | | | Yes | 15.21 | 7096 | 2.88 | 2.1E-11 | 1 in 1000000 | |
| A6 | | 123.6 | | 3.0 | 3.0 | 3.0 | 25 | 16.7 | 25.9 | 90.0 | 5.8 | 6.3 | 40.3 | 432.5 | 724.5 | 5.6 | 8.6 | 5.57 | 1.216 | 1.182 | 19.741 | 5.17 | 2238 | 0.78 | 20 | | | | | | Yes | 15.63 | 6763 | 3.02 | 2.6E-12 | 1 in 1000000 | |
| A7 | | 123.1 | | 3.0 | 3.0 | 3.0 | 25 | 16.2 | 25.5 | 90.0 | 6.2 | 6.4 | 42.2 | 413.1 | 714.6 | 5.4 | 8.5 | 5.40 | 1.223 | 1.175 | 19.031 | 5.32 | 2199 | 0.78 | 20 | | | | | | Yes | 15.29 | 6316 | 2.87 | 2.2E-11 | 1 in 1000000 | |
| A8 | | 122.7 | | 3.0 | 3.0 | 3.0 | 25 | 15.7 | 25.5 | 90.0 | 6.4 | 6.8 | 43.9 | 400.4 | 713.8 | 5.2 | 8.5 | 5.23 | 1.238 | 1.172 | 18.403 | 5.47 | 2189 | 0.77 | 20 | | | | | | Yes | 14.99 | 6003 | 2.74 | 1.5E-10 | 1 in 1000000 | |
| A9 | | 121.4 | | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 26.6 | 90.0 | 6.0 | 6.3 | 41.2 | 425.6 | 723.8 | 5.3 | 8.9 | 5.33 | 1.249 | 1.189 | 19.019 | 5.16 | 2196 | 0.77 | 20 | | | | | | Yes | 15.27 | 6498 | 2.96 | 6.4E-12 | 1 in 1000000 | |
| A10 | | 123.9 | | 3.0 | 3.0 | 3.0 | 25 | 16.3 | 16.4 | 90.0 | 6.3 | 5.9 | 47.0 | 267.3 | 504.0 | 5.4 | 5.5 | 5.43 | 1.003 | 1.002 | 16.340 | 5.84 | 1561 | 0.78 | 20 | | | | | | Yes | 14.16 | 3784 | 2.42 | 1.4E-08 | 1 in 1000000 | |
| A11 | | 124.2 | | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 16.3 | 90.0 | 6.3 | 6.0 | 47.6 | 260.8 | 497.3 | 5.3 | 5.4 | 5.33 | 1.009 | 1.007 | 16.115 | 5.92 | 1544 | 0.77 | 20 | | | | | | Yes | 14.03 | 3659 | 2.37 | 3.1E-08 | 1 in 1000000 | |
| A12 | | 123.2 | | 3.0 | 3.0 | 3.0 | 25 | 15.7 | 16.1 | 90.0 | 6.1 | 6.2 | 48.0 | 252.8 | 486.1 | 5.2 | 5.4 | 5.23 | 1.013 | 1.009 | 15.847 | 5.93 | 1498 | 0.76 | 20 | | | | | | Yes | 13.89 | 3512 | 2.34 | 4.4E-08 | 1 in 1000000 | |
| A13 | | 123.0 | | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 16.0 | 90.0 | 6.3 | 6.1 | 48.1 | 256.0 | 492.8 | 5.3 | 5.3 | 5.33 | 1.000 | 1.000 | 16.000 | 5.92 | 1515 | 0.78 | 20 | | | | | | Yes | 13.98 | 3579 | 2.36 | 3.5E-08 | 1 in 1000000 | |
| A14 | | 121.9 | | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 16.1 | 90.0 | 6.5 | 6.7 | 49.8 | 257.6 | 513.0 | 5.3 | 5.4 | 5.33 | 1.003 | 1.002 | 16.039 | 6.07 | 1563 | 0.78 | 20 | | | | | | Yes | 14.00 | 3606 | 2.31 | 7.7E-08 | 1 in 1000000 | |
| A15 | | 128.8 | | 3.0 | 3.0 | 3.0 | 25 | 23.5 | 37.0 | 90.0 | 5.2 | 6.1 | 29.7 | 869.5 | 1237.0 | 7.8 | 12.3 | 7.83 | 1.223 | 1.223 | 28.744 | 4.58 | 3984 | 0.87 | 20 | | | | | | Yes | 21.69 | 18859 | 4.73 | 5.2E-23 | 1 in 1000000 | |
| A16 | | 128.9 | | 3.0 | 3.0 | 3.0 | 25 | 17.6 | 30.5 | 90.0 | 6.4 | 6.3 | 39.2 | 536.8 | 883.2 | 5.9 | 10.2 | 5.87 | 1.268 | 1.255 | 22.086 | 5.30 | 2846 | 0.80 | 20 | | | | | | Yes | 16.71 | 8971 | 3.15 | 4.0E-13 | 1 in 1000000 | |
| A17 | | 128.8 | | 3.0 | 3.0 | 3.0 | 25 | 19.0 | 30.7 | 90.0 | 6.3 | 6.9 | 38.7 | 583.3 | 951.3 | 6.3 | 10.2 | 6.33 | 1.235 | 1.235 | 23.473 | 5.25 | 3064 | 0.82 | 20 | | | | | | Yes | 17.60 | 10268 | 3.35 | 2.3E-14 | 1 in 1000000 | |
| A18 | | 127.3 | | 3.0 | 3.0 | 3.0 | 25 | 18.1 | 30.7 | 90.0 | 6.2 | 6.4 | 38.4 | 555.7 | 901.5 | 6.0 | 10.2 | 6.03 | 1.258 | 1.258 | 22.773 | 5.16 | 2869 | 0.80 | 20 | | | | | | Yes | 17.09 | 9495 | 3.31 | 4.1E-14 | 1 in 1000000 | |
| A19 | | 125.9 | | 3.0 | 3.0 | 3.0 | 25 | 16.0 | 30.5 | 90.0 | 6.2 | 6.5 | 40.6 | 488.0 | 821.4 | 5.3 | 10.2 | 5.33 | 1.312 | 1.235 | 19.761 | 5.30 | 2585 | 0.77 | 20 | | | | | | Yes | 15.57 | 7598 | 2.94 | 8.6E-12 | 1 in 1000000 | |
| A20 | | 125.1 | | 3.0 | 3.0 | 3.0 | 25 | 15.3 | 30.5 | 90.0 | 6.3 | 6.4 | 41.5 | 466.7 | 797.0 | 5.1 | 10.2 | 5.10 | 1.332 | 1.222 | 18.699 | 5.34 | 2493 | 0.76 | 20 | | | | | | Yes | 15.10 | 7048 | 2.83 | 4.3E-11 | 1 in 1000000 | |
| A21 | | 124.4 | | 3.0 | 3.0 | 3.0 | 25 | 16.2 | 15.0 | 90.0 | 6.3 | 6.0 | 48.6 | 243.0 | 472.5 | 5.4 | 5.0 | 5.00 | 0.962 | 0.969 | 15.700 | 6.05 | 1469 | 0.78 | 20 | | | | | | Yes | 13.86 | 3368 | 2.29 | 9.5E-08 | 1 in 1000000 | |
| A22 | | 123.9 | | 3.0 | 3.0 | 3.0 | 25 | 16.2 | 15.4 | 90.0 | 6.2 | 6.0 | 48.0 | 249.5 | 479.4 | 5.4 | 5.1 | 5.13 | 0.975 | 0.980 | 15.871 | 5.95 | 1485 | 0.78 | 20 | | | | | | Yes | 13.94 | 3477 | 2.34 | 4.7E-08 | 1 in 1000000 | |
| A23 | | 123.6 | | 3.0 | 3.0 | 3.0 | 25 | 16.4 | 15.4 | 90.0 | 5.8 | 6.3 | 47.6 | 252.6 | 481.7 | 5.5 | 5.1 | 5.13 | 0.969 | 0.974 | 15.975 | 5.89 | 1489 | 0.77 | 20 | | | | | | Yes | 14.00 | 3536 | 2.38 | 2.8E-08 | 1 in 1000000 | |
| A24 | | 123.0 | | 3.0 | 3.0 | 3.0 | 25 | 16.4 | 15.4 | 90.0 | 6.3 | 6.2 | 48.5 | 252.6 | 490.3 | 5.5 | 5.1 | 5.13 | 0.969 | 0.974 | 15.975 | 5.97 | 1508 | 0.78 | 20 | | | | | | Yes | 14.00 | 3536 | 2.35 | 4.4E-08 | 1 in 1000000 | |
| A25 | | 121.9 | | 3.0 | 3.0 | 3.0 | 25 | 16.4 | 15.4 | 90.0 | 6.3 | 6.3 | 48.7 | 252.6 | 492.6 | 5.5 | 5.1 | 5.13 | 0.969 | 0.974 | 15.975 | 5.94 | 1501 | 0.78 | 20 | | | | | | Yes | 14.00 | 3536 | 2.36 | 3.8E-08 | 1 in 1000000 | |
| A26 | Tailgate Loading | 129.9 | 22.0 | 3.0 | 3.0 | 3.0 | 25 | 19.5 | 22.8 | 90.0 | 6.4 | 7.2 | 42.8 | 444.6 | 777.0 | 6.5 | 7.6 | 6.50 | 1.078 | 1.078 | 21.021 | 5.68 | 2523 | 0.83 | 20 | A | T | | 1610 | | 9.30 | Yes | 16.79 | 7466 | 1.81 | 1.0E-04 | 1 in 10976 |
| A27 | Tailgate Loading | 130.2 | 22.0 | 3.0 | 3.0 | 3.0 | 25 | 21.5 | 39.1 | 90.0 | 6.6 | 7.2 | 35.4 | 840.7 | 1301.0 | 7.2 | 13.0 | 7.17 | 1.290 | 1.290 | 27.744 | 5.04 | 4236 | 0.86 | 20 | A | T | | 2492 | | 8.00 | Yes | 20.21 | 16988 | 2.62 | 3.3E-09 | 1 in 1000000 |
| A28 | | 128.8 | | 3.0 | 3.0 | 3.0 | 25 | 22.4 | 24.8 | 90.0 | 6.4 | 6.3 | 38.0 | 555.5 | | | | | | | | | | | | | | | | | | | | | | | |

Table A.5: Pillar Stability Analysis

Run 5: Decrease Run 2 Pillars by 1 m and increase working section to 3.0 m

Key to Colour Coding of Factors of Safety / Width: Height Ratios

| | |
|------|---------------------|
| 4.50 | Greater than 3.0 |
| 2.40 | Between 2.2 and 3.0 |
| 2.10 | Between 1.8 and 2.2 |
| 1.70 | Between 1.5 and 1.8 |
| 1.20 | Less than 1.5 |

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 5
Calculations by JAW

| Analysis Id. | Comment | Depth | Panel Width/Span (Longwall only) | Seam Thickness | Working Section | Pillar Height Section | Unit Weight γ (kN/m³) | Pillar Details | | | Adway Det. | | Extract. Ratio | Pillar Area | Total Area | w1/ Height Ratio w1/H | w2/H Height Ratio w2/H | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment Transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress ("Yield") φ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|--------------------------------|-------|-------------------------------------|----------------|-----------------|-----------------------|-----------------------------|----------------|--------|--------------------|------------|--------|----------------|-------------|------------|-----------------------------|------------------------------|------------------------|----------------|-------|-----------------------|---------------------------------------|----------------------------------|-----------------------------------|------------------|------------------------------|-----------------------------------|-----------------|---------------------------------|--|------------------------------------|-------|----------------|-----------------------|----------|------------------------|--|
| | | | | | | | | Width | Length | Internal Angle (°) | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wΘ Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| A74 | | 122.3 | | 3.0 | 3.0 | 3.0 | 25 | 15.4 | 16.4 | 90.0 | 6.5 | 6.2 | 49.0 | 252.6 | 494.9 | 5.1 | 5.5 | 5.13 | 1.031 | 1.022 | 15.743 | 5.99 | 1513 | 0.77 | 20 | | | | | | Yes | 13.84 | 3494 | 2.31 | 7.4E-08 | 1 in 1000000 | |
| A75 | | 121.8 | | 3.0 | 3.0 | 3.0 | 25 | 15.6 | 15.9 | 90.0 | 6.2 | 6.4 | 49.0 | 248.0 | 486.1 | 5.2 | 5.3 | 5.20 | 1.010 | 1.007 | 15.709 | 5.97 | 1480 | 0.77 | 20 | | | | | | Yes | 13.83 | 3430 | 2.32 | 6.6E-08 | 1 in 1000000 | |
| A76 | | 121.8 | | 3.0 | 3.0 | 3.0 | 25 | 15.6 | 16.1 | 90.0 | 5.8 | 6.7 | 48.5 | 251.2 | 487.9 | 5.2 | 5.4 | 5.20 | 1.016 | 1.012 | 15.780 | 5.92 | 1486 | 0.76 | 20 | | | | | | Yes | 13.86 | 3481 | 2.34 | 4.6E-08 | 1 in 1000000 | |
| A77 | | 121.2 | | 3.0 | 3.0 | 3.0 | 25 | 15.6 | 16.0 | 90.0 | 6.0 | 6.0 | 47.5 | 249.6 | 475.2 | 5.2 | 5.3 | 5.20 | 1.013 | 1.009 | 15.745 | 5.77 | 1440 | 0.76 | 20 | | | | | | Yes | 13.84 | 3455 | 2.40 | 2.0E-08 | 1 in 1000000 | |
| A78 | Maingate Loading | 121.8 | 22.0 | 3.0 | 3.0 | 3.0 | 25 | 15.5 | 28.9 | 90.0 | 6.3 | 5.4 | 40.1 | 448.0 | 747.7 | 5.2 | 9.6 | 5.17 | 1.302 | 1.210 | 18.752 | 5.08 | 2277 | 0.77 | 20 | A | M | | 1025 | | 7.37 | Yes | 15.13 | 6778 | 2.05 | 3.0E-06 | 1 in 519867 |
| A79 | | 121.9 | | 3.0 | 3.0 | 3.0 | 25 | 15.2 | 16.6 | 90.0 | 7.6 | 6.3 | 51.7 | 252.3 | 522.1 | 5.1 | 5.5 | 5.07 | 1.044 | 1.030 | 15.658 | 6.31 | 1591 | 0.79 | 20 | | | | | | Yes | 13.79 | 3480 | 2.19 | 4.3E-07 | 1 in 1000000 | |
| A80 | Tailgate Loading / Double Goaf | 125.6 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 17.5 | 30.5 | 90.0 | 24.2 | 6.0 | 64.9 | 533.8 | 1522.1 | 5.8 | 10.2 | 5.83 | 1.271 | 1.254 | 21.945 | 8.95 | 4779 | 0.98 | 20 | A | G | | 3888 | | 16.24 | Yes | 16.64 | 8880 | 1.02 | 4.5E-01 | 1 in 2 |
| A81 | | 121.8 | | 3.0 | 3.0 | 3.0 | 25 | 14.4 | 16.5 | 90.0 | 6.2 | 6.1 | 49.0 | 237.6 | 465.6 | 4.8 | 5.5 | 4.80 | 1.068 | 1.040 | 14.979 | 5.97 | 1418 | 0.74 | 20 | | | | | | No | 13.59 | 3229 | 2.28 | 1.2E-07 | 1 in 1000000 | |
| B1 | | 121.2 | | 3.0 | 3.0 | 3.0 | 25 | 16.2 | 14.9 | 90.0 | 6.4 | 7.7 | 52.7 | 241.4 | 510.8 | 5.4 | 5.0 | 4.97 | 0.958 | 0.966 | 15.656 | 6.41 | 1548 | 0.78 | 20 | | | | | | Yes | 13.84 | 3341 | 2.16 | 6.4E-07 | 1 in 1000000 | |
| B2 | | 120.6 | | 3.0 | 3.0 | 3.0 | 25 | 15.8 | 14.9 | 90.0 | 6.4 | 7.7 | 53.1 | 235.4 | 501.7 | 5.3 | 5.0 | 4.97 | 0.971 | 0.978 | 15.449 | 6.43 | 1513 | 0.78 | 20 | | | | | | Yes | 13.72 | 3230 | 2.14 | 9.0E-07 | 1 in 1000000 | |
| B3 | | 120.1 | | 3.0 | 3.0 | 3.0 | 25 | 15.0 | 14.4 | 90.0 | 6.4 | 7.7 | 54.3 | 216.0 | 472.9 | 5.0 | 4.8 | 4.80 | 0.980 | 0.986 | 14.795 | 6.57 | 1420 | 0.76 | 20 | | | | | | Yes | 13.50 | 2917 | 2.05 | 2.9E-06 | 1 in 532475 | |
| B4 | | 120.2 | | 3.0 | 3.0 | 3.0 | 25 | 16.3 | 14.7 | 90.0 | 6.4 | 6.0 | 49.0 | 239.6 | 469.9 | 5.4 | 4.9 | 4.90 | 0.948 | 0.958 | 15.614 | 5.89 | 1412 | 0.79 | 20 | | | | | | Yes | 13.83 | 3314 | 2.35 | 4.3E-08 | 1 in 1000000 | |
| B5 | | 119.6 | | 3.0 | 3.0 | 3.0 | 25 | 15.9 | 14.8 | 90.0 | 6.4 | 6.0 | 49.3 | 235.3 | 463.8 | 5.3 | 4.9 | 4.93 | 0.964 | 0.972 | 15.461 | 5.89 | 1387 | 0.78 | 20 | | | | | | Yes | 13.73 | 3231 | 2.33 | 5.5E-08 | 1 in 1000000 | |
| B6 | | 119.2 | | 3.0 | 3.0 | 3.0 | 25 | 16.3 | 15.1 | 90.0 | 6.4 | 6.0 | 48.6 | 246.1 | 479.0 | 5.4 | 5.0 | 5.03 | 0.962 | 0.969 | 15.793 | 5.80 | 1427 | 0.79 | 20 | | | | | | Yes | 13.91 | 3424 | 2.40 | 2.0E-08 | 1 in 1000000 | |
| B7 | | 118.6 | | 3.0 | 3.0 | 3.0 | 25 | 17.3 | 23.6 | 90.0 | 6.4 | 6.2 | 42.2 | 408.3 | 706.3 | 5.8 | 7.9 | 5.77 | 1.154 | 1.141 | 19.744 | 5.13 | 2094 | 0.81 | 20 | | | | | | Yes | 15.73 | 6421 | 3.07 | 1.4E-12 | 1 in 1000000 | |
| B8 | | 119.0 | | 3.0 | 3.0 | 3.0 | 25 | 17.1 | 23.9 | 90.0 | 6.4 | 6.2 | 42.2 | 408.7 | 707.4 | 5.7 | 8.0 | 5.70 | 1.166 | 1.148 | 19.633 | 5.15 | 2104 | 0.80 | 20 | | | | | | Yes | 15.65 | 6396 | 3.04 | 2.0E-12 | 1 in 1000000 | |
| B9 | | 120.0 | | 3.0 | 3.0 | 3.0 | 25 | 17.0 | 23.9 | 90.0 | 6.4 | 6.2 | 42.3 | 406.3 | 704.3 | 5.7 | 8.0 | 5.67 | 1.169 | 1.149 | 19.527 | 5.20 | 2113 | 0.80 | 20 | | | | | | Yes | 15.59 | 6334 | 3.00 | 3.7E-12 | 1 in 1000000 | |
| B10 | | 121.3 | | 3.0 | 3.0 | 3.0 | 25 | 17.8 | 23.7 | 90.0 | 6.4 | 6.2 | 41.7 | 421.9 | 723.6 | 5.9 | 7.9 | 5.93 | 1.142 | 1.139 | 20.271 | 5.20 | 2194 | 0.81 | 20 | | | | | | Yes | 16.04 | 6765 | 3.08 | 1.1E-12 | 1 in 1000000 | |
| B11 | Maingate Loading | 121.8 | 22.0 | 3.0 | 3.0 | 3.0 | 25 | 14.2 | 39.0 | 90.0 | 7.1 | 5.8 | 42.0 | 553.8 | 954.2 | 4.7 | 13.0 | 4.73 | 1.466 | 1.247 | 17.714 | 5.25 | 2906 | 0.76 | 20 | A | M | | 1362 | | 7.71 | No | 14.80 | 8198 | 1.92 | 2.0E-05 | 1 in 61963 |
| B12 | | 121.0 | | 3.0 | 3.0 | 3.0 | 25 | 17.6 | 18.0 | 90.0 | 6.4 | 6.2 | 45.5 | 316.8 | 580.8 | 5.9 | 6.0 | 5.87 | 1.011 | 1.011 | 17.789 | 5.55 | 1757 | 0.81 | 20 | | | | | | Yes | 14.97 | 4741 | 2.70 | 2.7E-10 | 1 in 1000000 | |
| B13 | | 119.7 | | 3.0 | 3.0 | 3.0 | 25 | 15.8 | 17.7 | 90.0 | 6.4 | 6.2 | 47.3 | 279.7 | 530.6 | 5.3 | 5.9 | 5.27 | 1.057 | 1.043 | 16.472 | 5.68 | 1588 | 0.78 | 20 | | | | | | Yes | 14.18 | 3964 | 2.50 | 5.0E-09 | 1 in 1000000 | |
| B14 | | 118.4 | | 3.0 | 3.0 | 3.0 | 25 | 16.2 | 17.7 | 90.0 | 6.4 | 6.2 | 46.9 | 286.7 | 540.1 | 5.4 | 5.9 | 5.40 | 1.044 | 1.035 | 16.771 | 5.58 | 1599 | 0.79 | 20 | | | | | | Yes | 14.34 | 4111 | 2.57 | 1.7E-09 | 1 in 1000000 | |
| B15 | | 117.7 | | 3.0 | 3.0 | 3.0 | 25 | 16.3 | 18.5 | 90.0 | 6.4 | 6.2 | 46.2 | 301.6 | 560.7 | 5.4 | 6.2 | 5.43 | 1.063 | 1.051 | 17.131 | 5.47 | 1650 | 0.79 | 20 | | | | | | Yes | 14.50 | 4373 | 2.65 | 5.5E-10 | 1 in 1000000 | |
| B16 | | 119.0 | | 3.0 | 3.0 | 3.0 | 25 | 62.4 | 41.3 | 90.0 | 6.4 | 6.2 | 21.1 | 2577.1 | 3268.0 | 20.8 | 13.8 | 13.77 | 0.797 | 0.797 | 49.703 | 3.77 | 9722 | 1.01 | 20 | | | | | | Yes | 96.12 | 247720 | 25.48 | 1.1E-152 | 1 in 1000000 | |
| B17 | | 119.7 | | 3.0 | 3.0 | 3.0 | 25 | 15.1 | 30.1 | 90.0 | 6.5 | 6.7 | 42.8 | 454.5 | 794.9 | 5.0 | 10.0 | 5.03 | 1.332 | 1.214 | 18.337 | 5.23 | 2379 | 0.77 | 20 | | | | | | Yes | 14.95 | 6795 | 2.86 | 2.8E-11 | 1 in 1000000 | |
| B18 | Tailgate Loading | 119.9 | 22.0 | 3.0 | 3.0 | 3.0 | 25 | 15.7 | 30.1 | 90.0 | 6.6 | 6.7 | 42.4 | 472.6 | 820.6 | 5.2 | 10.0 | 5.23 | 1.314 | 1.226 | 19.244 | 5.21 | 2460 | 0.78 | 20 | A | T | | 1803 | | 9.02 | Yes | 15.34 | | | | |

Table A.5: Pillar Stability Analysis

Run 5: Decrease Run 2 Pillars by 1 m and increase working section to 3.0 m

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 5
Calculations by JAW

Key to Colour Coding of Factors of Safety / Width: Height Ratios

| | |
|------|---------------------|
| 4.50 | Greater than 3.0 |
| 2.40 | Between 2.2 and 3.0 |
| 2.10 | Between 1.8 and 2.2 |
| 1.70 | Between 1.5 and 1.8 |
| 1.20 | Less than 1.5 |

Indicating Pillar Located within Project Angle of Draw
Indicating Pillar Located beneath site

| Analysis Id: | Comment | Depth | Panel Width/Span (Longwall only) | Seam Thickness | Working Section | Pillar Height Section | Unit Weight γ (kN/m³) | Pillar Details | | | Adway Details | | Extract. Ratio | Pillar Area | Total Area | w1/ Height | w2/H Height | Width/ Height | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment Transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress (MPa) φ _b = 0.7 | Pillar Stress ("Abut") ("MPa") | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|----------------------------------|-------|-------------------------------------|----------------|-----------------|-----------------------|-----------------------------|--------------------|---------------------|--------------------------|---------------|-----------|----------------|-------------|------------|---------------|----------------|------------------|----------------|-------|-----------------|---------------------------------------|----------------------------------|-----------------------------------|------------------|------------------------------|-----------------------------------|-----------------|---------------------------------|---|--------------------------------------|-------|-------------------|--------------------------|------|---------------------------|--|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (") | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| B66 | Double Goaf Loading | 119.5 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 23.7 | 15.2 | 90.0 | 6.5 | 6.0 | 43.7 | 360.2 | 640.2 | 7.9 | 5.1 | 5.07 | 0.781 | 0.781 | 18.521 | 5.31 | 1913 | 0.90 | 20 | A | G | | 2113 | | 11.17 | Yes | 17.43 | 6280 | 1.56 | 2.4E-03 | 1 in 388 |
| B67 | Tailgate Loading | 119.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 23.7 | 15.2 | 90.0 | 6.5 | 6.2 | 44.3 | 360.2 | 646.3 | 7.9 | 5.1 | 5.07 | 0.781 | 0.781 | 18.521 | 5.34 | 1923 | 0.90 | 20 | A | T | | 1803 | | 10.34 | Yes | 17.43 | 6280 | 1.69 | 5.8E-04 | 1 in 1999 |
| B68 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.8 | 43.9 | 390.0 | 695.4 | 5.0 | 8.7 | 5.00 | 1.268 | 1.172 | 17.575 | 5.35 | 2086 | 0.76 | 20 | A | G | | 3287 | | 13.78 | Yes | 14.74 | 5750 | 1.07 | 3.6E-01 | 1 in 3 |
| B69 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.8 | 43.9 | 390.0 | 695.4 | 5.0 | 8.7 | 5.00 | 1.268 | 1.172 | 17.575 | 5.35 | 2086 | 0.76 | 20 | A | G | | 3287 | | 13.78 | Yes | 14.74 | 5750 | 1.07 | 3.6E-01 | 1 in 3 |
| B70 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.6 | 43.6 | 390.0 | 691.1 | 5.0 | 8.7 | 5.00 | 1.268 | 1.172 | 17.575 | 5.32 | 2073 | 0.76 | 20 | A | G | | 3267 | | 13.69 | Yes | 14.74 | 5750 | 1.08 | 3.5E-01 | 1 in 3 |
| B71 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.7 | 43.7 | 390.0 | 693.2 | 5.0 | 8.7 | 5.00 | 1.268 | 1.172 | 17.575 | 5.33 | 2080 | 0.76 | 20 | A | G | | 3277 | | 13.74 | Yes | 14.74 | 5750 | 1.07 | 3.5E-01 | 1 in 3 |
| B72 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.7 | 43.7 | 390.0 | 693.2 | 5.0 | 8.7 | 5.00 | 1.268 | 1.172 | 17.575 | 5.33 | 2080 | 0.76 | 20 | A | G | | 3277 | | 13.74 | Yes | 14.74 | 5750 | 1.07 | 3.5E-01 | 1 in 3 |
| B73 | Rotated Panel / Double Goaf | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 15.0 | 26.0 | 90.0 | 6.2 | 6.9 | 44.1 | 390.0 | 697.5 | 5.0 | 8.7 | 5.00 | 1.268 | 1.172 | 17.575 | 5.37 | 2092 | 0.76 | 20 | A | G | | 3297 | | 13.82 | Yes | 14.74 | 5750 | 1.07 | 3.6E-01 | 1 in 3 |
| B74 | Double Goaf Loading | 118.2 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 24.3 | 14.5 | 90.0 | 6.5 | 6.3 | 45.0 | 352.4 | 640.6 | 8.1 | 4.8 | 4.83 | 0.747 | 0.747 | 18.162 | 5.37 | 1893 | 0.91 | 20 | A | G | | 2043 | | 11.17 | Yes | 17.56 | 6188 | 1.57 | 2.1E-03 | 1 in 452 |
| B75 | Double Goaf Loading | 118.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 24.1 | 14.5 | 90.0 | 6.5 | 6.8 | 46.4 | 349.5 | 651.8 | 8.0 | 4.8 | 4.83 | 0.751 | 0.751 | 18.106 | 5.50 | 1923 | 0.91 | 20 | A | G | | 2087 | | 11.47 | Yes | 17.43 | 6091 | 1.52 | 3.8E-03 | 1 in 235 |
| B76 | Maingate Loading | 117.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 25.4 | 14.6 | 90.0 | 6.5 | 6.3 | 44.4 | 370.8 | 666.7 | 8.5 | 4.9 | 4.87 | 0.730 | 0.730 | 18.542 | 5.26 | 1950 | 0.92 | 20 | A | M | | 1118 | | 8.27 | Yes | 18.34 | 6803 | 2.22 | 2.8E-07 | 1 in 1000000 |
| B77 | Rotated panel / Maingate Loading | 118.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 14.4 | 26.7 | 90.0 | 6.7 | 6.3 | 44.8 | 384.5 | 696.3 | 4.8 | 8.9 | 4.80 | 1.299 | 1.170 | 16.849 | 5.34 | 2054 | 0.76 | 20 | A | M | | 1477 | | 9.18 | No | 14.43 | 5548 | 1.57 | 2.1E-03 | 1 in 447 |
| B78 | Rotated panel / Maingate Loading | 119.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 14.3 | 26.3 | 90.0 | 6.6 | 6.3 | 44.8 | 376.1 | 681.3 | 4.8 | 8.8 | 4.77 | 1.296 | 1.165 | 16.656 | 5.39 | 2027 | 0.75 | 20 | A | M | | 1459 | | 9.27 | No | 14.35 | 5395 | 1.55 | 2.8E-03 | 1 in 332 |
| B79 | Rotated panel / Maingate Loading | 120.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 14.5 | 26.3 | 90.0 | 6.4 | 6.3 | 44.0 | 381.4 | 681.3 | 4.8 | 8.8 | 4.83 | 1.289 | 1.168 | 16.935 | 5.36 | 2044 | 0.75 | 20 | A | M | | 1464 | | 9.20 | No | 14.47 | 5517 | 1.57 | 2.1E-03 | 1 in 454 |
| B80 | Rotated panel / Maingate Loading | 121.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 14.5 | 26.3 | 90.0 | 6.7 | 6.3 | 44.8 | 381.4 | 691.1 | 4.8 | 8.8 | 4.83 | 1.289 | 1.168 | 16.935 | 5.48 | 2091 | 0.76 | 20 | A | M | | 1500 | | 9.42 | No | 14.47 | 5517 | 1.54 | 3.1E-03 | 1 in 290 |
| B81 | Rotated panel / Maingate Loading | 122.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 14.5 | 26.3 | 90.0 | 6.6 | 6.3 | 44.6 | 381.4 | 687.9 | 4.8 | 8.8 | 4.83 | 1.289 | 1.168 | 16.935 | 5.50 | 2098 | 0.75 | 20 | A | M | | 1504 | | 9.45 | No | 14.47 | 5517 | 1.53 | 3.3E-03 | 1 in 273 |
| B82 | Rotated panel / Maingate Loading | 123.0 | 45.0 | 3.0 | 3.0 | 3.0 | 25 | 14.5 | 26.3 | 90.0 | 6.6 | 6.3 | 44.6 | 381.4 | 687.9 | 4.8 | 8.8 | 4.83 | 1.289 | 1.168 | 16.935 | 5.55 | 2115 | 0.75 | 20 | A | M | | 1517 | | 9.52 | No | 14.47 | 5517 | 1.52 | 3.8E-03 | 1 in 235 |
| B83 | | 113.0 | | 3.0 | 3.0 | 3.0 | 25 | 12.6 | 8.9 | 90.0 | 6.4 | 7.2 | 63.3 | 112.1 | 305.9 | 4.2 | 3.0 | 2.97 | 0.828 | 0.927 | 11.683 | 7.71 | 864 | 0.72 | 21 | A | M | | 105 | | 8.64 | No | 11.97 | 1343 | 1.38 | 1.8E-02 | 1 in 50 |
| B84 | | 113.5 | | 3.0 | 3.0 | 3.0 | 25 | 13.0 | 8.6 | 90.0 | 6.6 | 7.2 | 63.9 | 111.8 | 309.7 | 4.3 | 2.9 | 2.87 | 0.796 | 0.904 | 11.748 | 7.86 | 879 | 0.74 | 22 | A | M | | 109 | | 8.83 | No | 12.01 | 1342 | 1.36 | 2.4E-02 | 1 in 38 |
| B85 | | 113.8 | | 3.0 | 3.0 | 3.0 | 25 | 12.8 | 9.0 | 90.0 | 6.4 | 6.3 | 60.8 | 115.2 | 293.8 | 4.3 | 3.0 | 3.00 | 0.826 | 0.922 | 11.806 | 7.25 | 836 | 0.73 | 23 | A | M | | 101 | | 8.13 | No | 12.04 | 1387 | 1.48 | 6.0E-03 | 1 in 147 |

Table A.6: Pillar Stability Analysis

Run 2A: Additional Abutment load to western pillars beneath site

Key to Colour Coding of Factors of Safety / Width: Height Ratios

Project: Lake Macquarie Private Hospital Northern Expansion
Location: O'Brien Street, Gateshead
Analysis Assumptions: NSW Pillar formula
Project Number: 16471.21

Client: Akalan Projects
Date: 18/10/16
Sheet: 2
Calculations by JAW

4.50

Greater than 3.0

2.40

Between 2.2 and 3.0

2.10

Between 1.8 and 2.2

1.70

Between 1.5 and 1.8

1.20

Less than 1.5

Indicating Pillar Located within Project Angle of Draw

Indicating Pillar Located beneath site

| Analysis Id: | Comment | Depth | Panel Width/Span (Longwall only) | Seam Thickness | Working Section | Pillar Height Section | Unit Weight γ (kN/m³) | Pillar Details | | | Adway Det | | Extract. Ratio | Pillar Area | Total Area | w1/ Height Ratio | w2/H Height Ratio | Width/ Height Ratio | Width Modifier | | | Pillar Stress (Tributary) (MPa) | Pillar Load (Tributary) MN | Proportion Abutment transfer R | Abutment Angle ° | Abut (A) Yield (Y) (?) | Abutment Loading Type M,T,G | Shed Load MN | Abutment Load Received MN | Pillar Stress ("Yield") σ _y = 0.7 | Pillar Stress ("Abut") (MPa) | Squat | Power Law | | | | Probability of Failure NSW Power Formulae |
|--------------|---------------------|-------|-------------------------------------|----------------|-----------------|-----------------------|-----------------------------|--------------------|---------------------|-----------------------|-----------|-----------|----------------|-------------|------------|---------------------|----------------------|------------------------|----------------|-------|-----------------------|---------------------------------------|----------------------------------|-----------------------------------|------------------|------------------------------|-----------------------------------|-----------------|---------------------------------|---|------------------------------------|-------|-------------------|--------------------------|---------|------------------------|--|
| | | | | | | | | Width w1 (m) | Length w2 (m) | Internal Angle (") | b1 (m) | b2 (m) | | | | | | | Θ ₀ | Θ | wΘ Effective Width | | | | | | | | | | | | Strength (MPa) | "Ultimate" Load MN | FoS | Probability of Failure | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A6 | | 123.6 | | 2.4 | 2.4 | 2.4 | 25 | 17.7 | 26.9 | 90.0 | 4.8 | 5.3 | 34.3 | 476.1 | 724.5 | 7.4 | 11.2 | 7.38 | 1.206 | 1.206 | 21.351 | 4.70 | 2238 | 0.78 | 20 | | | | | | Yes | 21.66 | 10314 | 4.61 | 3.2E-22 | 1 in 1000000 | |
| A7 | | 123.1 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 26.5 | 90.0 | 5.2 | 5.4 | 36.2 | 455.8 | 714.6 | 7.2 | 11.0 | 7.17 | 1.213 | 1.213 | 20.860 | 4.82 | 2199 | 0.78 | 20 | | | | | | Yes | 21.08 | 9606 | 4.37 | 1.0E-20 | 1 in 1000000 | |
| A8 | | 122.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.7 | 26.5 | 90.0 | 5.4 | 5.8 | 38.0 | 442.6 | 713.8 | 7.0 | 11.0 | 6.96 | 1.227 | 1.227 | 20.488 | 4.95 | 2189 | 0.77 | 20 | | | | | | Yes | 20.58 | 9106 | 4.16 | 2.0E-19 | 1 in 1000000 | |
| A9 | | 121.4 | | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 27.6 | 90.0 | 5.0 | 5.3 | 35.2 | 469.2 | 723.8 | 7.1 | 11.5 | 7.08 | 1.238 | 1.238 | 21.040 | 4.68 | 2196 | 0.77 | 20 | | | | | | Yes | 21.04 | 9872 | 4.50 | 1.6E-21 | 1 in 1000000 | |
| A68 | Maingate Loading | 122.1 | 90.0 | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 35.4 | 90.0 | 5.3 | 5.1 | 34.3 | 566.4 | 862.7 | 6.7 | 14.8 | 6.67 | 1.377 | 1.377 | 22.039 | 4.65 | 2633 | 0.76 | 20 | A | M | | 2079 | | 8.32 | Yes | 20.96 | 11869 | 2.52 | 3.6E-09 | 1 in 1000000 |
| A69 | | 122.1 | | 2.4 | 2.4 | 2.4 | 25 | 17.4 | 19.4 | 90.0 | 5.6 | 6.5 | 43.3 | 337.6 | 595.7 | 7.3 | 8.1 | 7.25 | 1.054 | 1.054 | 18.346 | 5.39 | 1818 | 0.79 | 20 | | | | | | Yes | 19.86 | 6704 | 3.69 | 1.8E-16 | 1 in 1000000 | |
| A70 | | 122.1 | | 2.4 | 2.4 | 2.4 | 25 | 16.9 | 19.2 | 90.0 | 5.4 | 6.5 | 43.4 | 324.5 | 573.1 | 7.0 | 8.0 | 7.04 | 1.064 | 1.064 | 17.977 | 5.39 | 1749 | 0.78 | 20 | | | | | | Yes | 19.36 | 6282 | 3.59 | 7.2E-16 | 1 in 1000000 | |
| A71 | | 121.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.9 | 19.2 | 90.0 | 4.9 | 6.5 | 42.1 | 324.5 | 560.3 | 7.0 | 8.0 | 7.04 | 1.064 | 1.064 | 17.977 | 5.23 | 1698 | 0.77 | 20 | | | | | | Yes | 19.36 | 6282 | 3.70 | 1.5E-16 | 1 in 1000000 | |
| A72 | | 120.6 | | 2.4 | 2.4 | 2.4 | 25 | 16.9 | 19.2 | 90.0 | 5.0 | 6.5 | 42.3 | 324.5 | 562.8 | 7.0 | 8.0 | 7.04 | 1.064 | 1.064 | 17.977 | 5.23 | 1697 | 0.77 | 20 | | | | | | Yes | 19.36 | 6282 | 3.70 | 1.5E-16 | 1 in 1000000 | |
| A73 | Maingate Loading | 124.2 | 90.0 | 2.4 | 2.4 | 2.4 | 25 | 16.5 | 31.9 | 90.0 | 5.3 | 4.7 | 34.0 | 526.4 | 797.9 | 6.9 | 13.3 | 6.88 | 1.318 | 1.318 | 21.750 | 4.71 | 2477 | 0.76 | 20 | A | M | | 2190 | | 8.87 | Yes | 21.09 | 11103 | 2.38 | 2.7E-08 | 1 in 1000000 |
| A74 | | 122.3 | | 2.4 | 2.4 | 2.4 | 25 | 16.4 | 17.4 | 90.0 | 5.5 | 5.2 | 42.3 | 285.4 | 494.9 | 6.8 | 7.3 | 6.83 | 1.030 | 1.030 | 16.885 | 5.30 | 1513 | 0.77 | 20 | | | | | | Yes | 18.49 | 5276 | 3.49 | 3.2E-15 | 1 in 1000000 | |
| A75 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 16.6 | 16.9 | 90.0 | 5.2 | 5.4 | 42.3 | 280.5 | 486.1 | 6.9 | 7.0 | 6.92 | 1.009 | 1.009 | 16.749 | 5.28 | 1480 | 0.77 | 20 | | | | | | Yes | 18.51 | 5194 | 3.51 | 2.4E-15 | 1 in 1000000 | |
| A76 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 16.6 | 17.1 | 90.0 | 4.8 | 5.7 | 41.8 | 283.9 | 487.9 | 6.9 | 7.1 | 6.92 | 1.015 | 1.015 | 16.846 | 5.23 | 1486 | 0.76 | 20 | | | | | | Yes | 18.57 | 5271 | 3.55 | 1.3E-15 | 1 in 1000000 | |
| A77 | | 121.2 | | 2.4 | 2.4 | 2.4 | 25 | 16.6 | 17.0 | 90.0 | 5.0 | 5.0 | 40.6 | 282.2 | 475.2 | 6.9 | 7.1 | 6.92 | 1.012 | 1.012 | 16.798 | 5.10 | 1440 | 0.76 | 20 | | | | | | Yes | 18.54 | 5233 | 3.63 | 3.9E-16 | 1 in 1000000 | |
| A78 | Maingate Loading | 121.8 | 90.0 | 2.4 | 2.4 | 2.4 | 25 | 16.5 | 29.9 | 90.0 | 5.3 | 4.4 | 34.0 | 493.4 | 747.7 | 6.9 | 12.5 | 6.88 | 1.289 | 1.289 | 21.265 | 4.62 | 2277 | 0.77 | 20 | A | M | | 1777 | | 8.22 | Yes | 20.85 | 10288 | 2.54 | 2.7E-09 | 1 in 1000000 |
| A79 | | 121.9 | | 2.4 | 2.4 | 2.4 | 25 | 16.2 | 17.6 | 90.0 | 6.6 | 5.3 | 45.4 | 285.1 | 522.1 | 6.8 | 7.3 | 6.75 | 1.041 | 1.041 | 16.871 | 5.58 | 1591 | 0.79 | 20 | | | | | | Yes | 18.38 | 5241 | 3.29 | 5.2E-14 | 1 in 1000000 | |
| A81 | | 121.8 | | 2.4 | 2.4 | 2.4 | 25 | 15.4 | 17.5 | 90.0 | 5.2 | 5.1 | 42.1 | 269.5 | 465.6 | 6.4 | 7.3 | 6.42 | 1.064 | 1.064 | 16.383 | 5.26 | 1418 | 0.74 | 20 | | | | | | Yes | 17.75 | 4785 | 3.38 | 1.6E-14 | 1 in 1000000 | |
| B1 | | 121.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 15.9 | 90.0 | 5.4 | 6.7 | 46.5 | 273.5 | 510.8 | 7.2 | 6.6 | 6.63 | 0.961 | 0.961 | 16.524 | 5.66 | 1548 | 0.78 | 20 | | | | | | Yes | 18.71 | 5118 | 3.31 | 4.3E-14 | 1 in 1000000 | |
| B2 | | 120.6 | | 2.4 | 2.4 | 2.4 | 25 | 16.8 | 15.9 | 90.0 | 5.4 | 6.7 | 46.8 | 267.1 | 501.7 | 7.0 | 6.6 | 6.63 | 0.972 | 0.972 | 16.338 | 5.66 | 1513 | 0.78 | 20 | | | | | | Yes | 18.39 | 4911 | 3.25 | 1.0E-13 | 1 in 1000000 | |
| B3 | | 120.1 | | 2.4 | 2.4 | 2.4 | 25 | 16.0 | 15.4 | 90.0 | 5.4 | 6.7 | 47.9 | 246.4 | 472.9 | 6.7 | 6.4 | 6.42 | 0.981 | 0.981 | 15.694 | 5.76 | 1420 | 0.76 | 20 | | | | | | Yes | 17.62 | 4342 | 3.06 | 1.5E-12 | 1 in 1000000 | |
| B4 | | 120.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 15.7 | 90.0 | 5.4 | 5.0 | 42.2 | 271.6 | 469.9 | 7.2 | 6.5 | 6.54 | 0.952 | 0.952 | 16.461 | 5.20 | 1412 | 0.79 | 20 | | | | | | Yes | 18.73 | 5088 | 3.60 | 6.0E-16 | 1 in 1000000 | |
| B5 | | 119.6 | | 2.4 | 2.4 | 2.4 | 25 | 16.9 | 15.8 | 90.0 | 5.4 | 5.0 | 42.4 | 267.0 | 463.8 | 7.0 | 6.6 | 6.58 | 0.966 | 0.966 | 16.331 | 5.19 | 1387 | 0.78 | 20 | | | | | | Yes | 18.44 | 4923 | 3.55 | 1.3E-15 | 1 in 1000000 | |
| B6 | | 119.2 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 16.1 | 90.0 | 5.4 | 5.0 | 41.8 | 278.5 | 479.0 | 7.2 | 6.7 | 6.71 | 0.964 | 0.964 | 16.678 | 5.12 | 1427 | 0.79 | 20 | | | | | | Yes | 18.86 | 5253 | 3.68 | 2.0E-16 | 1 in 1000000 | |
| B7 | | 118.6 | | 2.4 | 2.4 | 2.4 | 25 | 18.3 | 24.6 | 90.0 | 5.4 | 5.2 | 36.3 | 450.2 | 706.3 | 7.6 | 10.3 | 7.63 | 1.147 | 1.147 | 20.987 | 4.65 | 2094 | 0.81 | 20 | | | | | | Yes | 21.90 | 9860 | 4.71 | 7.5E-23 | 1 in 1000000 | |
| B8 | | 119.0 | | 2.4 | 2.4 | 2.4 | 25 | 18.1 | 24.9 | 90.0 | 5.4 | 5.2 | 36.3 | 450.7 | 707.4 | 7.5 | 10.4 | 7.54 | 1.158 | 1.158 | 20.962 | 4.67 | 2104 | 0.80 | 20 | | | | | | Yes | 21.74 | 9799 | 4.66 | 1.6E-22 | 1 in 1000000 | |
| B9 | | 120.0 | | 2.4 | 2.4 | 2.4 | 25 | 18.0 | 24.9 | 90.0 | 5.4 | 5.2 | 36.4 | 448.2 | 704.3 | 7.5 | 10.4 | 7.50 | 1.161 | 1.161 | 20.895 | 4.71 | 2113 | 0.80 | 20 | | | | | | Yes | 21.64 | 9697 | 4.59 | 4.2E-22 | 1 in 1000000 | |
| B10 | | 121.3 | | 2.4 | 2.4 | 2.4 | 25 | 18.8 | 24.7 | 90.0 | 5.4 | 5.2 | 35.8 | 464.4 | 723.6 | 7.8 | 10.3 | 7.83 | 1.136 | 1.136 | 21.350 | 4.73 | 2194 | 0.81 | 20 | | | | | | Yes | 22.48 | 10439 | 4.76 | 3.7E-23 | 1 in 1000000 | |
| B11 | Maingate Loading | 121.8 | 90.0 | 2.4 | 2.4 | 2.4 | 25 | 15.2 | 40.0 | 90.0 | 6.1 | 4.8 | 36.3 | 608.0 | 954.2 | 6.3 | 16.7 | 6.33 | 1.449 | 1.449 | 22.029 | 4.78 | 2906 | 0.76 | 20 | A | M | | 2290 | | 8.55 | Yes | 20.56 | 12498 | 2.41 | 1.8E-08 | 1 in 1000000 |
| B12 | | 121.0 | | 2.4 | 2.4 | 2.4 | 25 | 18.6 | 19.0 | 90.0 | 5.4 | 5.2 | 39.2 | 353.4 | 580.8 | 7.8 | 7.9 | 7.75 | 1.011 | 1.011 | 18.798 | 4.97 | 1757 | 0.81 | 20 | | | | | | Yes | 20.92 | 7393 | 4.21 | 1.0E-19 | 1 in 1000000 | |
| B13 | | 119.7 | | 2.4 | 2.4 | 2.4 | 25 | 16.8 | 18.7 | 90.0 | 5.4 | 5.2 | 40.8 | 314.2 | 530.6 | 7.0 | 7.8 | 7.00 | 1.054 | 1.054 | 17.699 | 5.05 | 1588 | 0.78 | 20 | | | | | | Yes | 19.15 | 6017 | 3.79 | 4.1E-17 | 1 in 1000000 | |
| B14 | | 118.4 | | 2.4 | 2.4 | 2.4 | 25 | 17.2 | 18.7 | 90.0 | 5.4 | 5.2 | 40.5 | 321.6 | 540.1 | 7.2 | 7.8 | 7.17 | 1.042 | 1.042 | 17.919 | 4.97 | 1599 | 0.79 | 20 | | | | | | Yes | 19.50 | 6273 | 3.92 | 6.0E-18 | 1 in 1000000 | |
| B15 | | 117.7 | | 2.4 | 2.4 | 2.4 | 25 | 17.3 | 19.5 | 90.0 | 5.4 | 5.2 | 39.8 | 337.4 | 560.7 | 7.2 | 8.1 | 7.21 | 1.060 | 1.060 | 18.334 | 4.89 | 1650 | 0.79 | 20 | | | | | | Yes | 19.79 | 6677 | 4.05 | 1.0E-18 | 1 in 1000000 | |
| B41 | Double Goaf Loading | 121.0 | 45.0 | 2.4 | 2.4 | 2.4 | 25 | 17.0 | 37.8 | 90.0 | 5.4 | 5.0 | 33.0 | 642.6 | 958.7 | 7.1 | 15.8 | 7.08 | 1.380 | 1.380 | 23.453 | 4.51 | 2900 | 0.78 | 20 | A | G | | 4338 | | 11.26 | Yes | | | | | |



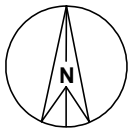
LEGEND:

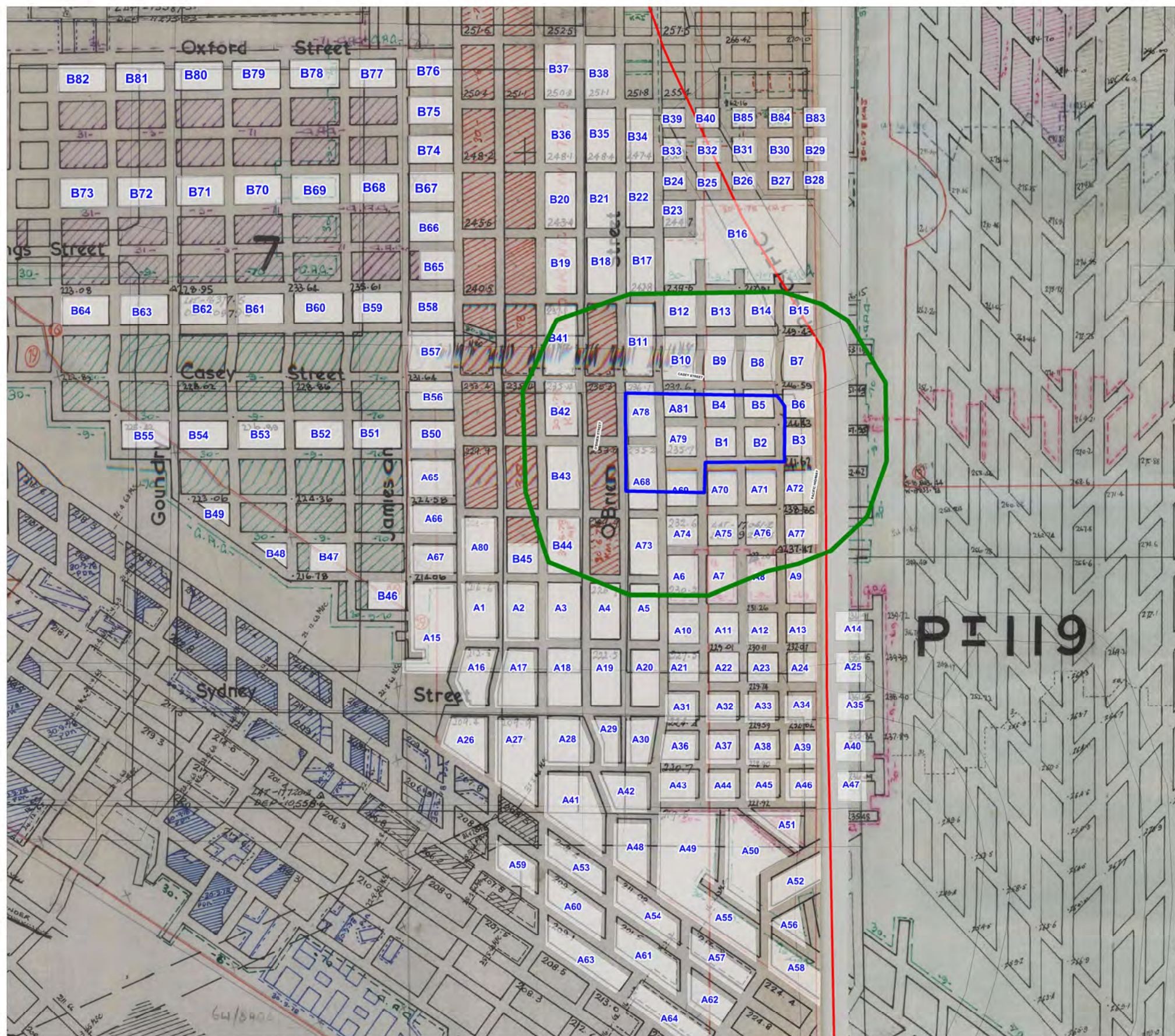


SITE EXTENTS



ANGLE OF DRAW (MINE WORKINGS)





LEGEND:



SITE EXTENTS

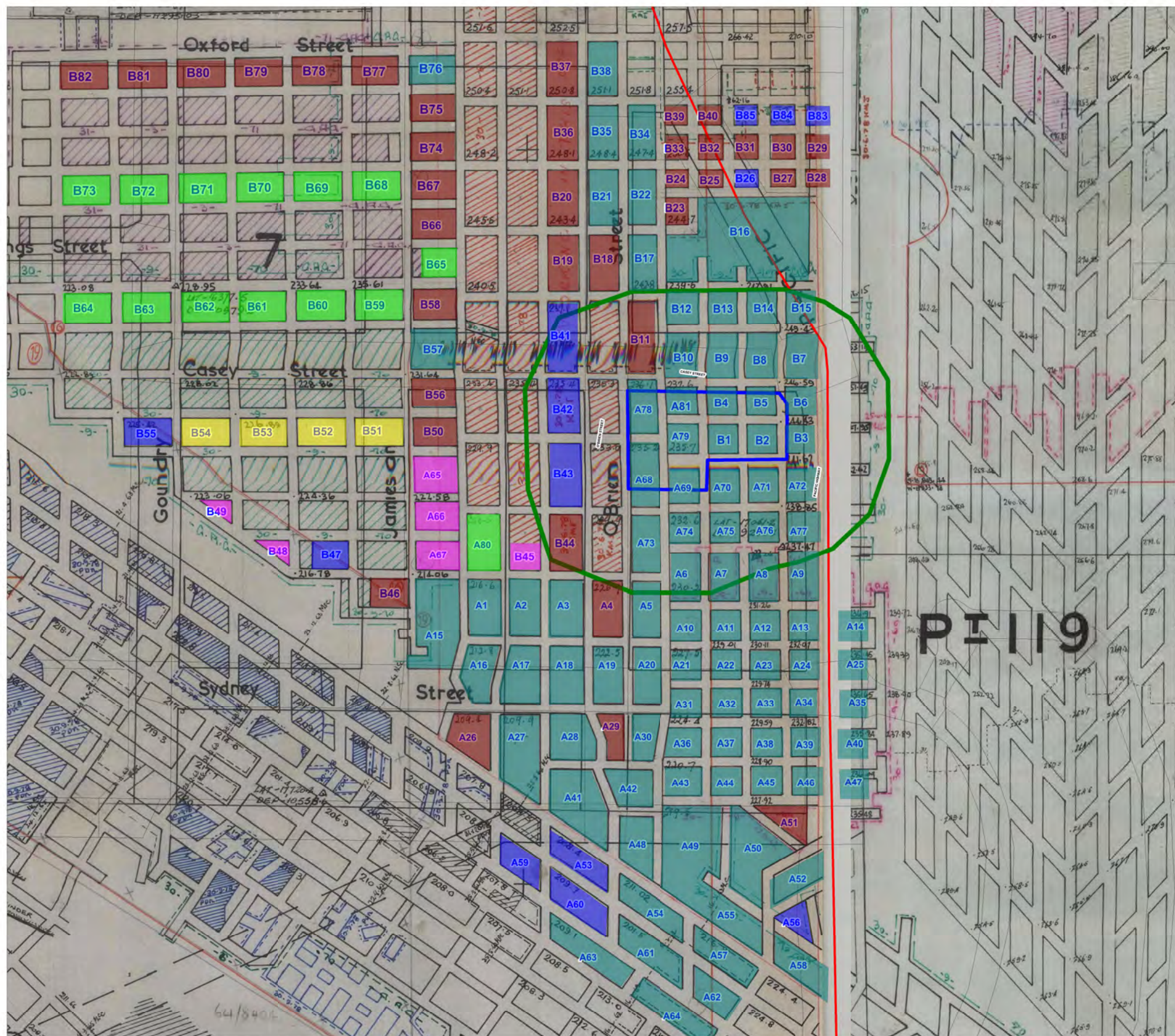


ANGLE OF DRAW (MINE WORKINGS)



Location of Pillar and
Numbering Used in Analysis

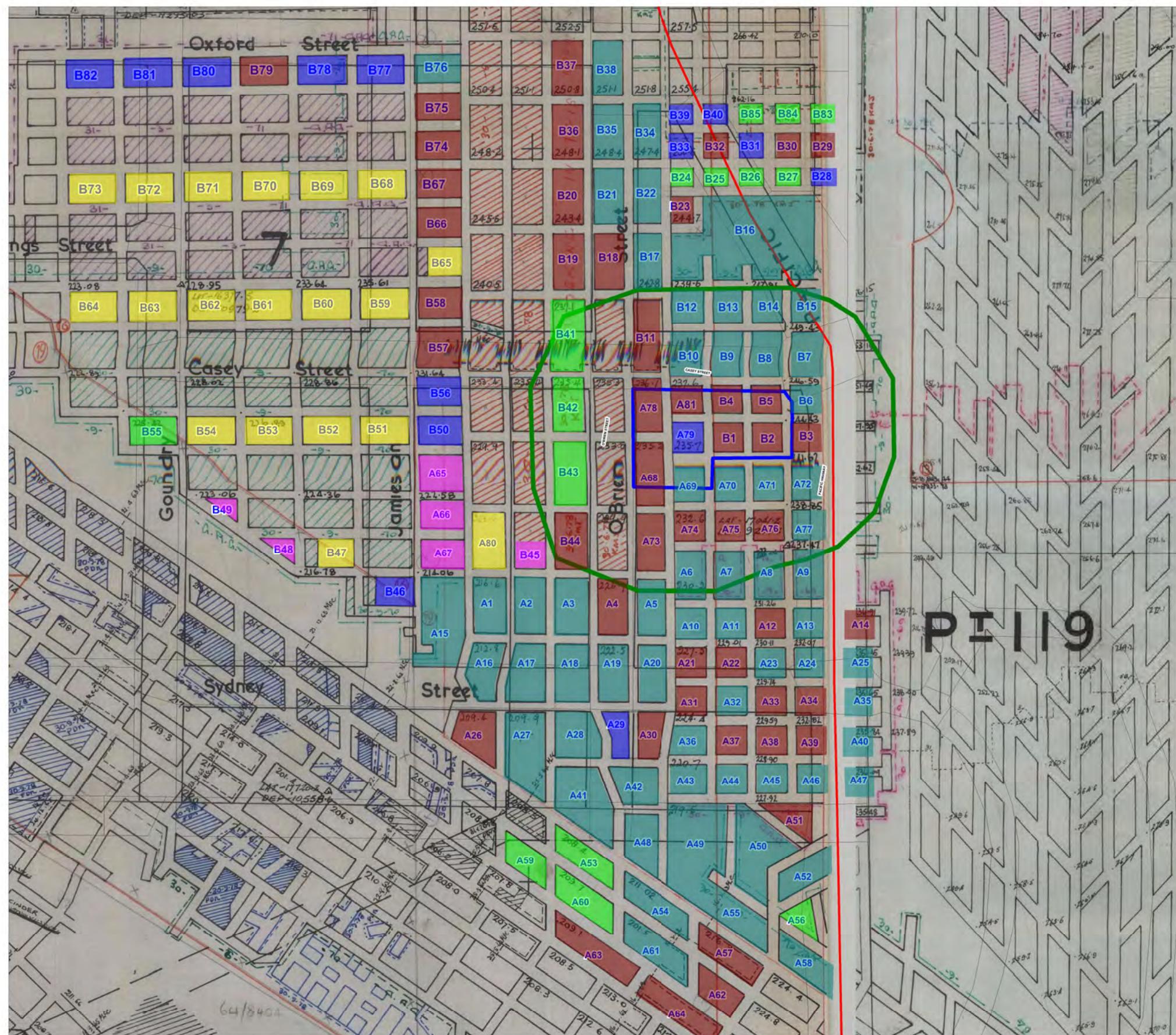




LEGEND:

- SITE EXTENTS
- ANGLE OF DRAW (MINE WORKINGS)
- B5 Location of Pillar and Numbering Used in Analysis
- Pillar Factor of Safety Greater than 3.0
- Pillar Factor of Safety Between 2.2 and 3.0
- Pillar Factor of Safety Between 1.8 and 2.2
- Pillar Factor of Safety Between 1.5 and 1.8
- Pillar Factor of Safety Less than 1.5
- Pillars Assumed Crushed

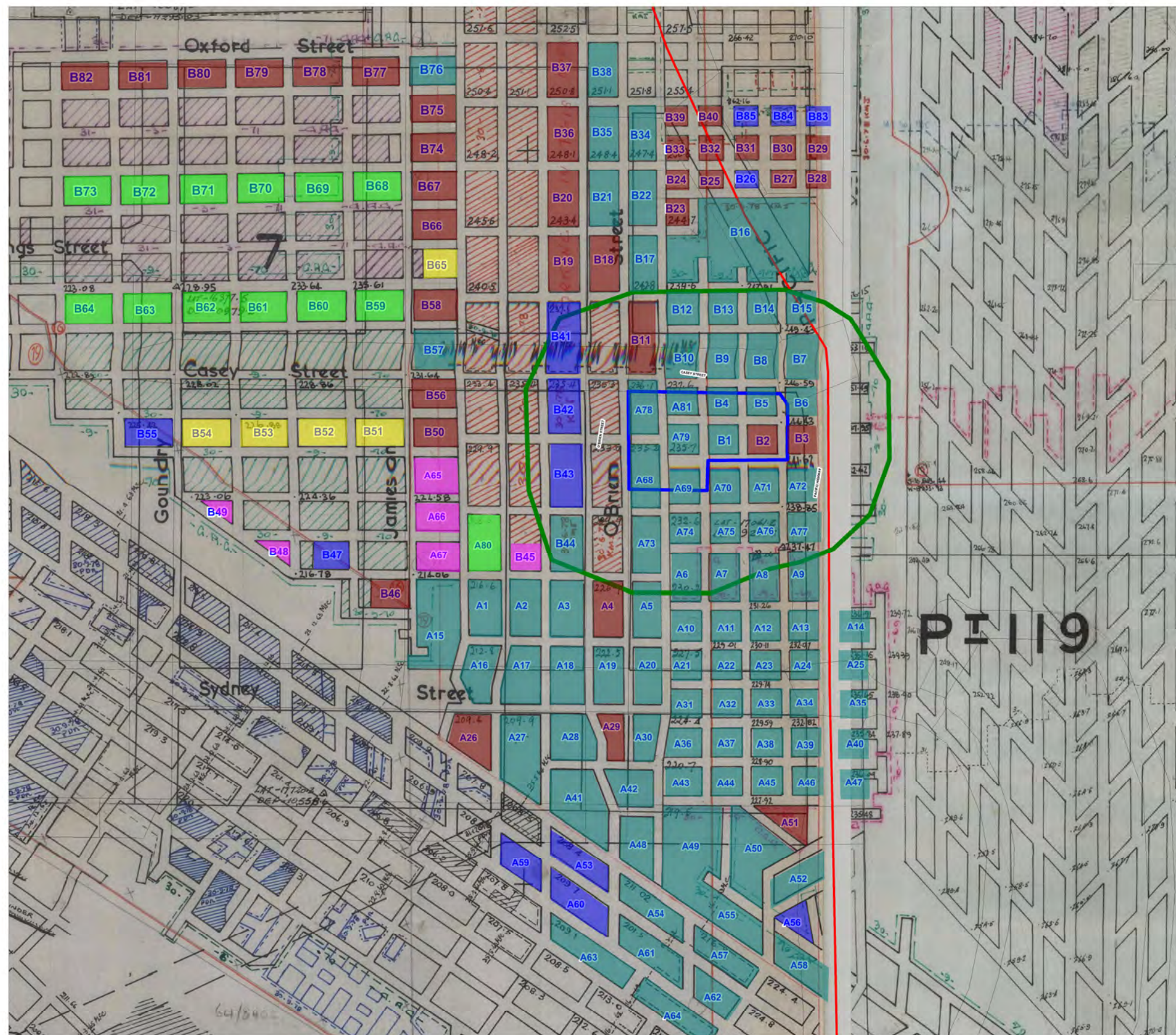




LEGEND:

- SITE EXTENTS
- ANGLE OF DRAW (MINE WORKINGS)
- B5** Location of Pillar and Numbering Used in Analysis
- Pillar Factor of Safety Greater than 3.0
- Pillar Factor of Safety Between 2.2 and 3.0
- Pillar Factor of Safety Between 1.8 and 2.2
- Pillar Factor of Safety Between 1.5 and 1.8
- Pillar Factor of Safety Less than 1.5
- Pillars Assumed Crushed





LEGEND:

- SITE EXTENTS
- ANGLE OF DRAW (MINE WORKINGS)
- B5 Location of Pillar and Numbering Used in Analysis
- Pillar Factor of Safety Greater than 3.0
- Pillar Factor of Safety Between 2.2 and 3.0
- Pillar Factor of Safety Between 1.8 and 2.2
- Pillar Factor of Safety Between 1.5 and 1.8
- Pillar Factor of Safety Less than 1.5
- Pillars Assumed Crushed



Attachment 5: High-level social and economic benefits assessment

Lake Macquarie Private Hospital Redevelopment

**High level assessment of benefits from expansion of
services at Lake Macquarie Private Hospital**

11 October 2021

Disclaimer

This report has been prepared for Ramsay Health Care Limited for use and benefit in accordance with and for the purpose set out in our engagement letter with Ramsay Health Care Limited dated 21 September 2021. In doing so, we acted exclusively in Ramsay Health Care Limited interests.

We accept no responsibility, duty or liability:

- to anyone other than Ramsay Health Care Limited in connection with this report
- to Ramsay Health Care Limited for the consequences of using or relying on it for a purpose other than that referred to above.

We make no representation concerning the appropriateness of this report for anyone other than Ramsay Health Care Limited. If anyone other than Ramsay Health Care Limited chooses to use or rely on it they do so at their own risk.

This disclaimer applies:

- to the maximum extent permitted by law and, without limitation, to liability arising in negligence or under statute; and
- even if we consent to anyone other than Ramsay Health Care Limited receiving or using this report.

Liability limited by a scheme approved under Professional Standards Legislation.

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1 Background and purpose

1.1 Background

Since 1973, Lake Macquarie Private Hospital has provided private health care services to the communities of Newcastle and Lake Macquarie, as well as the broader referral region of Hunter – New England.

Lake Macquarie Private Hospital is a 187-bed medical and advanced surgical hospital owned and operated by Ramsay Health Care Limited. Together with Warners Bay Private Hospital (also owned and operated by Ramsay Health Care Limited), Lake Macquarie Private Hospital treats 35,000 patients a year. It provides specialty disciplines including cardiovascular care, orthopaedics, oncology and rehabilitation. It is also home to the Hunter Cancer Centre, the Hunter Region's only comprehensive private oncology service providing Medical Oncology, Radiation Oncology, Research, Support Services and Education.

Figure 1 - Lake Macquarie Private Hospital



Lake Macquarie Private Hospital was redeveloped in 2015 to include the Hunter Region's first private Emergency Department. It treats more than 12,000 patients a year. The Emergency Department has six beds including a state-of-the-art resuscitation room, triage room and procedure room. Other services include intensive care unit, cardiac theatre, recovery room, coronary care unit and cardiac catheterisation laboratories.

1.2 Lake Macquarie Private Hospital Redevelopment

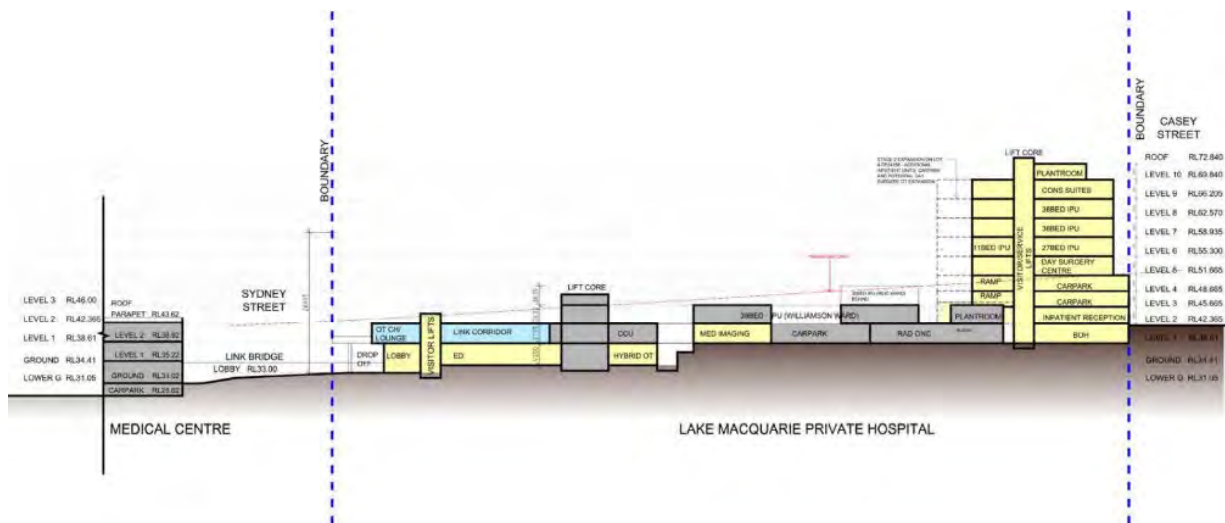
Ramsay Health Care Limited are currently investigating the redevelopment of Lake Macquarie Private Hospital to increase capacity and meet the private health needs of the local communities. The redevelopment will be completed in five stages, with a total capital expenditure of approximately \$120 million. Stage 1-4 of the redevelopment is proposed to be completed by 2025 and includes:

- A net increase of 57 beds, bringing total beds to 243
- An additional six (6) emergency department bays
- An additional three (3) inpatient theatres, with one (1) being a hybrid theatre
- An additional three (3) day surgery theatres
- Consulting suites
- An additional eight (8) day oncology chairs
- A pharmacy.

The redevelopment will also include compliance upgrades to meet current National Safety and Quality Health Service (NSQHS) Standards and Australasian Health Facility Guidelines (AusHFG), including:

- A new central sterilising unit
- The relocation of the medical imaging onsite, which is currently housed in the medical centre opposite the hospital
- A fire and smoke control upgrade
- A power supply upgrade
- An emergency generator upgrade.

Figure 2 - Concept design for Lake Macquarie Private Hospital Redevelopment



1.3 Purpose of this assessment

PricewaterhouseCoopers Consulting (Australia) Pty Ltd (PwC) were engaged to provide high level guidance on the social and economic benefits associated with the redevelopment of the Lake Macquarie Private Hospital. This was carried out through a qualitative rapid desktop appraisal.

A number of assumptions and limitations underpin this benefit assessment:

- Future expansion activity is contingent on Ramsay Health Care Limited's application to the Lake Macquarie City Council for planning approvals to increase in the allowable development height for Lake Macquarie Private Hospital.
- The scope of the redevelopment is based on supply and demand projections that have not been viewed or verified by PwC. No assessment of the service need or demand for additional beds has been conducted by PwC. All benefits are contingent on current and future demand for services at Lake Macquarie Private Hospital.
- No analysis was performed on alternative options or scenarios in relation to service expansion, local service provision or alternative investments / divestments.
- Benefits are assessed in a qualitative manner, or where possible some metrics were quantified. No assessment of value for money or comparison of benefits to expected costs was made as part of this assessment.

2 Social and economic benefits

2.1 Beneficiaries of the Lake Macquarie Private Hospital Redevelopment

The redevelopment of Lake Macquarie Private Hospital has the potential to deliver a range of benefits to patients and their families and carers, staff of Lake Macquarie Private Hospital, business and industry, the broader NSW community and NSW Government. The beneficiaries of the redevelopment are presented in Figure 3.

Figure 3 - Potential beneficiaries of the Lake Macquarie Private Hospital Redevelopment



2.2 Benefit summary

Benefits of the redevelopment of Lake Macquarie Private Hospital are expected to include increased health and wellbeing for patients, access to health care closer to home, improved safety and efficiency, increased resilience and economic benefits of additional local employment. These are explored further below, including identification of expected beneficiaries.

Health and wellbeing benefits for patients



The Lake Macquarie Private Hospital Redevelopment has the potential to improve patient health and wellbeing through increased capacity in inpatient theatres, day theatres, inpatient beds, consulting suites and oncology chairs.

In 2021, Lake Macquarie Private Hospital experienced 22,207 inpatient and day patient admissions, 5,000 day surgery treatments and 13,008 emergency department attendances. Inpatient bed utilisation ranges from 80-90% on weekdays (average 72% total) and theatre utilisation on average is 80% (at peak times over 100%).

The population for Lake Macquarie Local Government Area (LGA) is expected to increase from 202,350 residents in 2016 to 232,700 in 2041 (15% increase).¹ Inpatient and day patient admissions are expected to grow to 30,970 (additional capacity to approximately 9,300 or 30%) and emergency department attendances are expected to grow to 19,245. In absence of redevelopment at Lake Macquarie Private Hospital, this projected activity would not be able to be met within the existing facility.

Expansion of capacity at Lake Macquarie Private Hospital will assist in meeting the growing health care demand in the Hunter-New England region. Failing to meet the growing health service demand would have a detrimental impact on patients' health and wellbeing arising from delay in access to healthcare or bed blockages. Waiting for access to health care mainly involves a prolonged period of decreased health and an affected psychological and social life of the patient in waiting. Provision of additional inpatient theatres, day theatres, inpatient beds and consulting suites will provide greater capacity in the private health system and reduce delays in accessing surgical or medical care, reduce bed block, and therefore improve the health and wellbeing of patients.

¹ NSW Department of Planning, Industry and Environment (2020), Lake Macquarie City Council, 2019 NSW Population Projections, www.planning.nsw.gov.au

In addition, the redevelopment will provide enhanced choice for residents in the Hunter-New England Region, with greater choice over public and private health care options.

Provision of an additional eight oncology chairs, in particular, will improve the health and wellbeing of oncology patients. Cancer is a major cause of illness in Australia and has a substantial social and economic impact on individuals, families and the community. Cancer as a disease group was the leading cause of burden in Australia in 2011, accounting for 19% of the total disease burden². Increased capacity in oncology at Lake Macquarie Private Hospital will reduce delays in access to care and provide care closer to home for cancer patients, improving health and wellbeing outcomes.

By increasing capacity in the health system in the Hunter-New England region, Lake Macquarie Private Hospital redevelopment will also improve health and wellbeing outcomes of public hospital patients. Where there is less pressure on the public health system, through patients receiving health care in the private system, patients of the public health system will experience reduced delays in access to health care. While John Hunter Hospital, the principal referral centre and tertiary public hospital for the Hunter-New England Region, is currently being redeveloped to provide additional inpatient beds, theatres and expanded emergency department, additional capacity will still be required within the public and private health network to meet the future health care needs of the region. In addition, increased capacity in the public health system has flow-on implications to the private health system, increasing demand for private health services.

Access to health care closer to home



Where future demand for healthcare services cannot be met at Lake Macquarie Private Hospital, patients may need to access health care within the public system, or at an alternative private service further away from patients' homes.

In the absence of the redevelopment, it is expected that patients would be required to travel to surrounding hospitals (public or alternative private hospitals) to receive treatment, most commonly by car. At times where theatres are at capacity, patients currently have to travel to other private hospitals. As demand increases for services at Lake Macquarie Private Hospital, in absence of redevelopment, a growing number of patients will need to travel to other private hospitals to receive care. As a result, a direct benefit of the redevelopment is the reduced travel costs (both in terms of time saved and resources used) incurred by patients who would no longer be required to travel elsewhere for treatment. Benefits may also arise to families, carers and visitors to patients that do not have to travel additional distances to support or care for patients.

Improved safety and efficiency



The redevelopment of Lake Macquarie Private Hospital will deliver a new central sterilising unit, ensuring that all reusable surgical products and instruments are cleaned and sterilised in accordance with national standards. Proper sterilisation of surgical equipment is vital to the safety of patients and in reducing the risk of microbial contamination and transmission of disease. A new central sterilising unit at Lake Macquarie Private Hospital will support the delivery of quality patient care and reduced risk of hospital surgical infections.

In addition, the redevelopment of Lake Macquarie Private Hospital will improve efficiency and delivery of health care at Lake Macquarie Private Hospital through the new pharmacy and the relocation of the medical imaging onsite, which is currently housed in the medical centre opposite the hospital. Access to an onsite pharmacy has the potential to improve pharmaceutical care for patients and ensure they have access to pharmaceuticals when required, including post-hospital requirements.

The relocation of the medical imaging onsite will reduce the time and cost associated with the current requirement for vehicle transfers to offsite medical imaging. Onsite access to medical imaging will ensure timely access to care through faster diagnoses and improve staff efficiency and patient flows.

² Australian Institute of Health and Welfare (2020), Cancer Overview, [cited at www.aihw.gov.au, published 14 December 2020, viewed 27 September 2021]

Onsite car parking will also provide greater safety and efficiency for patients, staff and visitors. The provision of car parking onsite eliminates the need for patients, staff and visitors to cross the road to access Lake Macquarie Private Hospital, reducing the safety risks and improving accessibility.

Increased resilience



Increased resilience through a power supply upgrade and an emergency generator will be delivered through the redevelopment. The upgrades will increase power supply capacity to support increased demand for services and will be designed for service continuity during events such as emergencies and power outages.

A new emergency generator ensures that during an event, emergency procedures can continue to be delivered and that the hospital can support business as usual activities in addition to the increased demand from disaster response activities. The readiness and capacity to cater for surges in demand at critical times extends to the other hospitals within the health network which will be supported by the emergency generator located at Lake Macquarie Private Hospital. The reliability of power supply will have flow on benefits in terms of avoided delays / backlog of procedures caused by the downtime from power outages and will result in increased safety and better health outcomes for the community.

Increased capacity in the private health care system also provides increased resilience across both the private and public health care system. This has been evident in the recent COVID-19 pandemic where the private system (including Lake Macquarie Private Hospital) has supported the public system by providing additional capacity to the public system within private hospitals to support the freeing-up of beds to support COVID-19 patients. Additional capacity at Lake Macquarie Private Hospital provides increased resilience across the public and private health network for similar incidents in the future.

Economic benefits of additional local employment



The Lake Macquarie Private Hospital Redevelopment aligns with NSW Government and local plans and strategies for growing the Hunter-New England Region.

Lake Macquarie Private Hospital is among Lake Macquarie's largest employers, with a current workforce of 792 nursing, allied health, medical specialist and support staff.³ The Lake Macquarie Private Hospital Redevelopment is expected to provide 169 new staff roles and 20 new visiting medical officer (VMO), anaesthetist and assistant surgeon roles.⁴ The redevelopment will attract skilled workers to the Hunter – New England Region and provide local jobs for local residents, growing the local economy and making the Hunter Region a greater attraction for skilled health care workers. This aligns with the NSW Department of Planning and Environment (2018) *Greater Newcastle Metropolitan Plan 2036*, specifically Strategy 4 – Grow health precincts and connect the health network.⁵ Attraction of speciality health care workers to the region will provide improved access to expertise for both public and private patients.

In addition to the new workforce associated with the on-going operation of the new services provided by the Lake Macquarie Private Hospital Redevelopment, construction of the project will create additional jobs and economic activity during the construction period. It is estimated that construction will create 800 - 1,000 direct and in-direct jobs over the 26-month construction period (February 2023 – April 2025).⁶ The number of direct construction jobs is estimated at 108 full-time equivalent jobs over the construction

³ Provided by Ramsay Health Care Limited for the purpose of this assessment

⁴ Provided by Ramsay Health Care Limited for the purpose of this assessment

⁵ NSW Department of Planning and Environment (2018), *Greater Newcastle Metropolitan Plan 2036*, www.planning.nsw.gov.au, September 2018

⁶ Provided by Ramsay Health Care Limited for the purpose of this assessment

period.⁷ This is equivalent to approximately \$9.5 million (in 2021/22 prices) in additional household income over the construction period.⁸

2.3 Impacts if the redevelopment did not occur

In the absence of the redevelopment of Lake Macquarie Private Hospital, there is a potential that the facility would be unable to continue the delivery of service at the existing site. This would place an increased burden on the already at / close to capacity public health system. Increased demand for health care within the public system will have two key impacts:

- Detrimental health and wellbeing outcomes for the Hunter-New England communities through increased delays in accessing care, overcrowding and increased travel times and costs to access care further from home. Lake Macquarie Private Hospital provides the only private emergency department in the Hunter-New England Region and, as such, patients would need to access public emergency departments should Lake Macquarie Private Hospital no longer provide this service. Public emergency departments are currently available at Belmont Hospital (9km / 13 mins from Lake Macquarie Private Hospital) and John Hunter Hospital (10km / 14 mins from Lake Macquarie Private Hospital). Both of these emergency departments are currently operating at or close to capacity.⁹
- Increased costs to the NSW Government through both operating and capital expenditure. The movement of patients from the private to public health care system will mean that the NSW Government would experience greater burden in the delivery of health care. As the average cost of care at a public hospital is \$5,030 per inpatient separation (in 2021/22 prices)¹⁰, this would equate to an additional operating cost to the NSW Government of \$81.9 million (in 2021/22 prices) in 2025 based on projected inpatient admissions of 16,280 in 2025 post-redevelopment¹¹. In addition, the NSW Government would also experience additional operating costs associated with the 14,690 day-only admissions, 5,000 day surgery attendances and 19,245 emergency department attendances not considered within this calculation. In addition, as there is greater pressure and demand for the public health system, the NSW Government may need to invest in the expansion of capacity to meet the future demand. This investment could require significant capital investment from the NSW Government to ensure the continued delivery of care for patients.

Further, Lake Macquarie Private Hospital plays an important role in the Hunter-New England community. It is one of the largest employers in Lake Macquarie, providing 792 skilled jobs and a source of economic activity. Since commencement of ownership over Lake Macquarie Private Hospital in 2002, Ramsay Health Care Limited has invested significantly in the facility to provide the bed base and services it provides today. Since 2002, the total investment in the facility is \$91.1 million (nominal), including investment in furniture, fittings and equipment. This represents significant investment in providing private health care to the local community, including creation of jobs and economic activity.

It also plays an important role in the character of the local community through the following endeavours that would be lost were Lake Macquarie Private Hospital unable to continue the delivery of service:

- Major sponsorship of the Ramsay Health Care Lake Macquarie Running Festival.
- Support of the Music in the Park community event held on Friday nights through summer
- Sponsorship of two major sporting clubs.

⁷ NSW Treasury (2021) NSW Treasury Employment Calculator, [cited at www.treasury.nsw.gov.au, published 19 September 2021, viewed 28 September 2021], assumes construction industry average direct employment multiplier of 0.9 full-time equivalent jobs per \$1 million expenditure.

⁸ Australian Bureau of Statistics (2021), Average Weekly Earnings, Australia, May 2021, Released 19 August 2021, adopted average weekly earnings by industry (construction), full time adults by industry, original

⁹ Bureau of Health Information (2021), Healthcare Observer, Emergency Department statistics – Belmont Hospital and John Hunter Hospital, Apr-Jun 2021 (estimated using time from arrival to leaving and comparison across public hospitals in local health district – Belmont (53%), John Hunter Hospital (51.5%) leaving within 4 hours

¹⁰ Australian Institute of Health and Welfare (2019), Spending on admitted patients, [cited at www.aihw.gov.au, published 22 October 2019, viewed 27 September 2021] – assumes the national weighted average unit (NWAU) for John Hunter Hospital for 2014-15 across all acute admitted patients for 2014/15 – escalated to 2021/22 dollars using consumer price index of 1.6%

¹¹ Inpatient admission projects post-development provided by Ramsay Health Care Limited for the purpose of this assessment.

Social and economic benefits

- Breakfast club for local primary school.
- Membership of both Warners Bay business network and Hunter Chamber of Business.

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